

GTT Users meeting

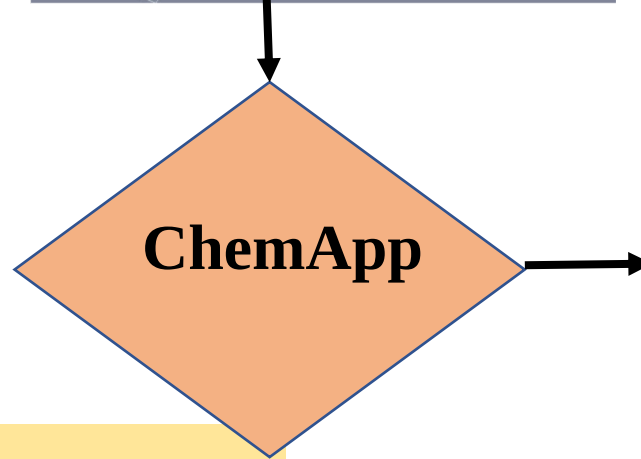
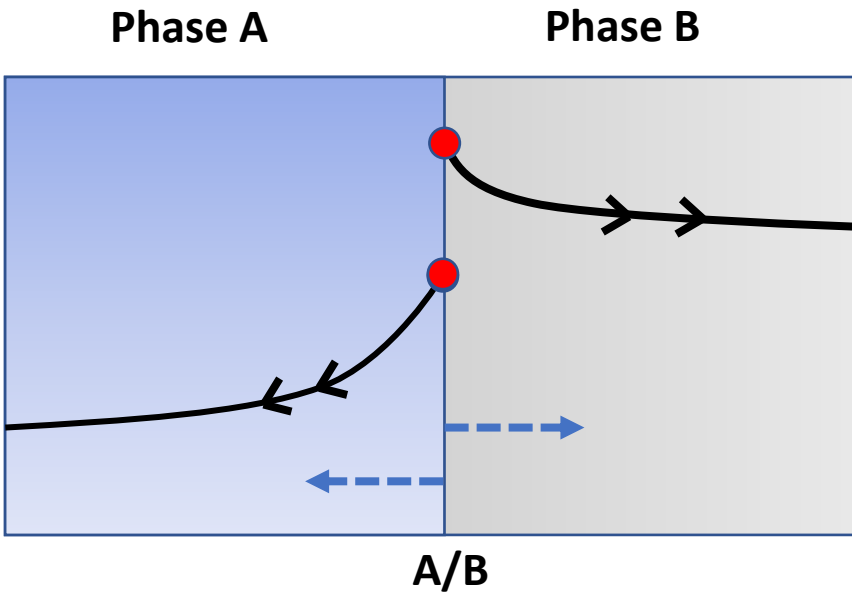
29-30 June 2022

Modelling of solid-state transformation kinetics in alloys using the ChemApp thermodynamic library: few case studies on commercial alloys

Manas Paliwal
Assistant Professor
Metallurgical and Materials Science
IIT Kharagpur

- *Nishant Kumar * SNU*
- *Ashutosh Kumar and Siddharth Samrah * McGill University*
- *Prof. In-Ho Jung SNU*

ChemApp for solving phase transformation problems



$$v = \left(\frac{dx}{dt} \right) = \frac{J_k^{R/L} - J_k^{L/R}}{C_k^{R/L} - C_k^{L/R}}$$

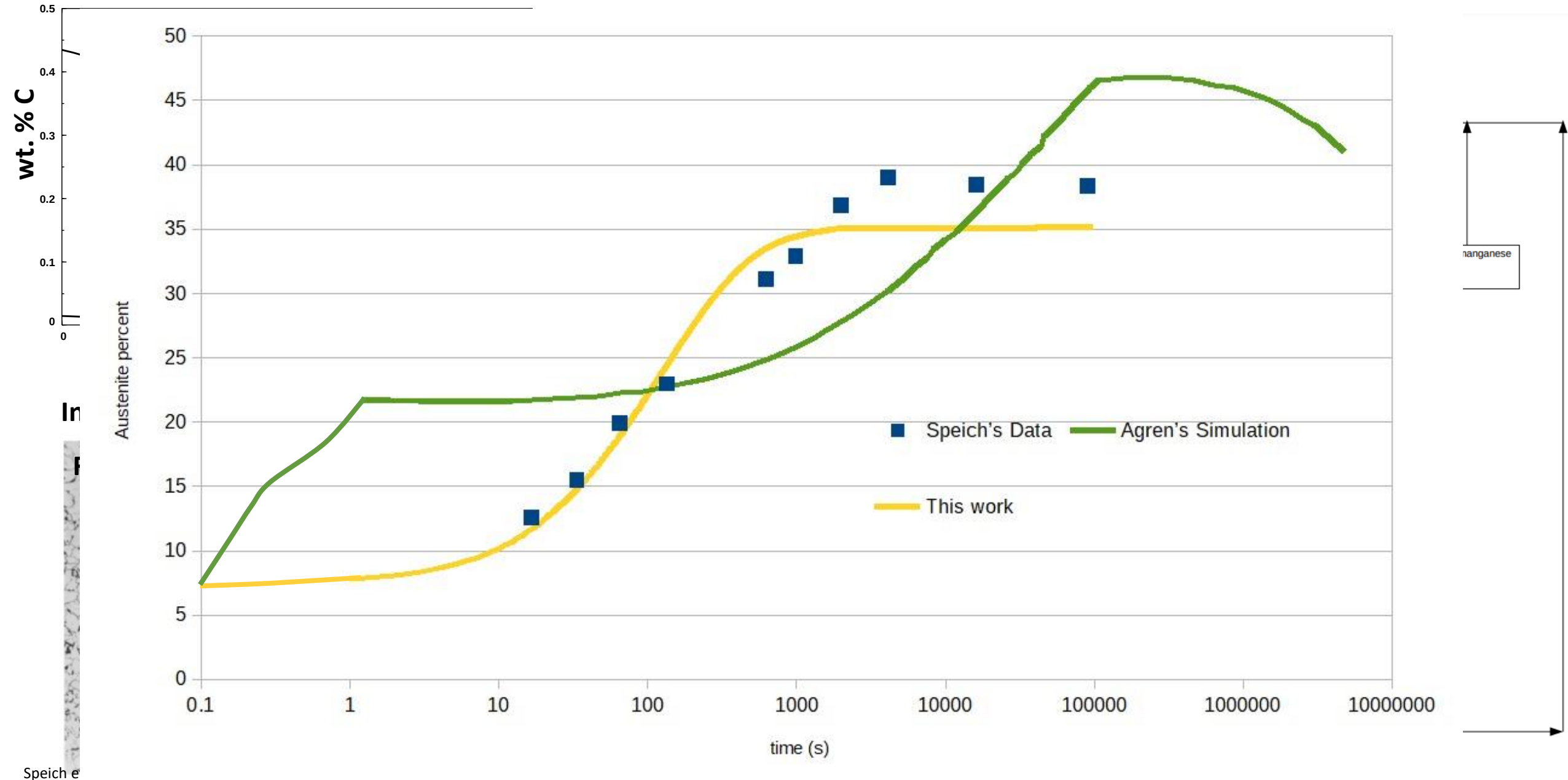
$$J_k = \sum_{j=0}^{n-1} D_{kj}^n \frac{\partial C_j}{\partial x}$$

$$D_{kj}^n = \sum_{i=0}^n (\delta_{ik} - c_k) c_i M_i \left(\frac{\partial \mu_i}{\partial c_j} - \frac{\partial \mu_i}{\partial c_n} \right)$$

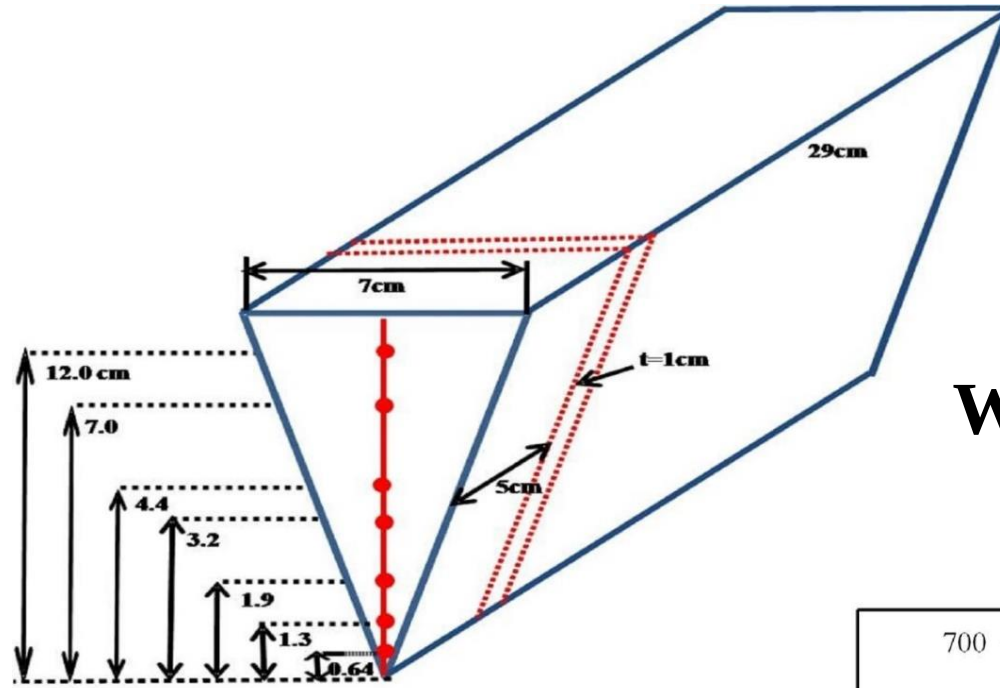
$$\frac{\partial C_k}{\partial t} = \nabla \cdot (D_{kj}^n \nabla C_k)$$

- * Solidification calculations
- * Phase dissolution or growth
- * Solute redistribution
- * Precipitation calculations

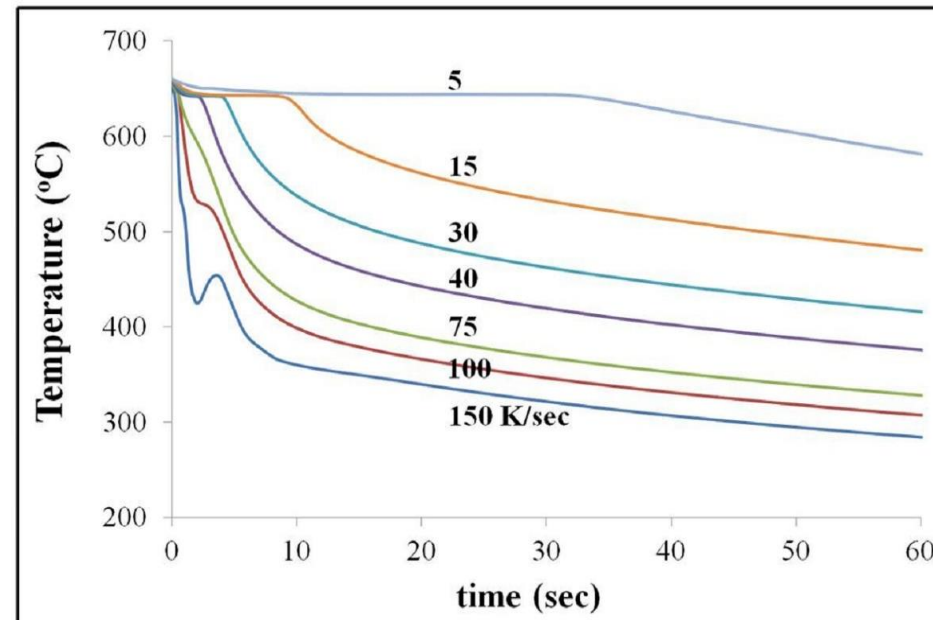
Ferrite to Austenite Growth: Fe-1.5 Mn-0.06 C system



Mg- 6 wt. % Sn – 1 wt. % Al: As-cast



Water cooled Cu mold



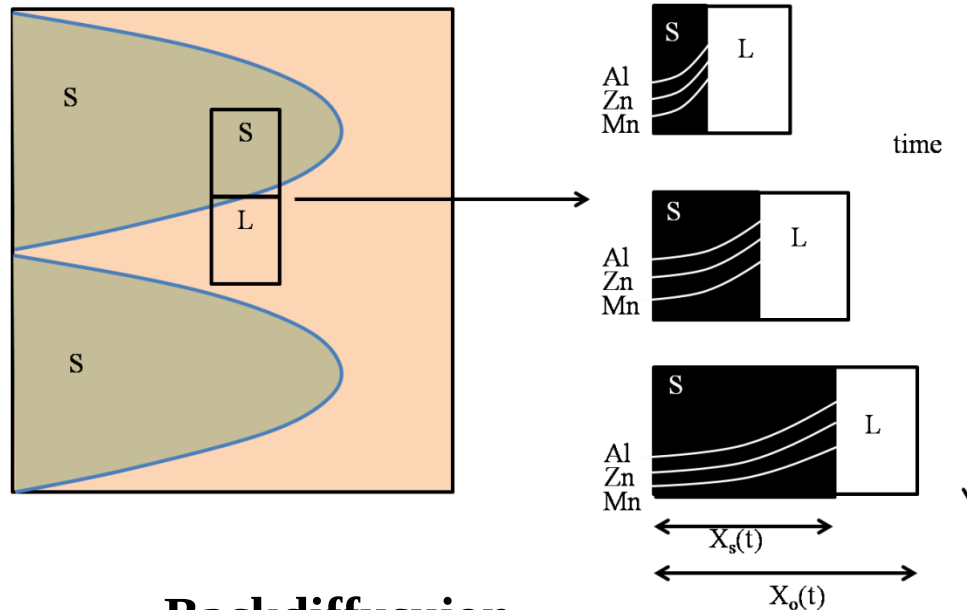
Solidification model

Morphology

Kurz, Giovanola and Trivedi (KGT model)

Kurz W, Giovanola B, Trivedi R. Acta Metall. 1986;34:823

Microsegregation



Backdiffusion

$$\frac{\partial C_{si}}{\partial t} = D_{si} \frac{\partial^2 C_{si}}{\partial x^2}$$

Solute balance

$$\int_0^{X_{si}} C_{si} dx + \int_{X_{si}}^{X_o} C_{li} dx = X_o C_{oi}$$

Coarsening²

$$X_o(t)^3 - X_o(0)^3 = \int_0^t M_i dt$$

Local thermodynamic eqb.

$$C_{si} = k_i C_{li}$$

[4]. M. Paliwal and I.-H Jung, Acta Mat. 61 (2013) 4848-4860.

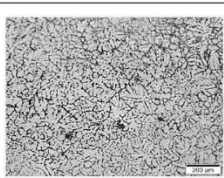
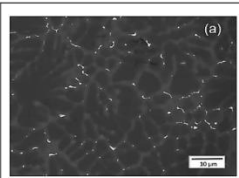
[5]. M. Paliwal, D.-H Kang, E. Esaadiqi and I.-H Jung Metall. Trans. 45A (2014) 3308-3320

[6]. M. Paliwal and I.-H Jung, J. Cryst. Growth, 394 (2014) 28-38.

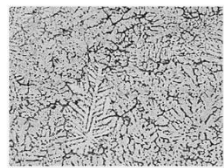
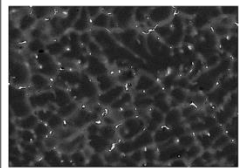
² Roosz et al. Mat. Sci. Tech. 1986;2:1149

Mg- 6 wt. % Sn – 1 wt. % Al: As-cast

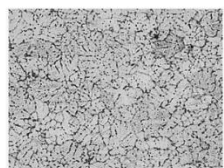
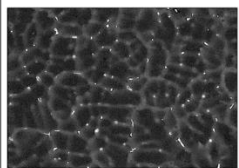
150K/sec



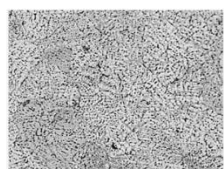
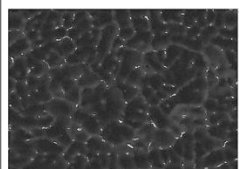
100K/sec



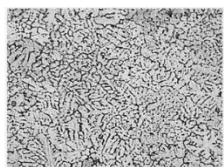
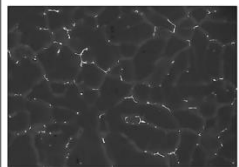
75K/sec



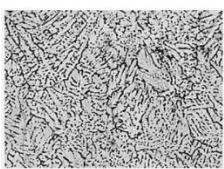
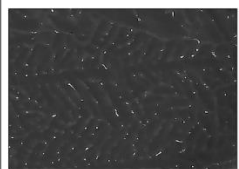
40K/sec



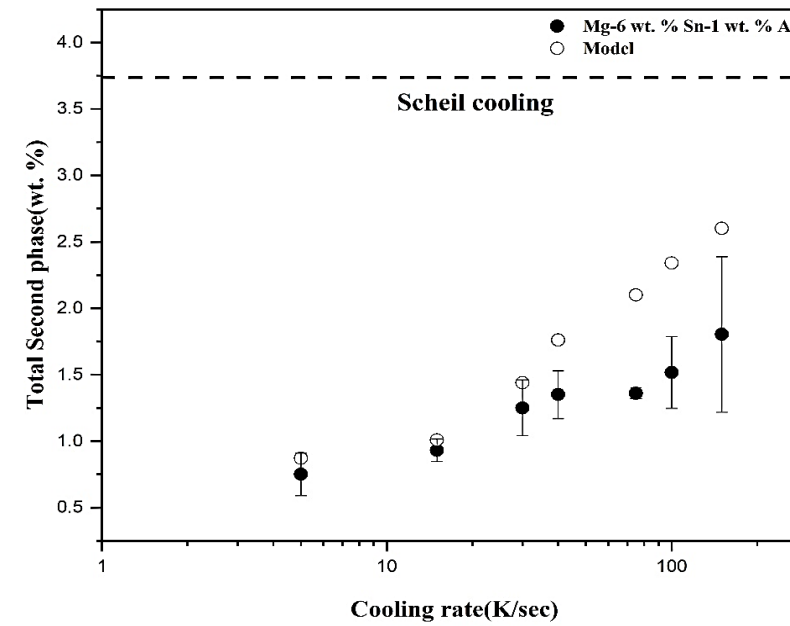
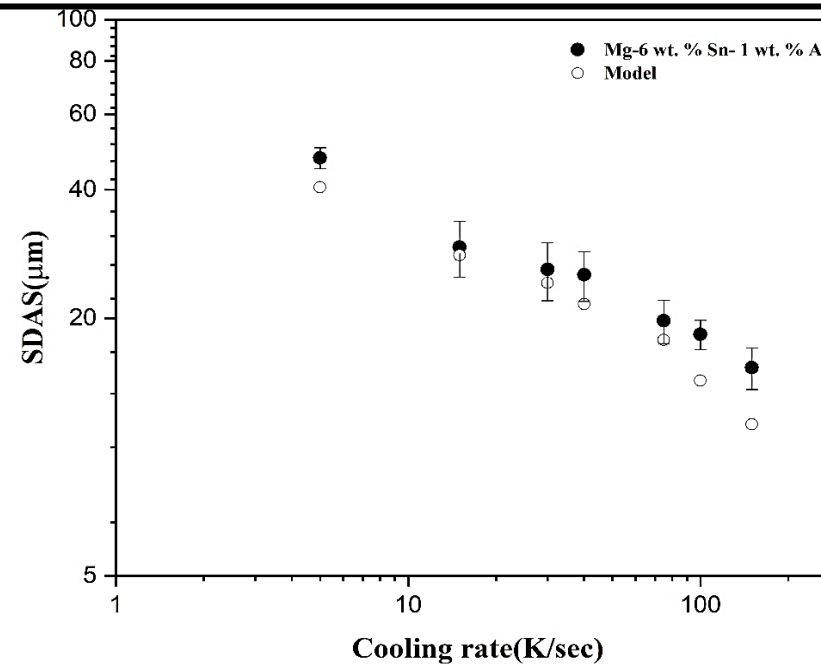
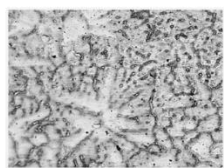
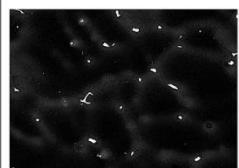
30K/sec



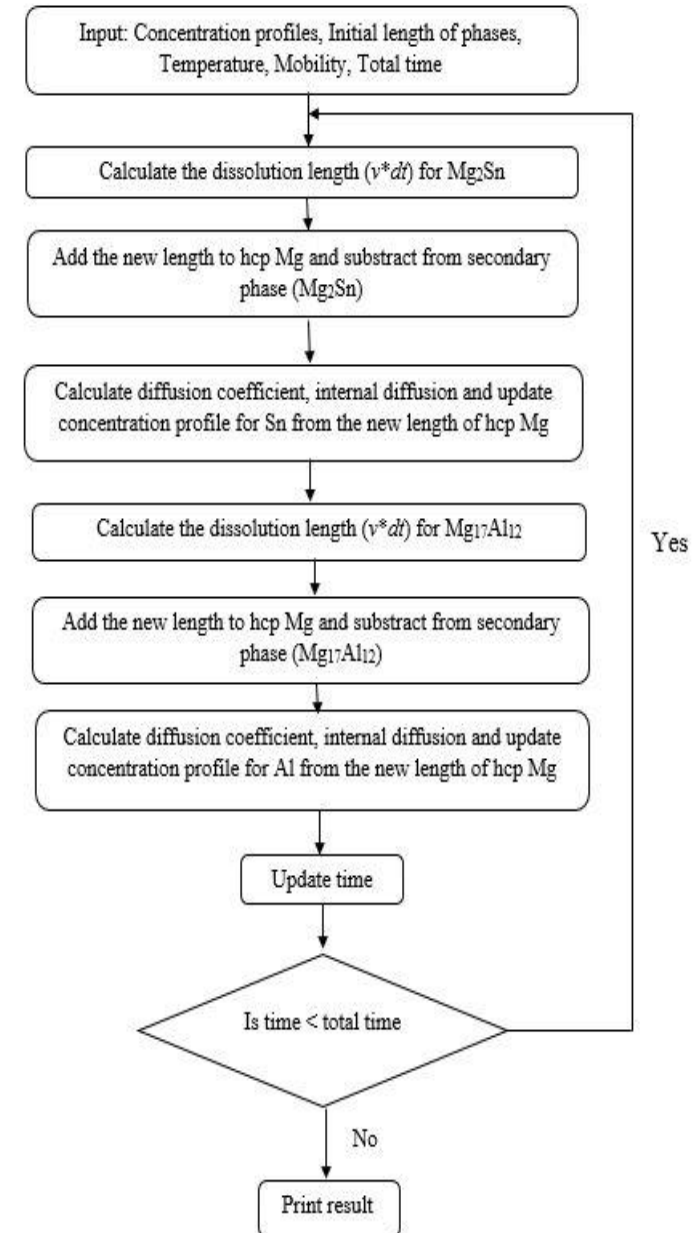
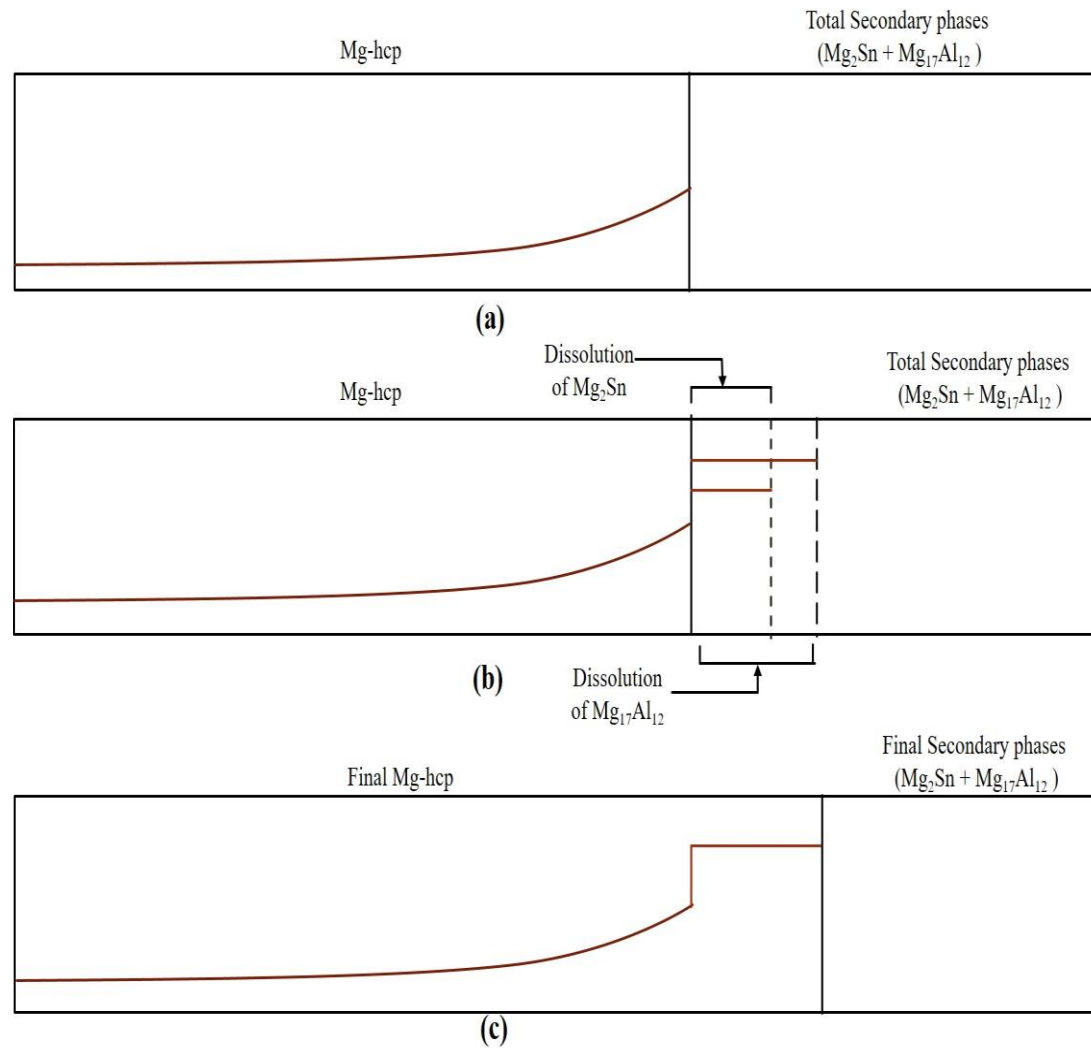
15K/sec



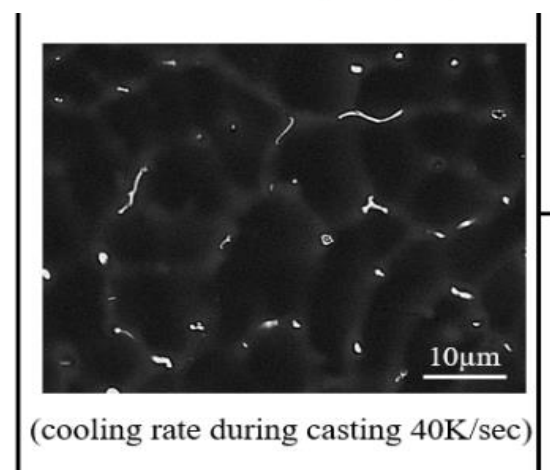
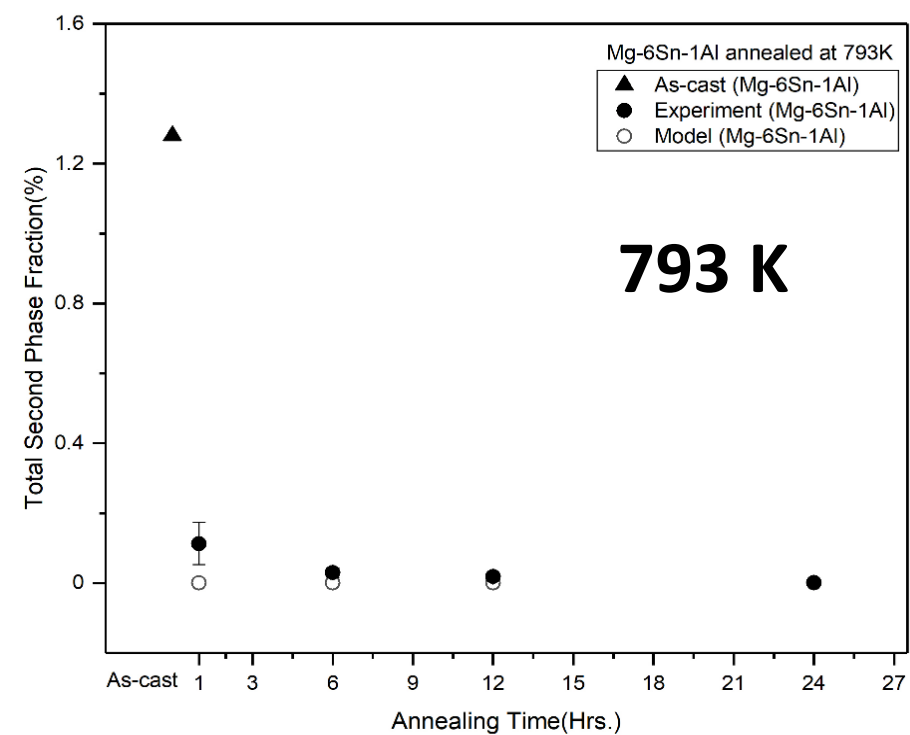
5K/sec



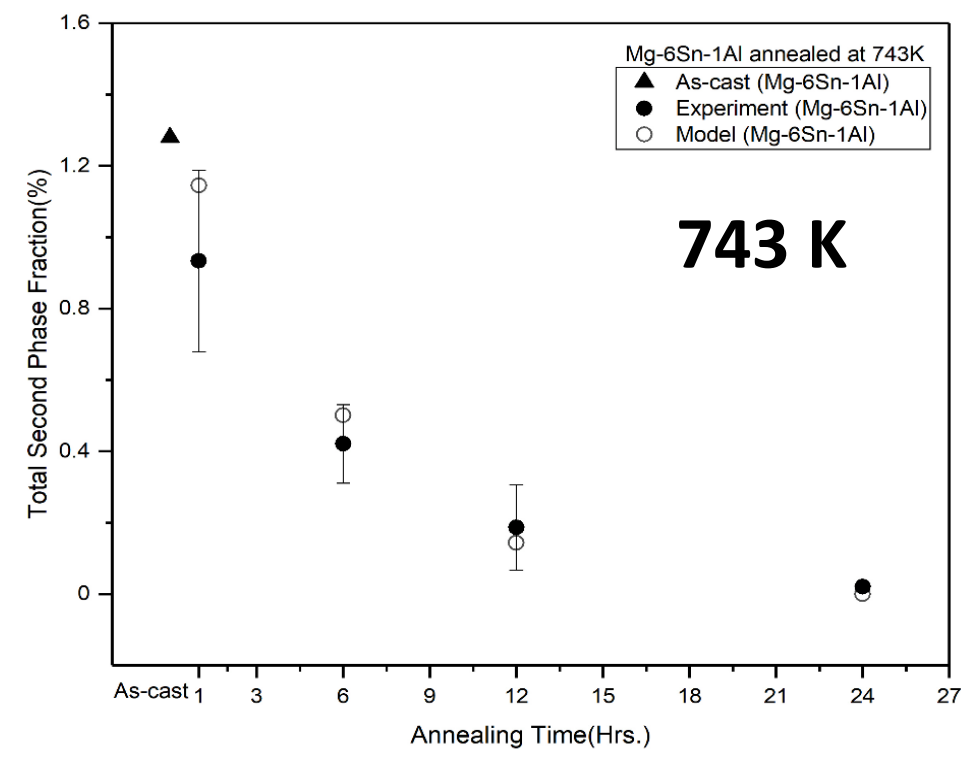
Homogenization and dissolution model



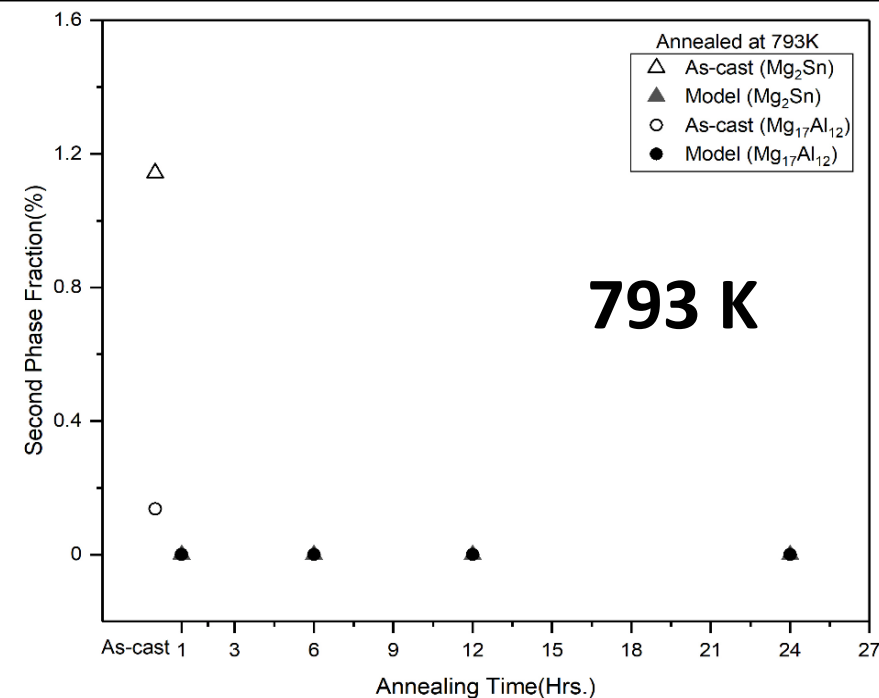
Mg- 6 wt. % Sn – 1 wt. % Al: Homogenization



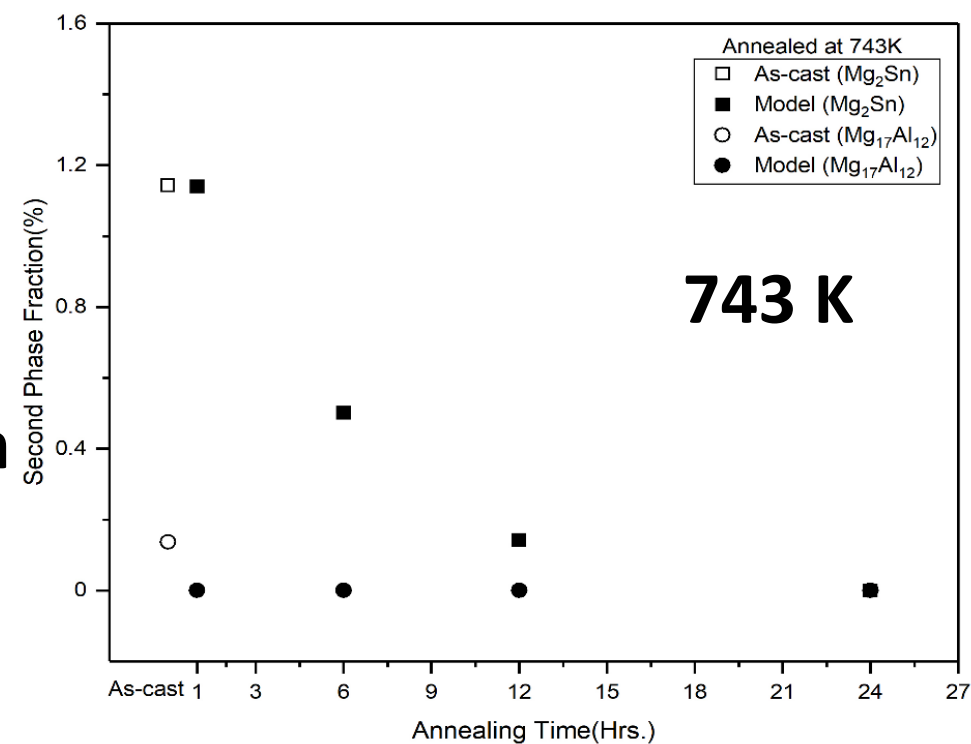
As-cast: Mg_2Sn + $Mg_{17}Al_{12}$



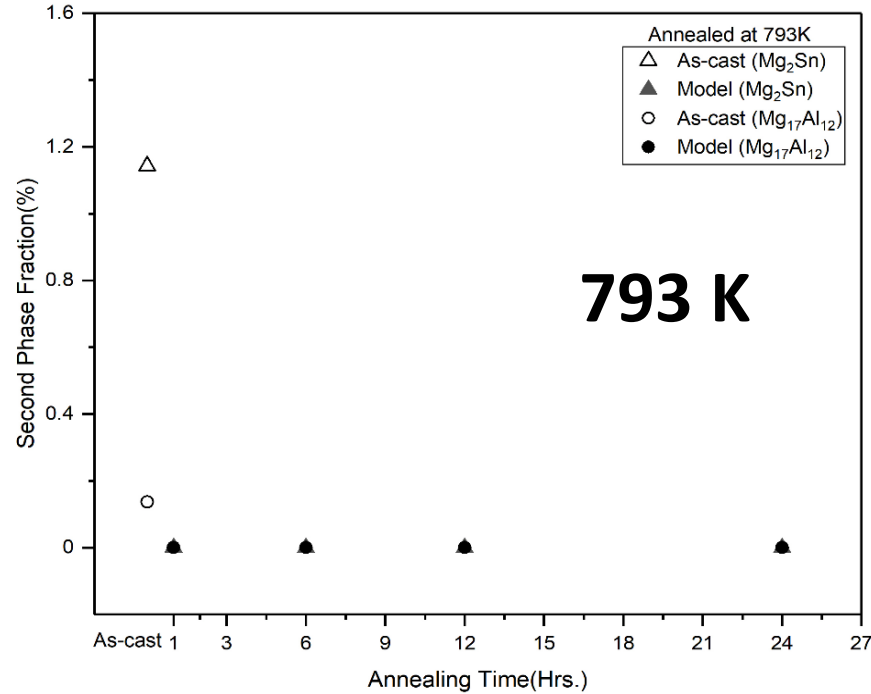
Mg- 6 wt. % Sn – 1 wt. % Al



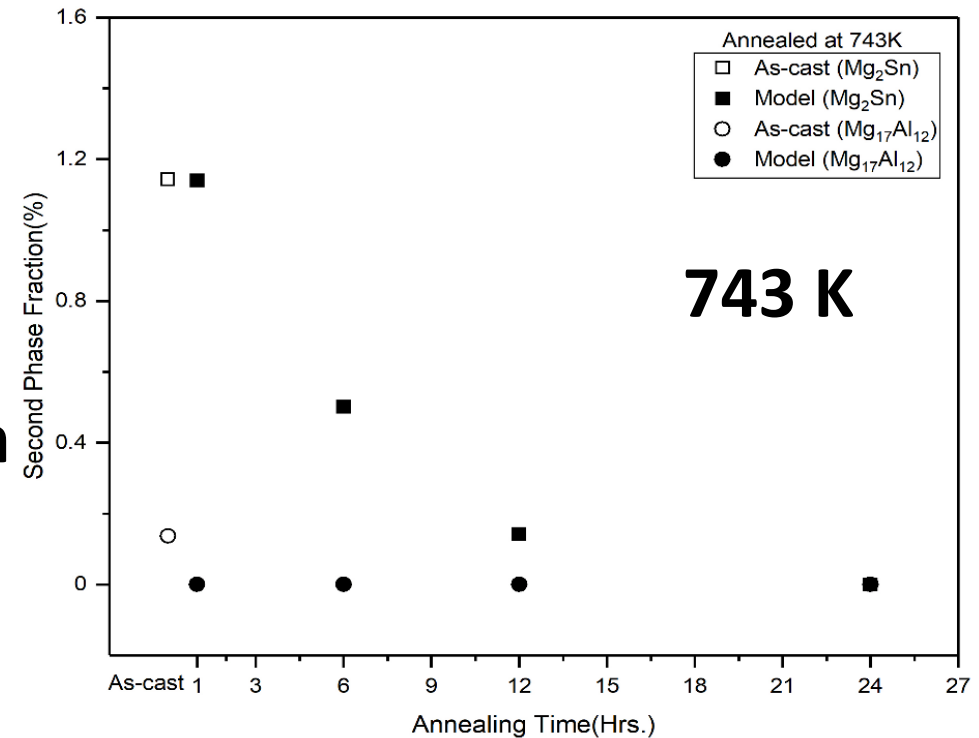
Dissolution kinetics of Mg_2Sn and $Mg_{17}Al_{12}$ phases are different



Mg- 6 wt. % Sn – 1 wt. % Al

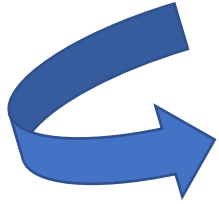


Dissolution kinetics of Mg_2Sn and $\text{Mg}_{17}\text{Al}_{12}$ phases are different



Ni alloy making route: Downstream process for 925 alloy

Secondary phase



Homogenization
1150-1200 °C

Extrusion
1100 °C

**Solution
Treatment**
1030-1050 °C

Ageing
720 °C

As-cast

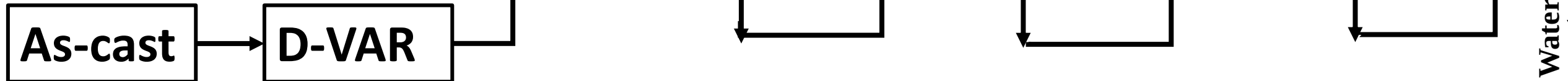
D-VAR

Air cooled

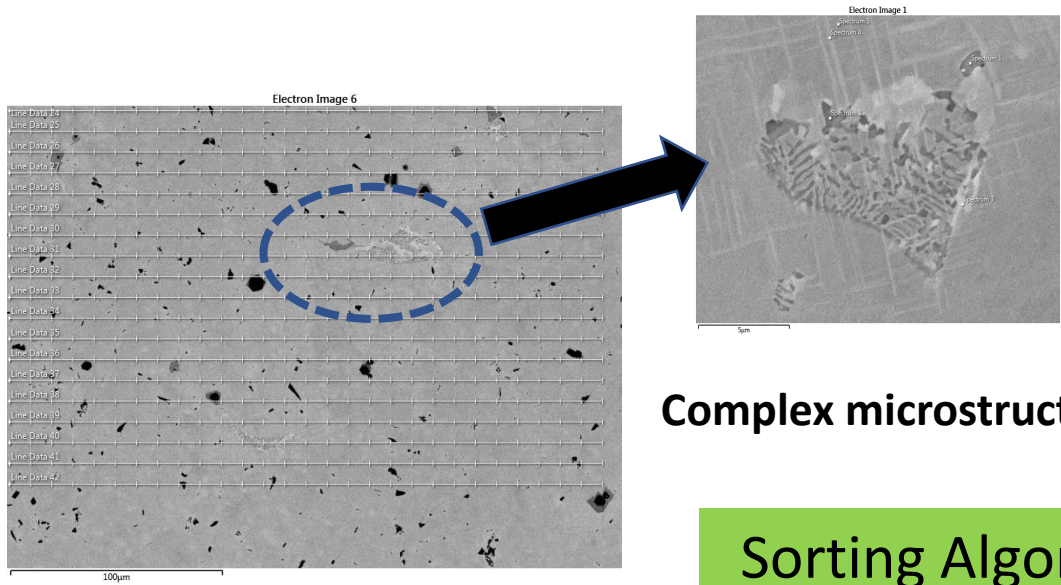
Air cooled

Water quenched

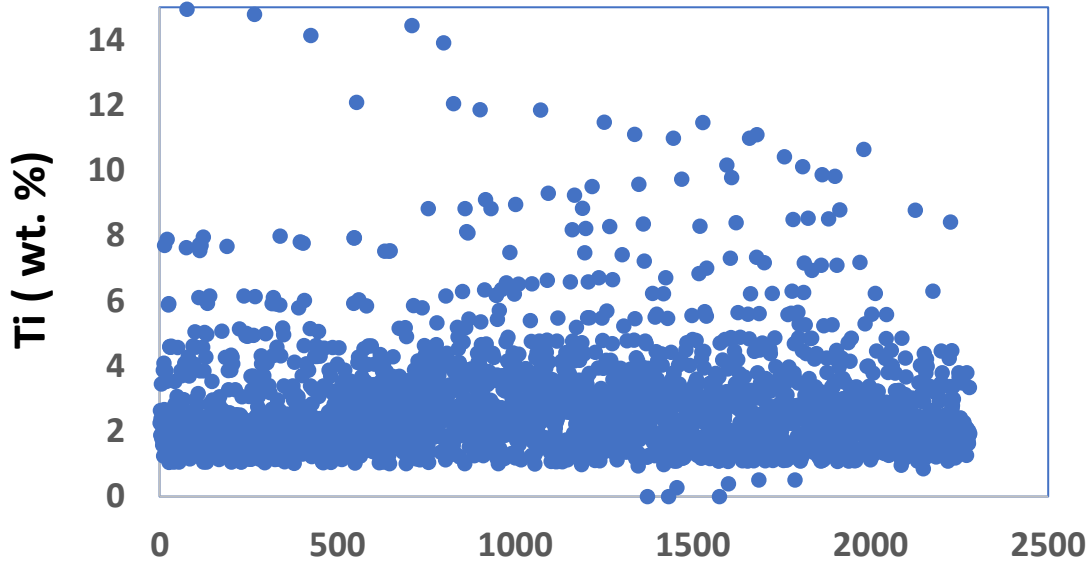
Water quenched



925 Alloy: As-cast microstructure characterization

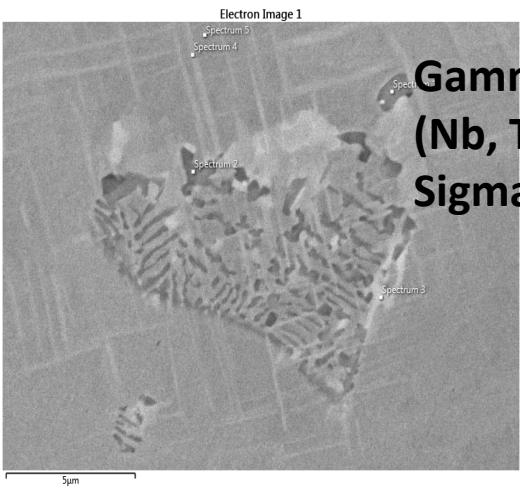


Complex microstructure



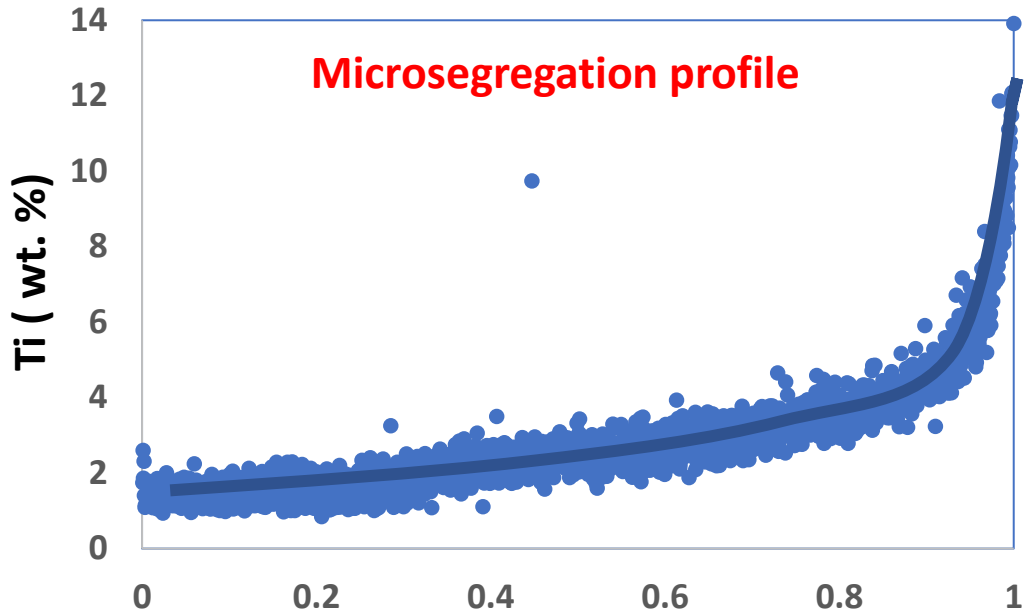
Sorting Algorithm: Microsegregation

Secondary Phases



Gamma Phase,
(Nb, Ti) (C,N)
Sigma Phase

Homogenization
calculations

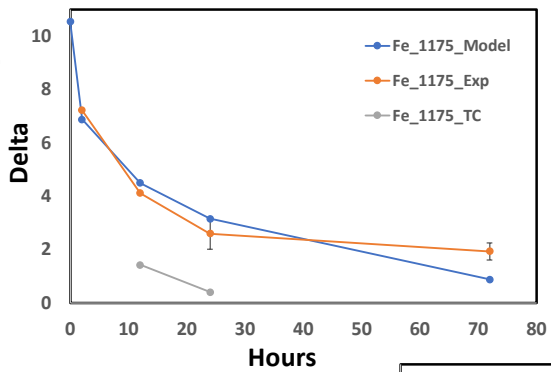
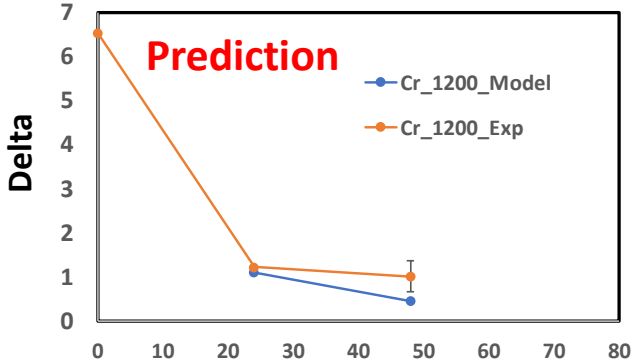
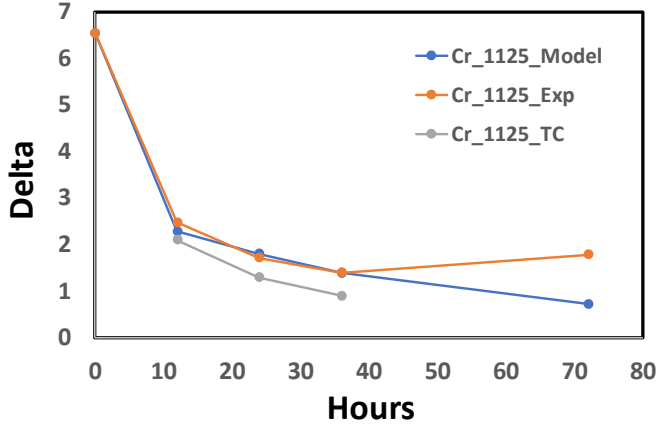
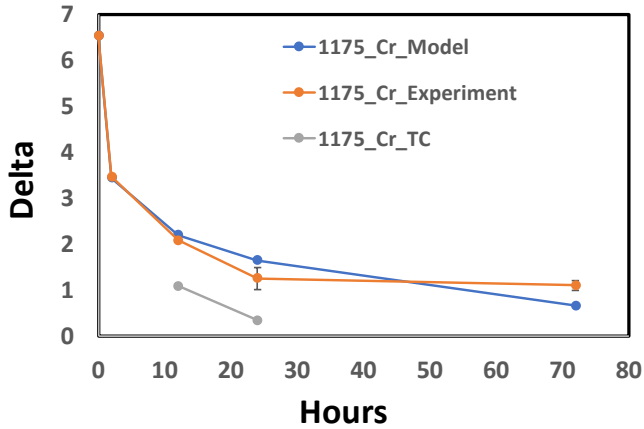


Solid fraction

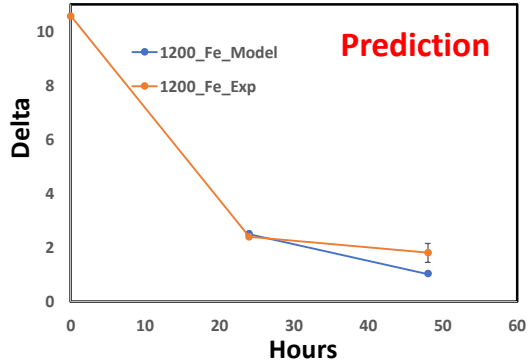
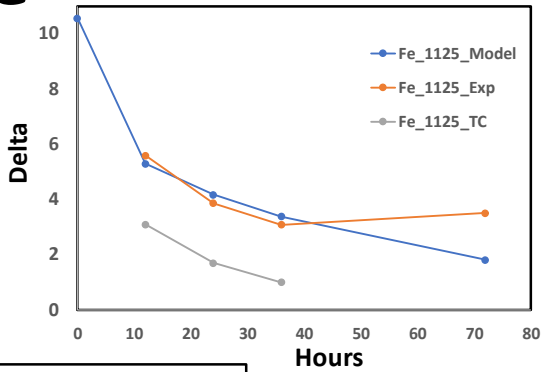
Ni 925 alloy: Homogenization

C	Si	Mn	Cr	Ni	Mo	W	Co	V	Ti	Cu	Al	Nb	B	N	Mg
0.01	0.2	0.39	20.25	42.75	3.03	<0.01	0.033	0.054	2.38	1.92	0.26	0.31	0.0029	0.007	0.032

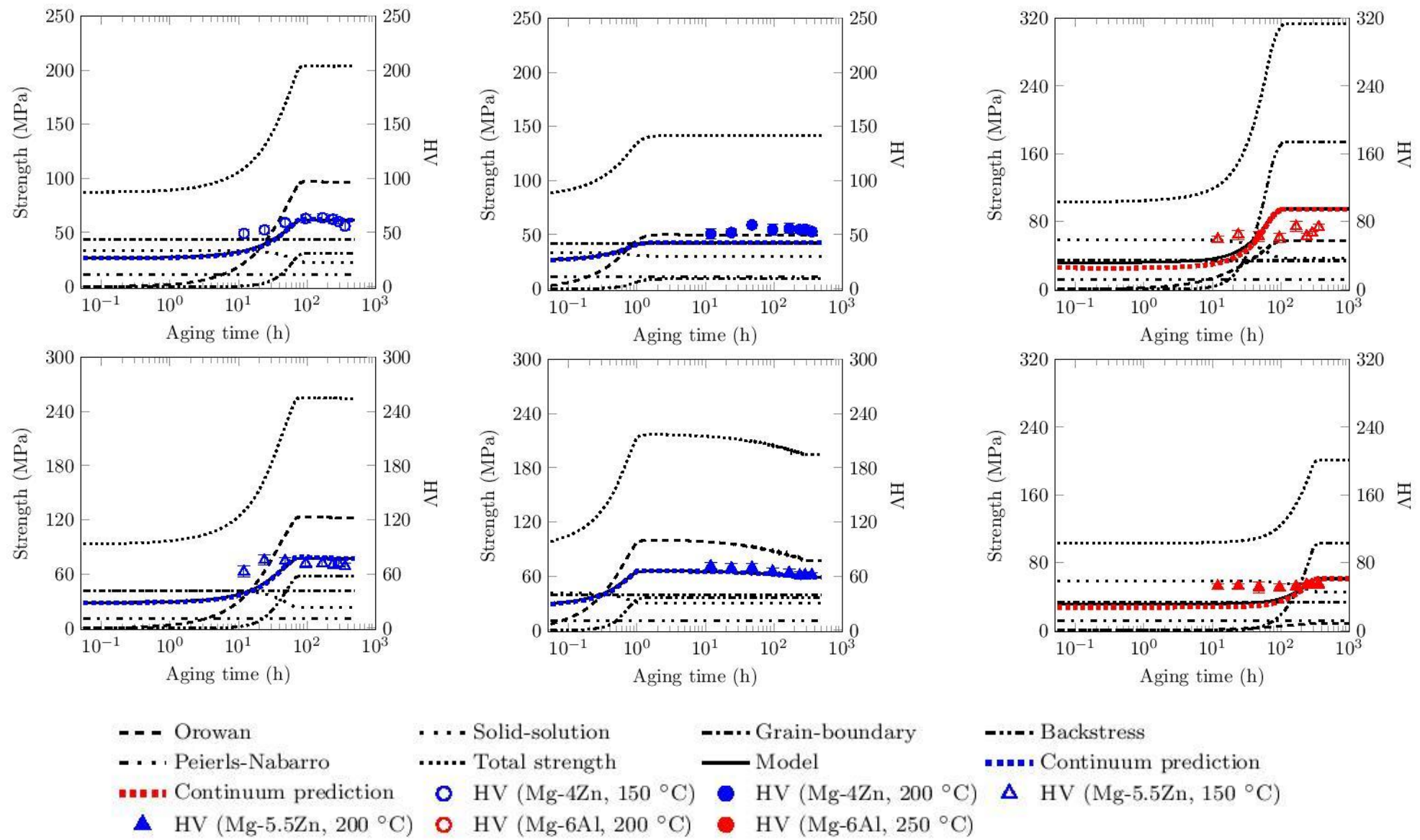
Cr



Fe



Strength Prediction



* Samrah et al. Mechanics of Materials 2022

Thank you

manas.paliwal@metal.iitkgp.ac.in