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Materials Chemistry II

-Applications 2-

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Outline

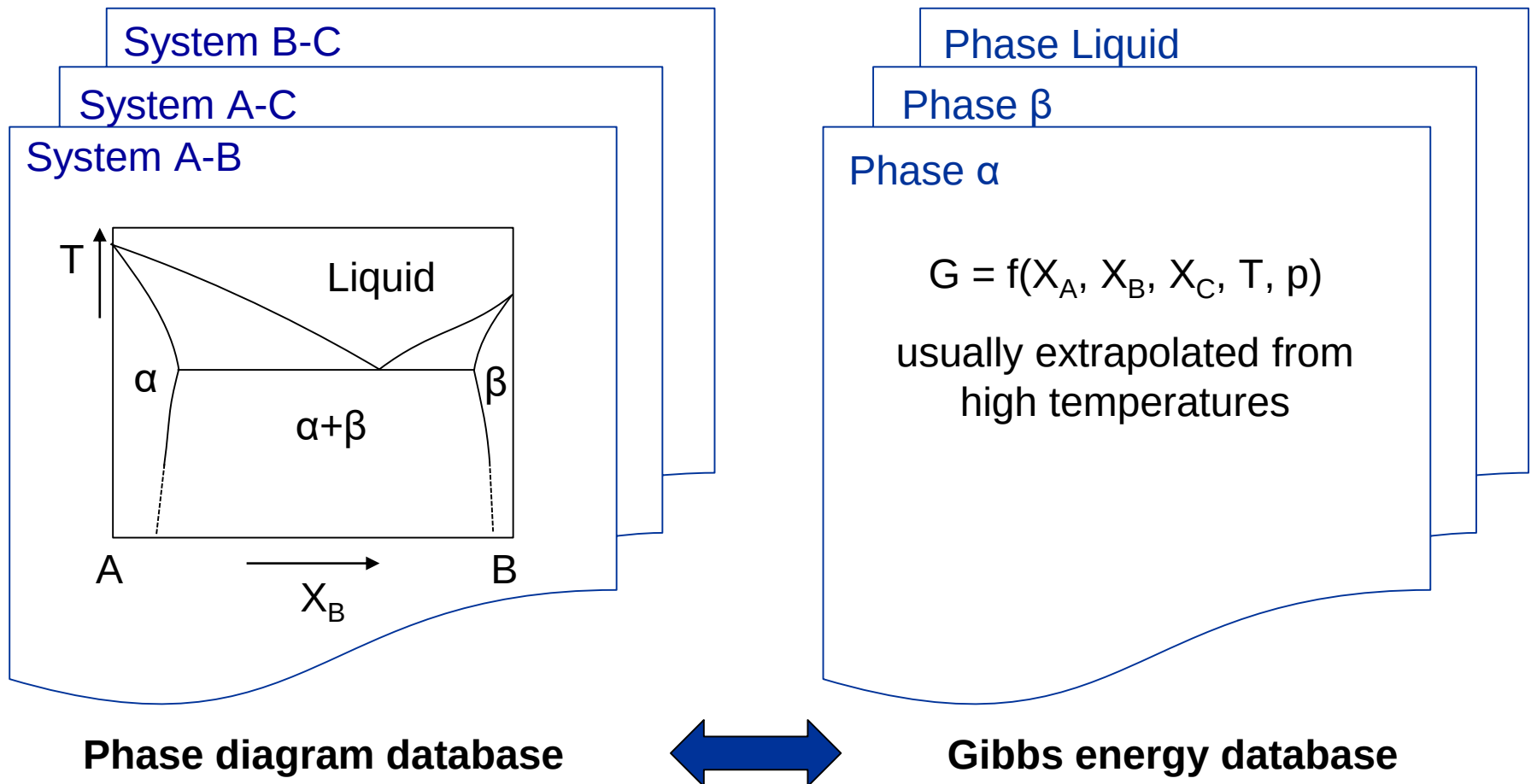
1. Understanding processes&materials based on $G(x,T,p)$
QUALITATIVE APPLICATION OF MC II
2. Modelling $G(x,T,p)$ based on theory&experiment
QUALITATIVE $\rightarrow$ QUANTITATIVE
3. Modelling processes&materials based on $G(x,T,p)$
QUANTITATIVE APPLICATION OF MC II

Outline

1. Understanding processes&materials based on $G(x,T,p)$
QUALITATIVE APPLICATION OF MC II
2. **CalPhaD method**
Calculation of Phase Diagrams
3. Modelling processes&materials based on $G(x,T,p)$
QUANTITATIVE APPLICATION OF MC II

CalPhaD

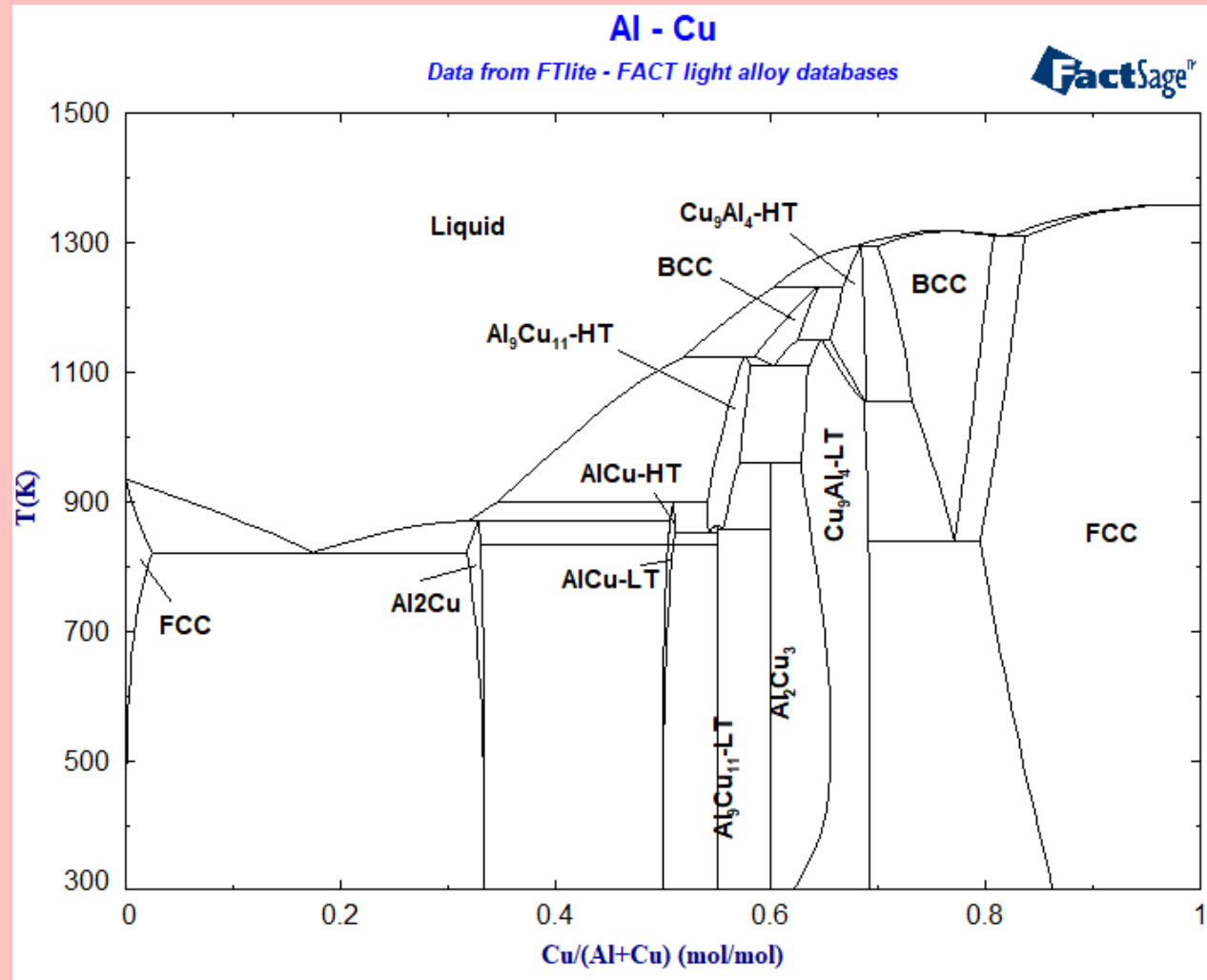
(Calculation of Phase Diagrams)



What information can be extracted from the Al-Cu phase diagram?

A) $\Omega_{\text{fcc}} < \Omega_{\text{bcc}}$

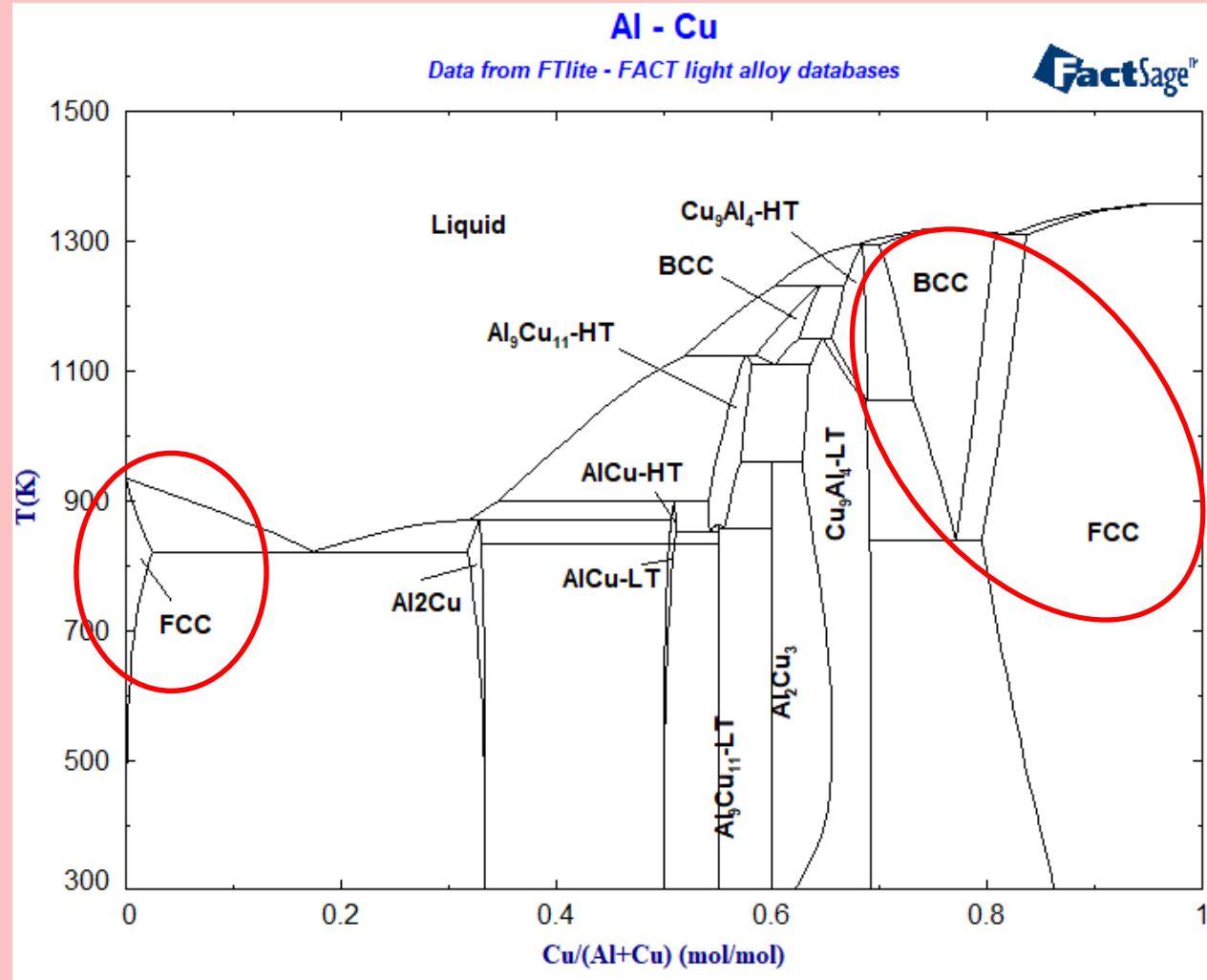
B) $\Omega_{\text{fcc}} > \Omega_{\text{bcc}}$



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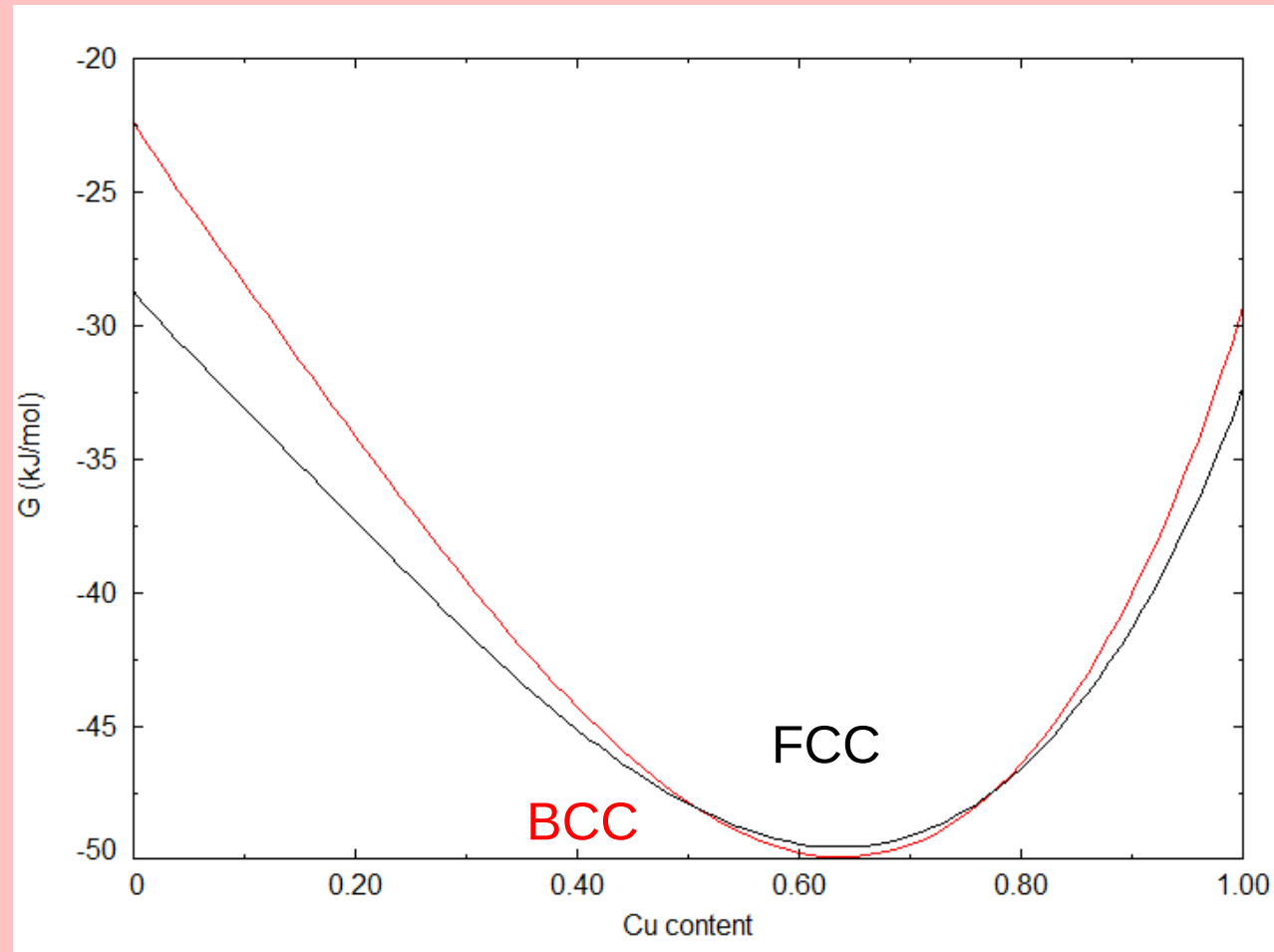
B) $\Omega_{\text{fcc}} > \Omega_{\text{bcc}}$



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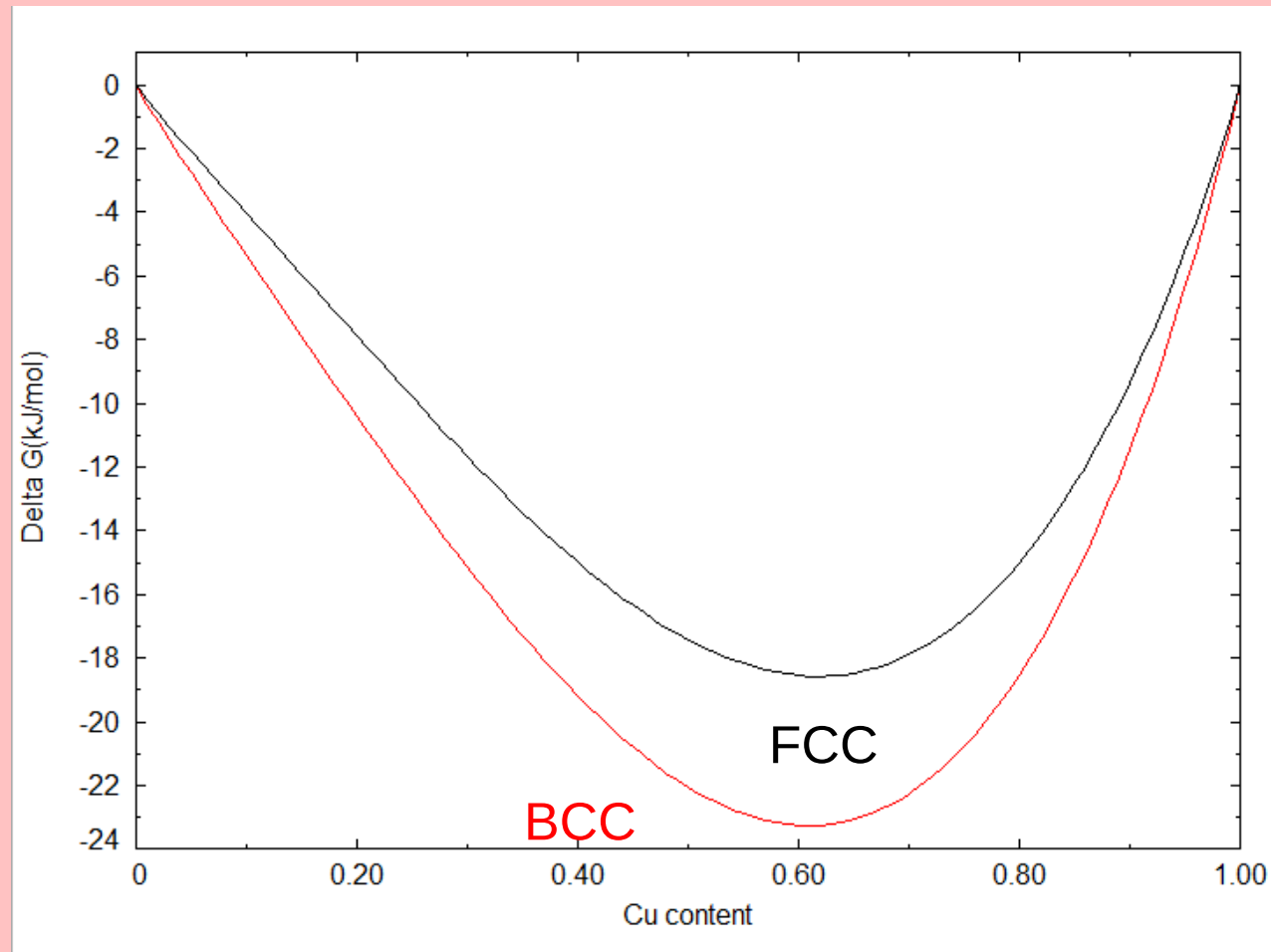
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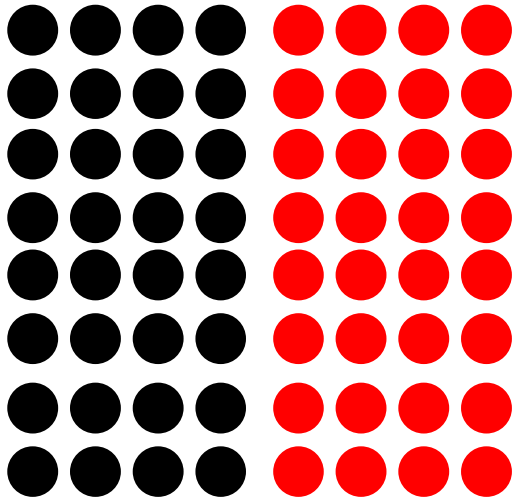
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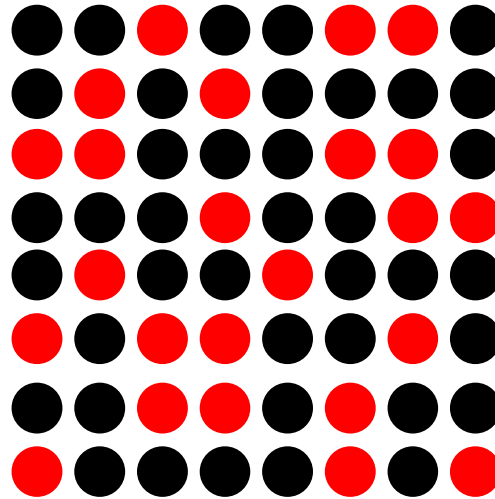
Strategy:

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}}$$

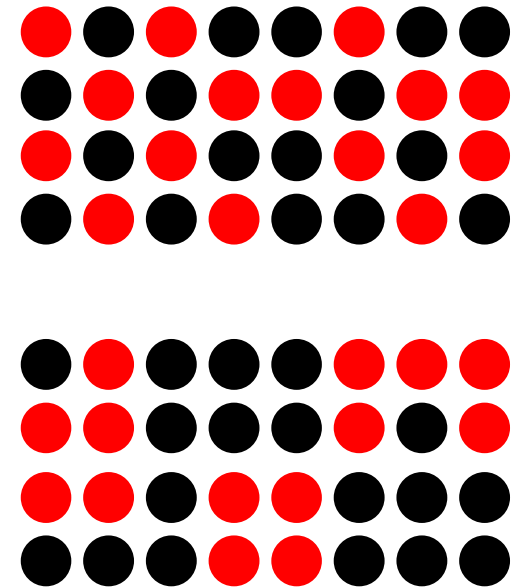
Think about **bonds** & **configurations**



mechanical mixture
(two powders)



ideal/regular solution
mixed



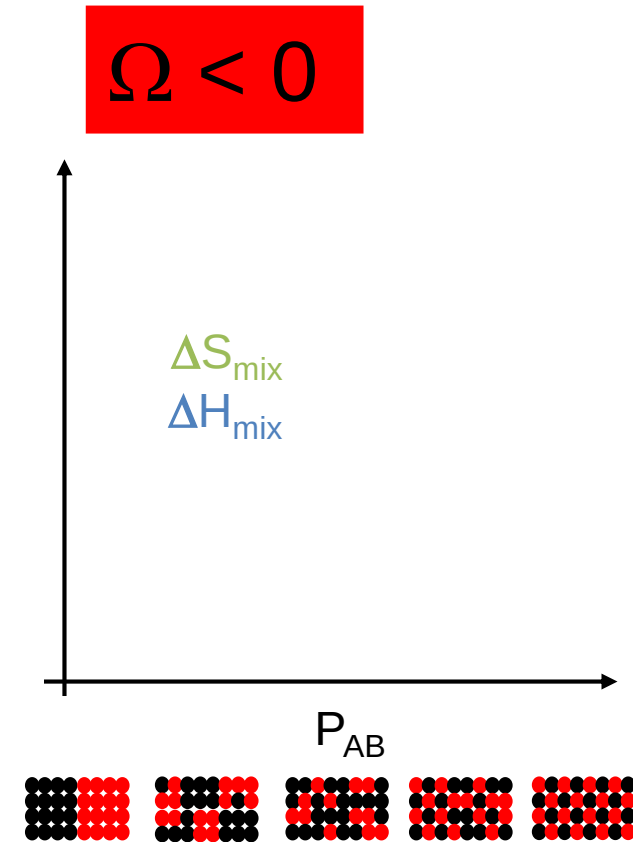
real solution
ordering/clustering

What happens if Ω is significantly different from 0?

Example: Solution of 50% A and 50% B

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}}$$

- ΔG_{mix} minimizes with **minimum** ΔH_{mix} and **maximum** ΔS_{mix}

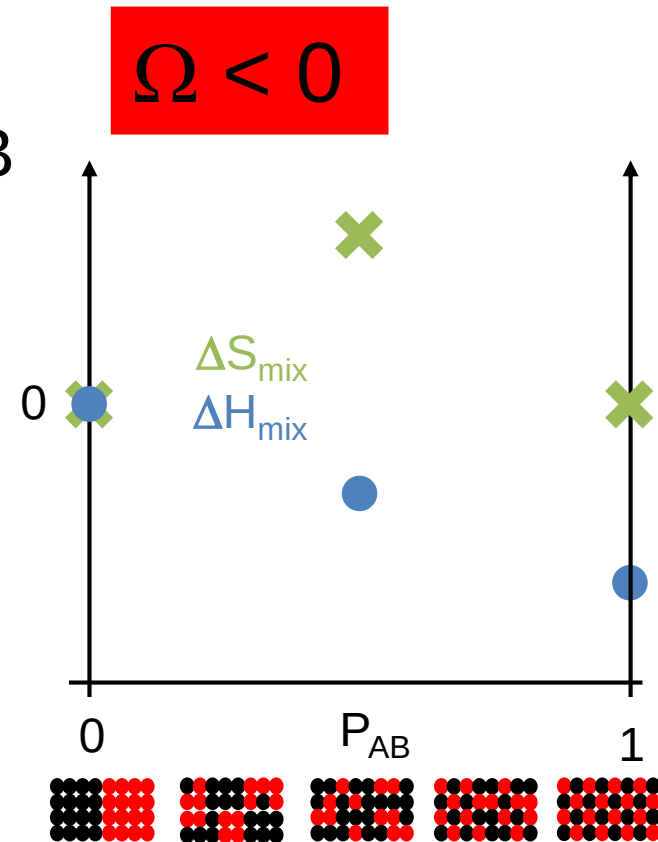


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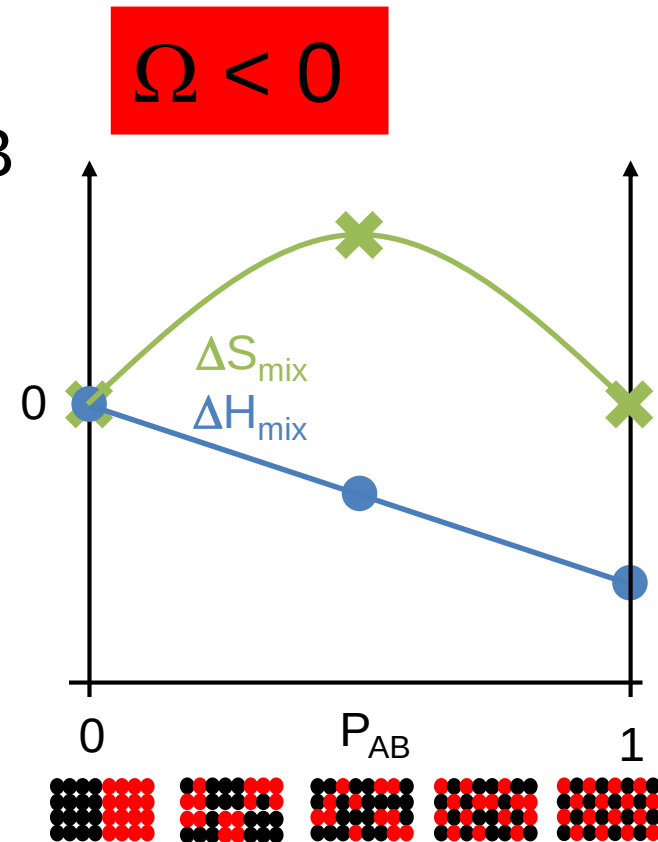


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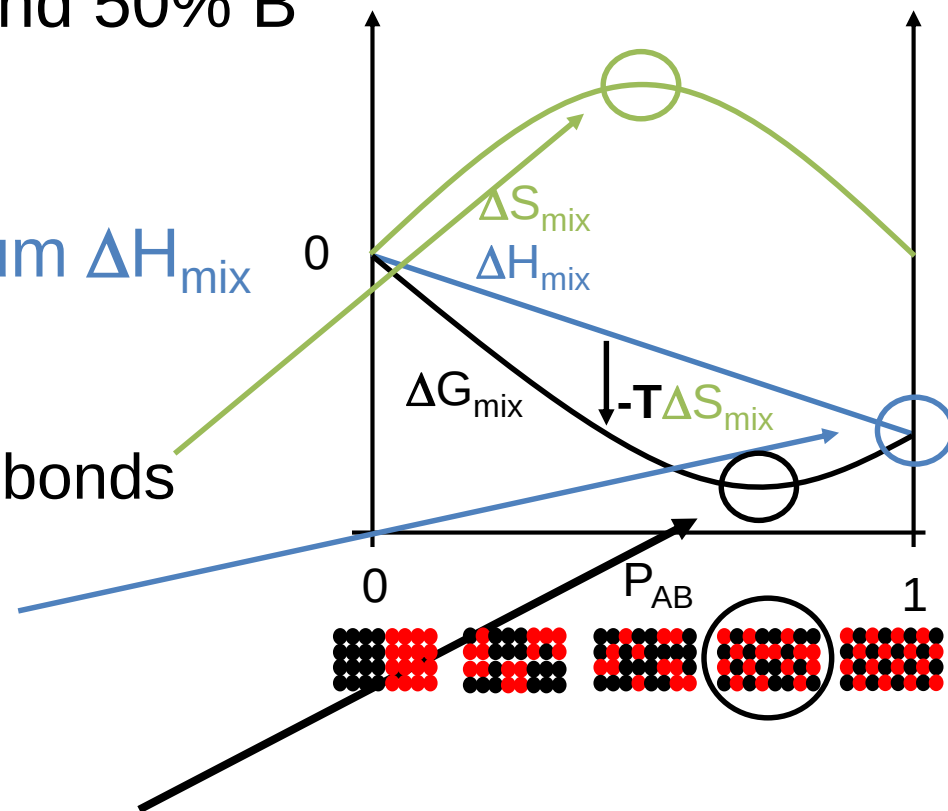
- ΔG_{mix} minimizes with **minimum** ΔH_{mix} and **maximum** ΔS_{mix}

ΔS_{mix} maximizes when # of A-B bonds
 $= 2 \cdot X_A \cdot X_B$

ΔH_{mix} minimizes with **maximum**
 number of A-B bonds

ΔG_{mix} minimizes between 0.5 and 1!

$$\Omega < 0$$



What happens if Ω is significantly different from 0?

$$\Omega < 0$$

Example: Solution of **75% A** and **25% B**

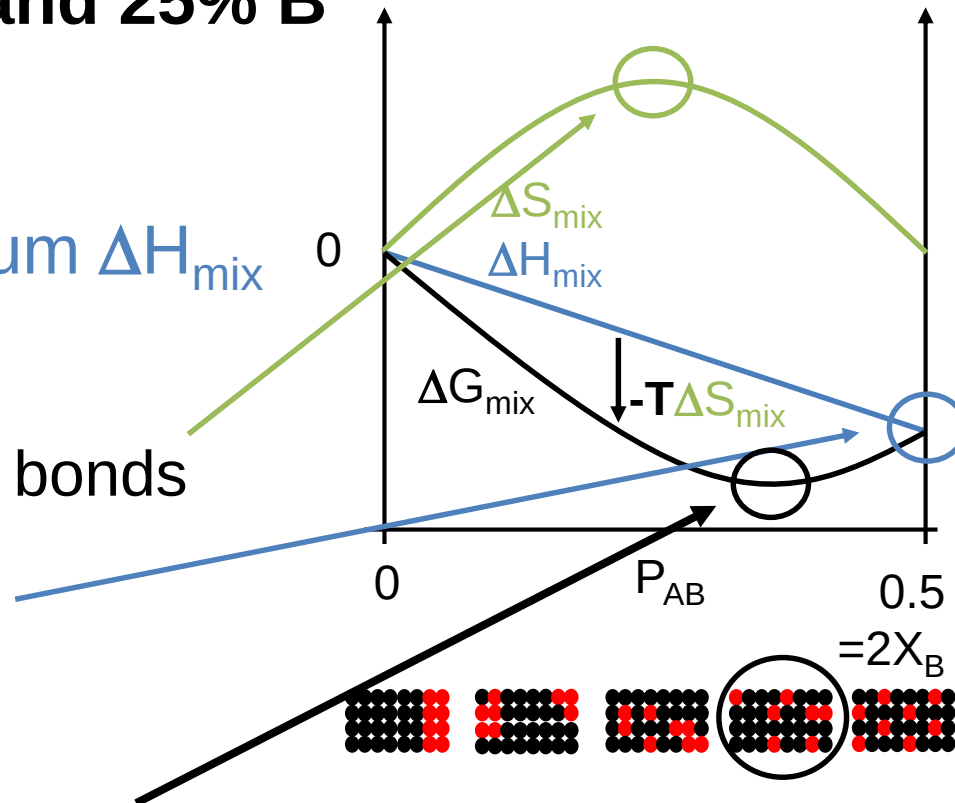
$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}}$$

- ΔG_{mix} minimizes with **minimum** ΔH_{mix} and **maximum** ΔS_{mix}

ΔS_{mix} maximizes when # of A-B bonds
 $= 2 \cdot X_A \cdot X_B$

ΔH_{mix} minimizes with **maximum**
 number of A-B bonds

ΔG_{mix} minimizes between $P_{\text{AB,random}}$ and $P_{\text{AB,max}}!$

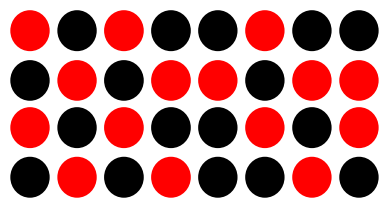


Strategy:

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}}$$

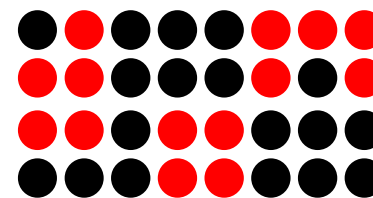
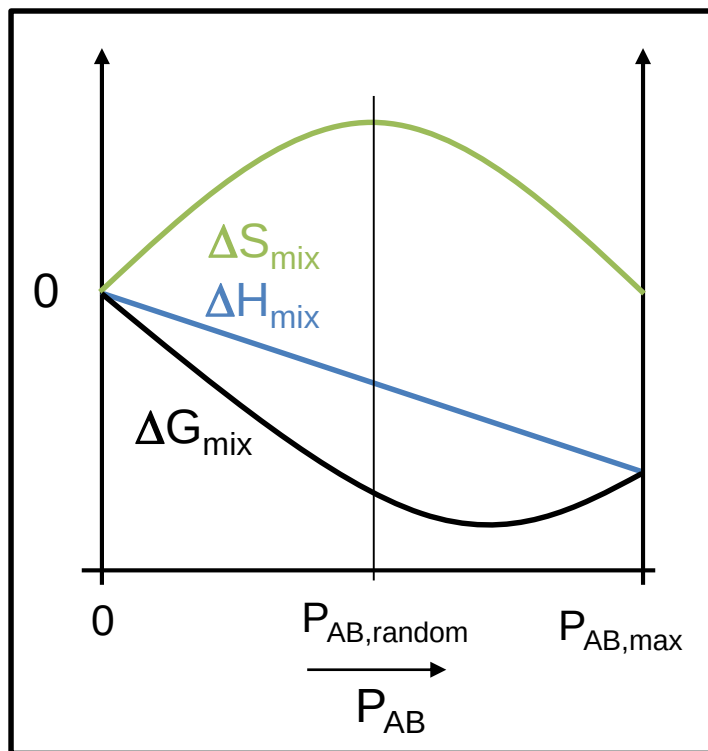
Think about **bonds** & **configurations**

REAL SOLUTIONS



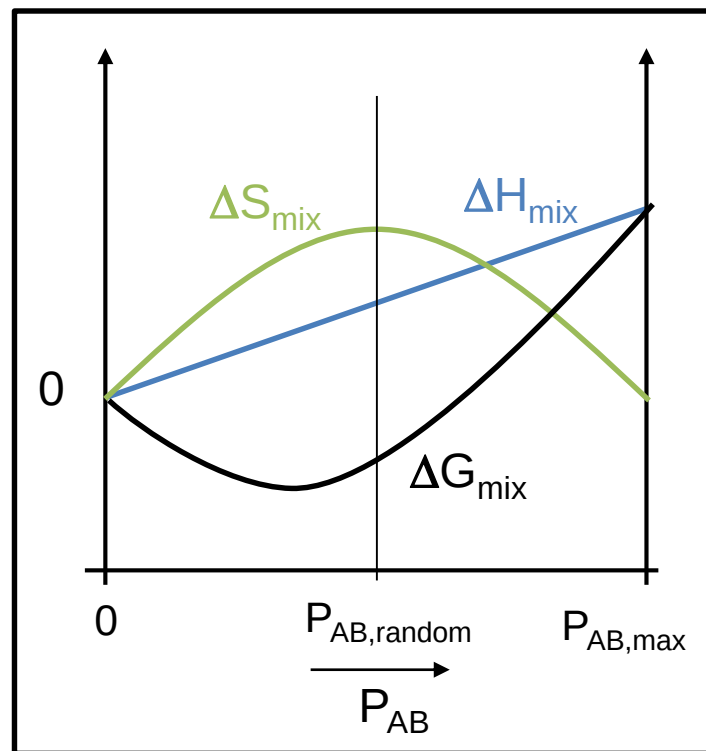
$\Omega < 0$

Ordering

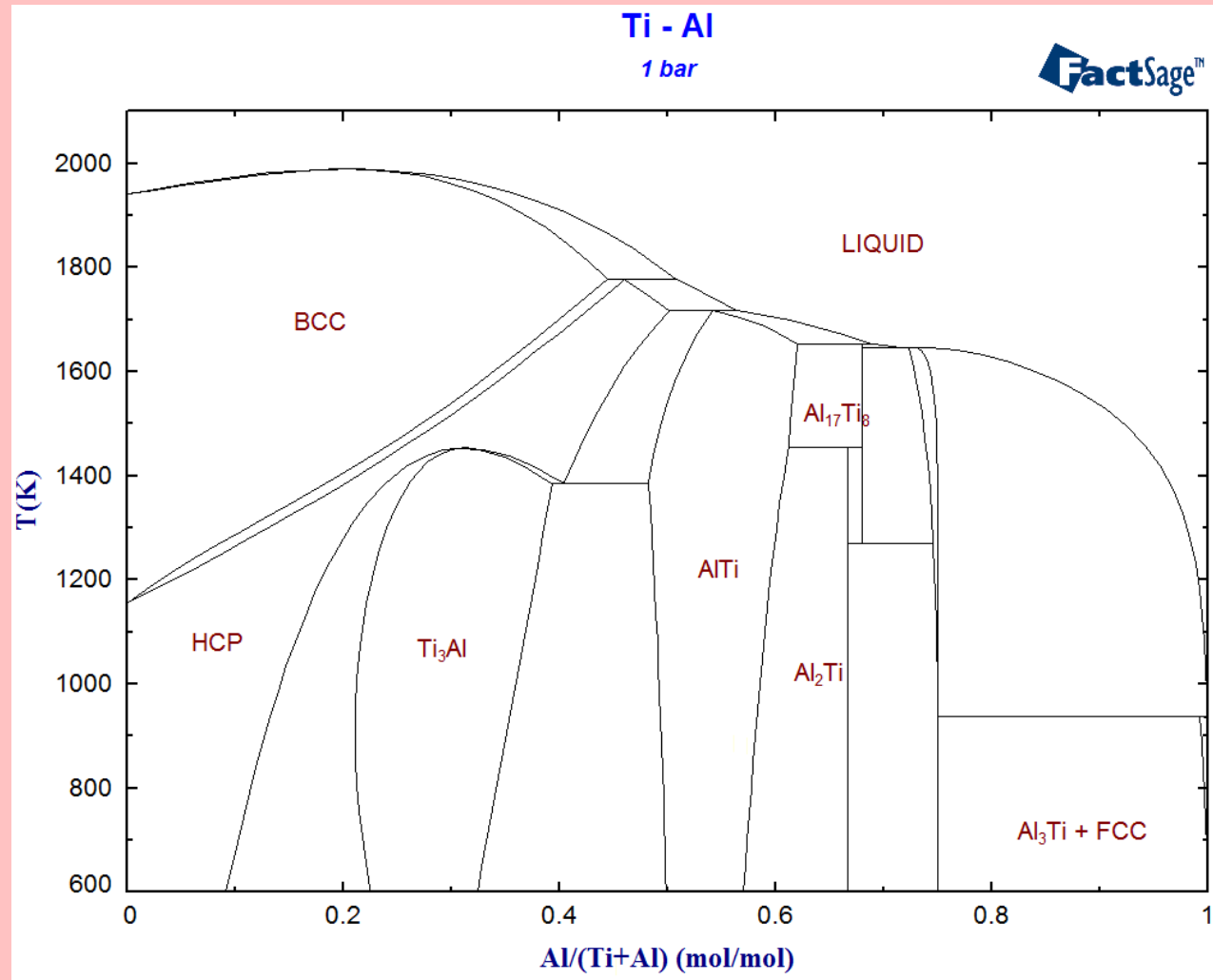
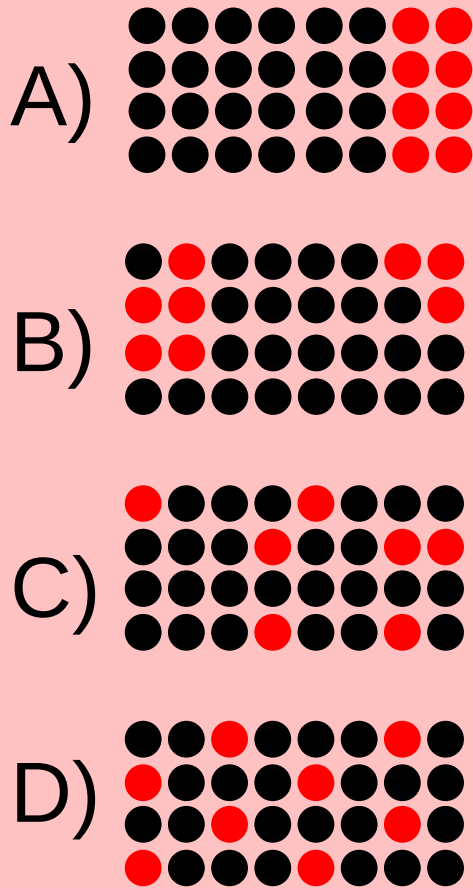


$\Omega > 0$

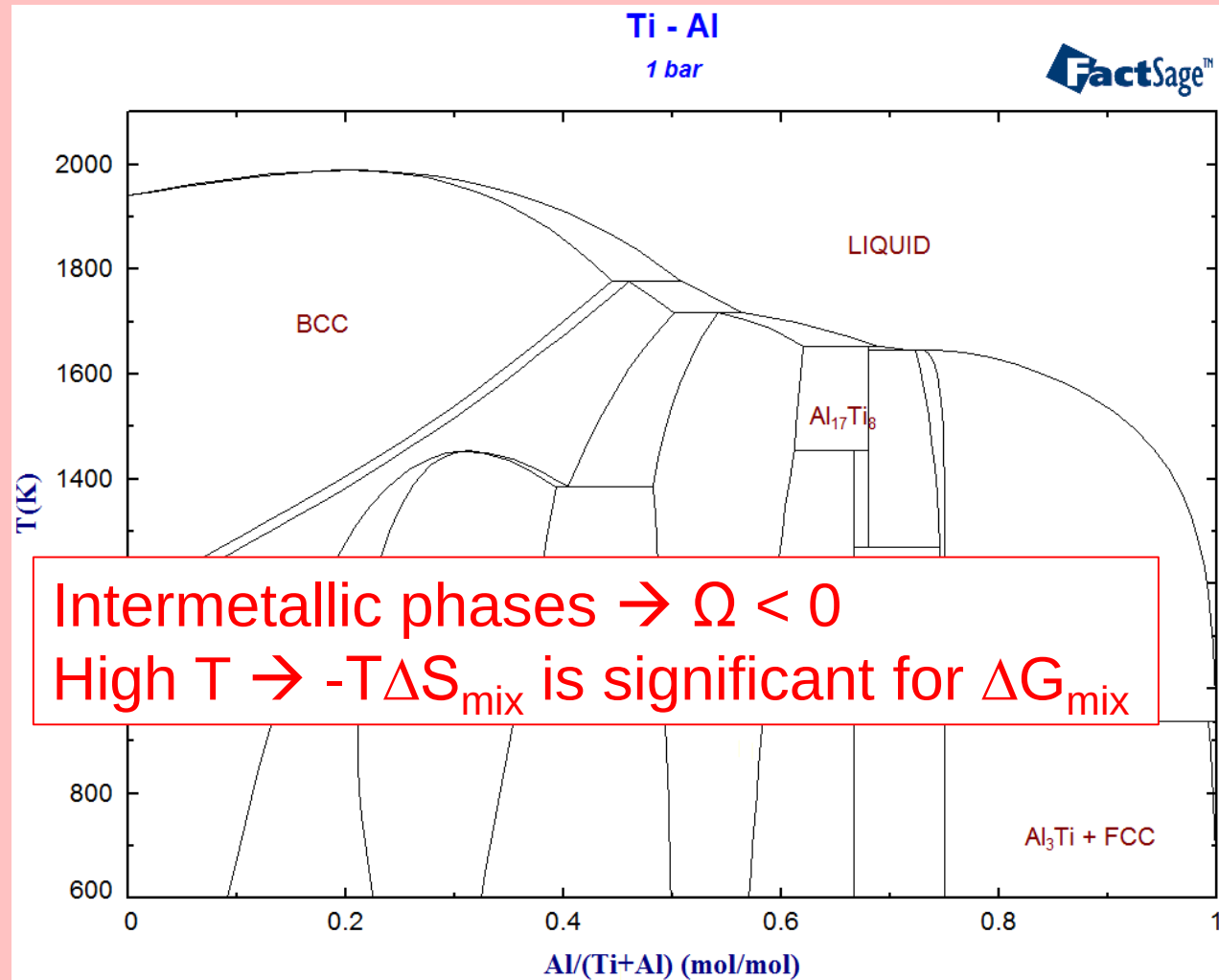
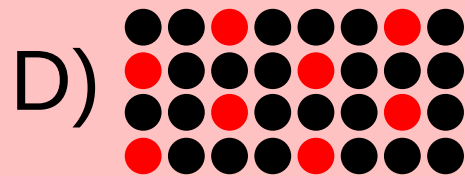
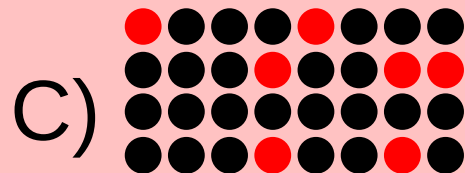
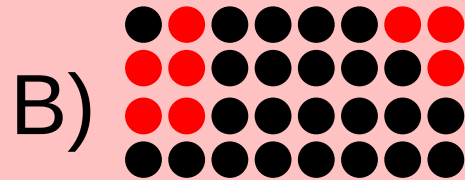
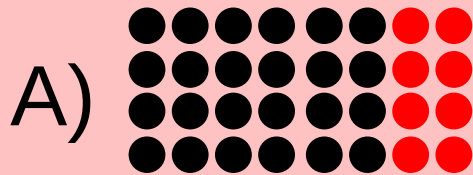
Clustering



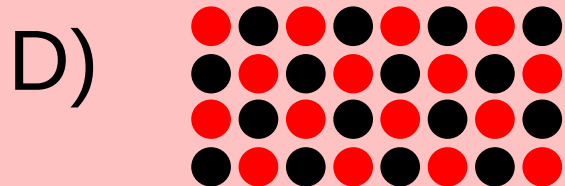
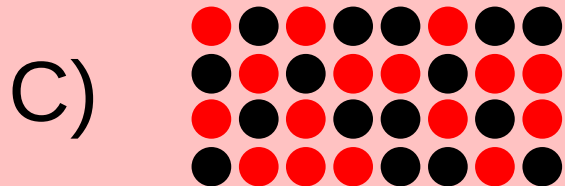
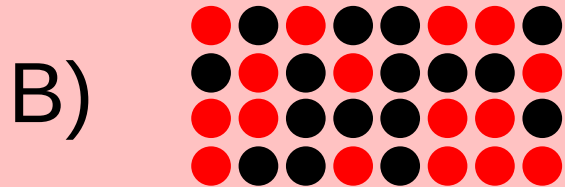
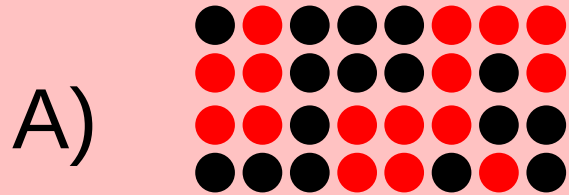
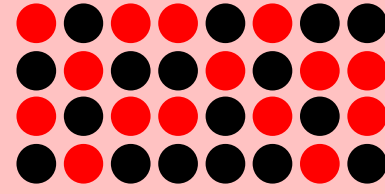
What could be a sensible atomic arrangement
for BCC-Ti_{0.75}Al_{0.25} at 1800K?



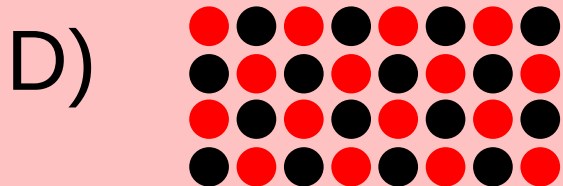
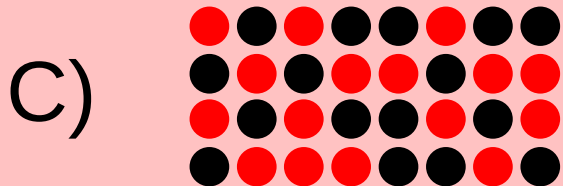
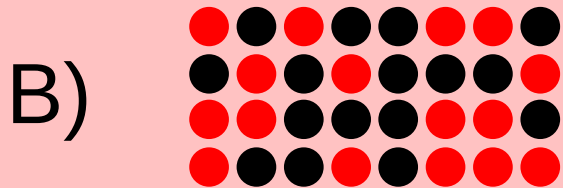
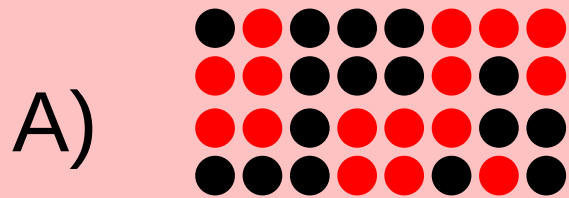
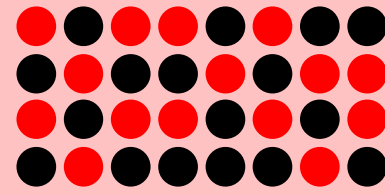
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The following atomic arrangement is observed for an alloy at 1500K. What could be a sensible atomic arrangement at 300K?



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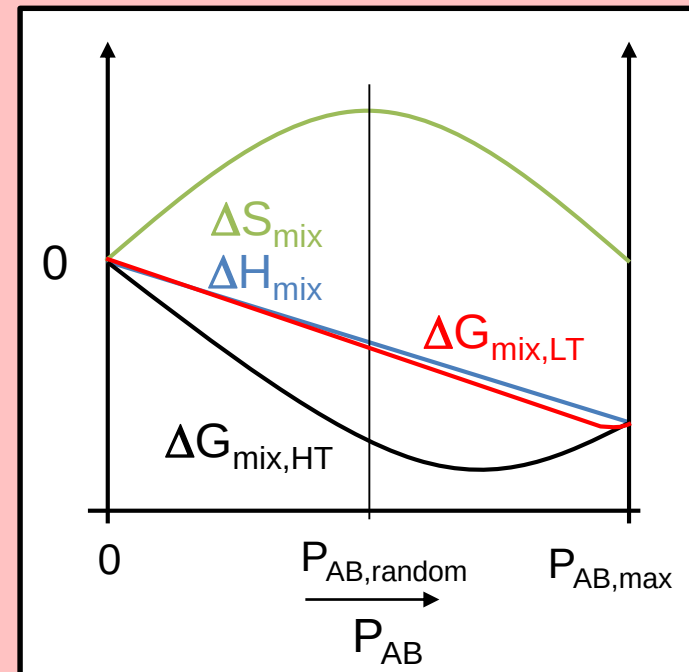
Ordering ($P_{AB} > P_{AB,random}$)

→ $\Omega < 0$

Lower T

→ $-T\Delta S_{mix}$ less significant for ΔG_{mix}

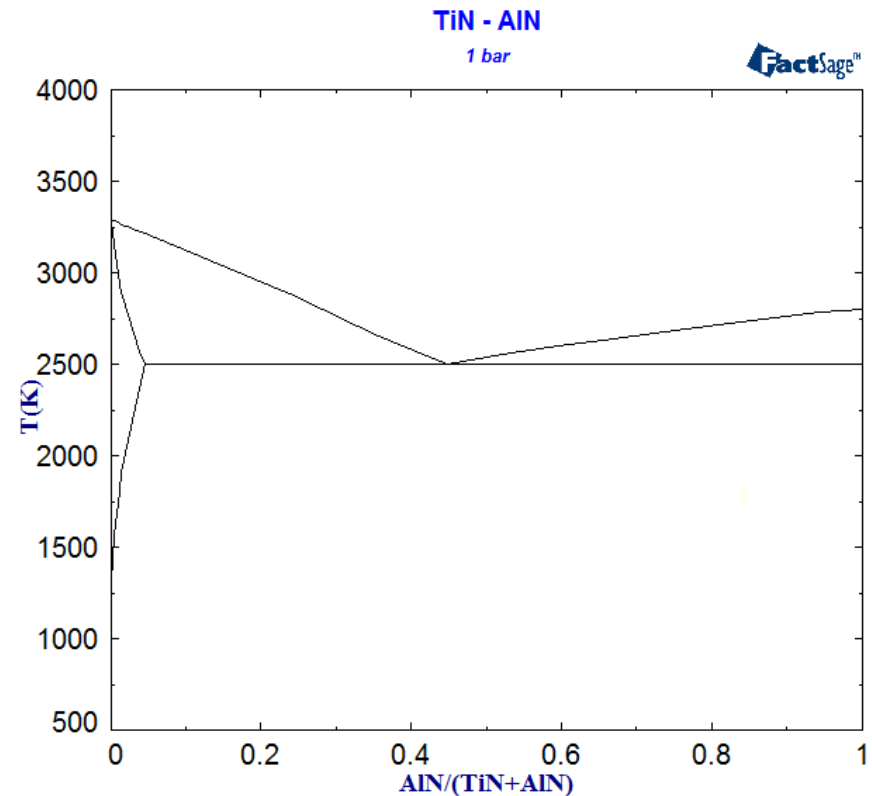
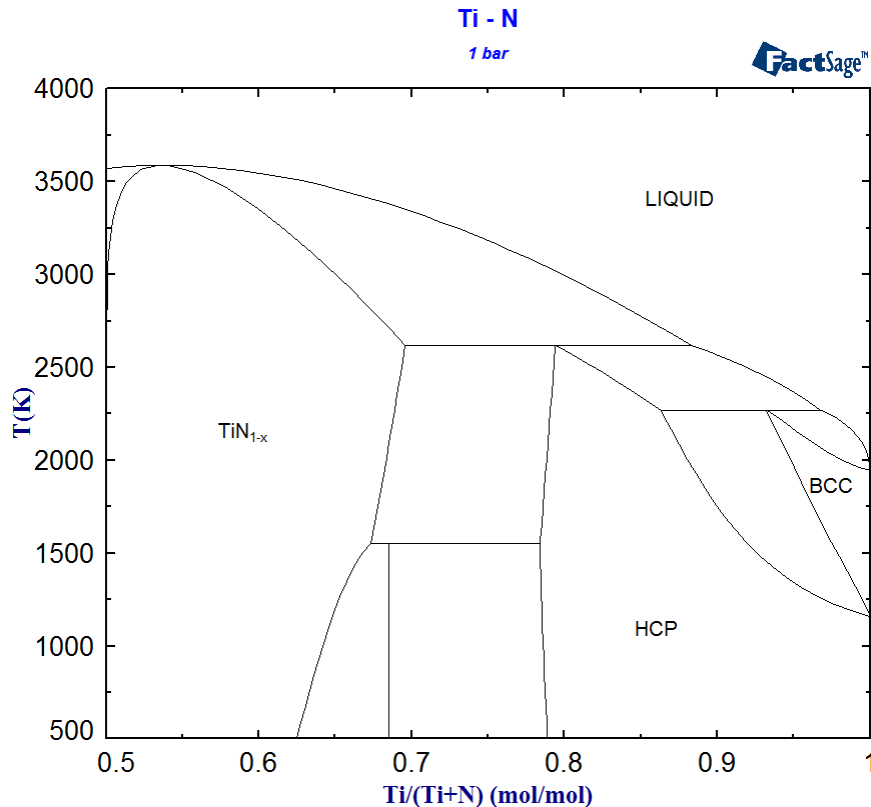
→ ΔH_{mix} minimization!



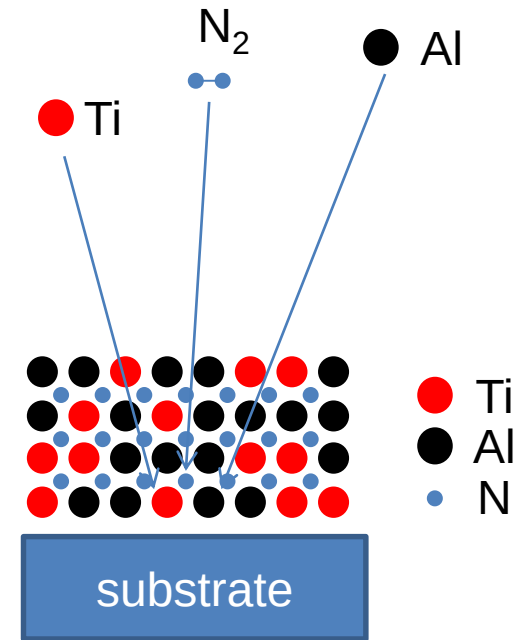
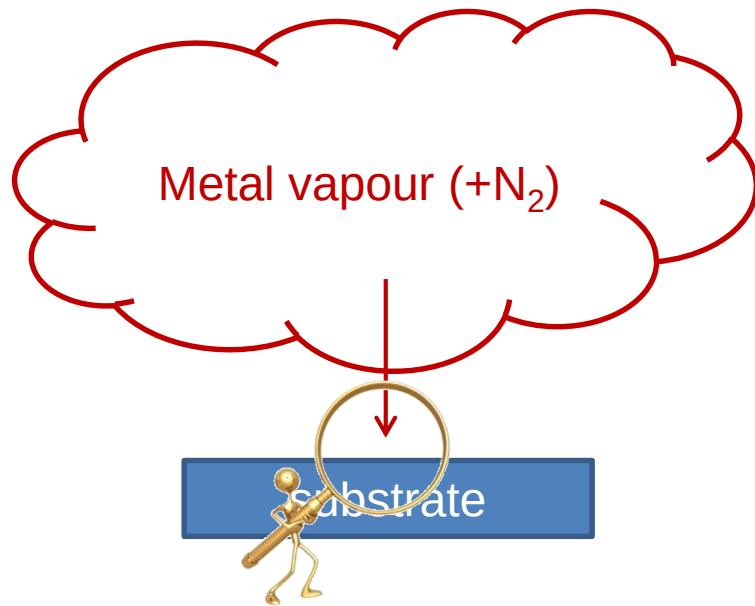
Application: (Ti,Al)N coatings for cutting tools

State of the art for protective coatings on cutting tools :
1980 - 2000 TiN
Since ~2000 (Ti,Al)N coatings

WHY?

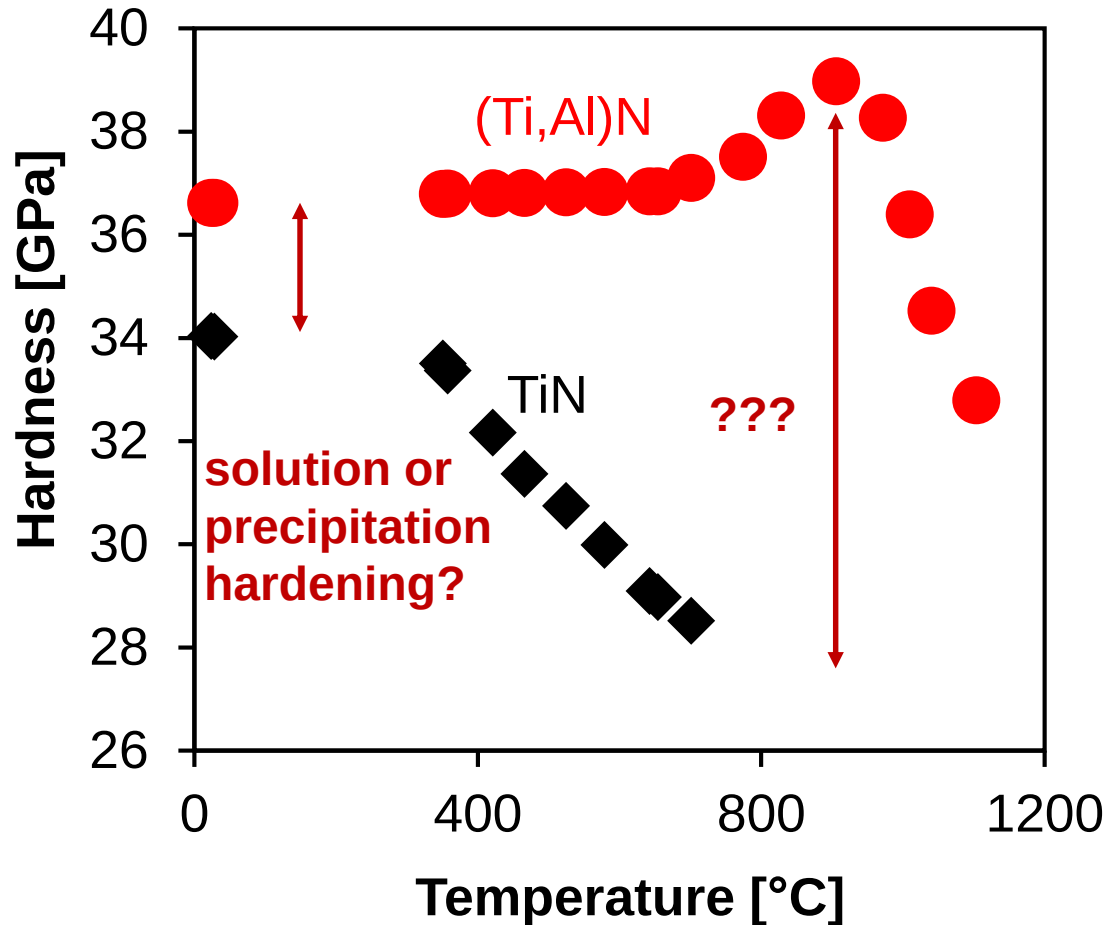


Vapour phase condensation



From metal vapour to solid within a fraction of 1 μs
→ Extreme quenching rates ($\gg 10^{10} \text{ }^\circ\text{C/s}$)!

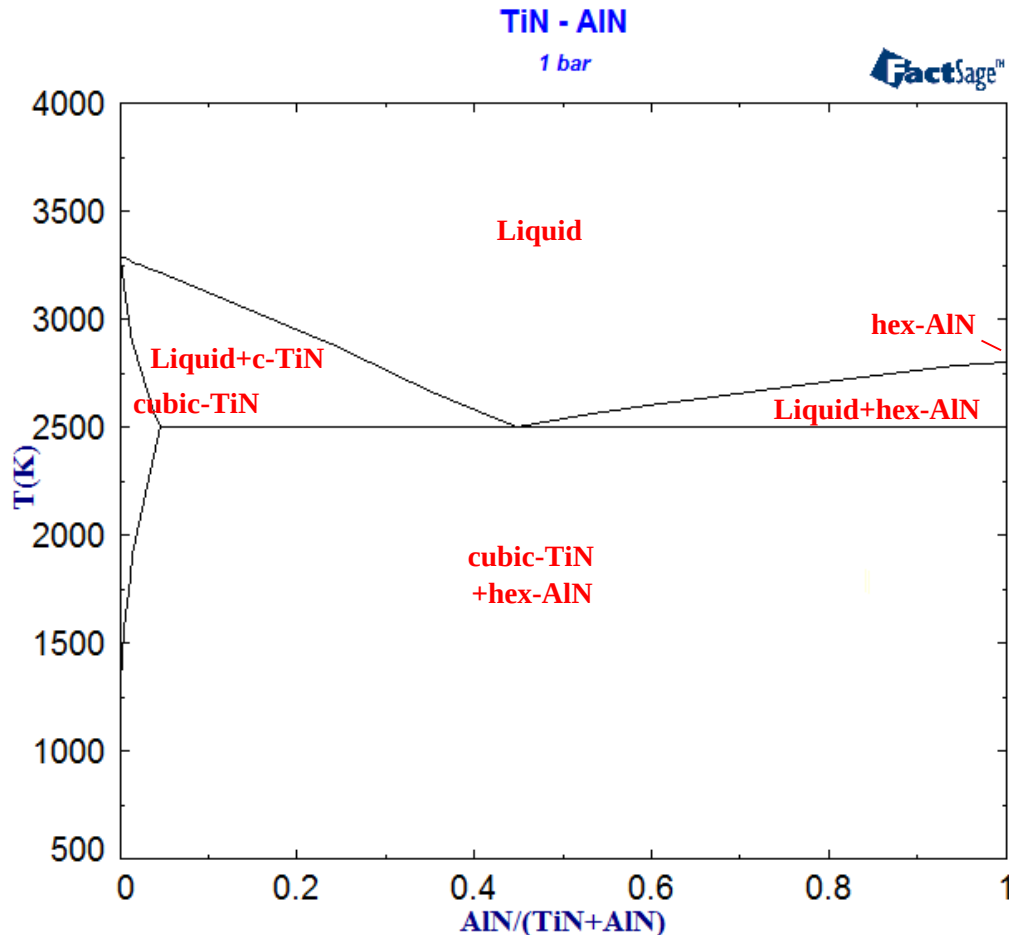
Application: (Ti,Al)N coatings for cutting tools



H increases by Al addition!

But WHY?

Vapour phase condensation

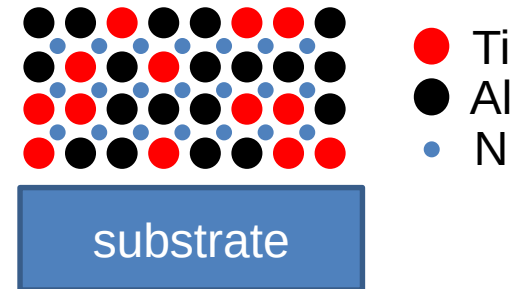


Atoms cannot form two phases
TiN+AlN because of limited mobility
(non-equilibrium processing).

What do we learn from the phase
diagram?

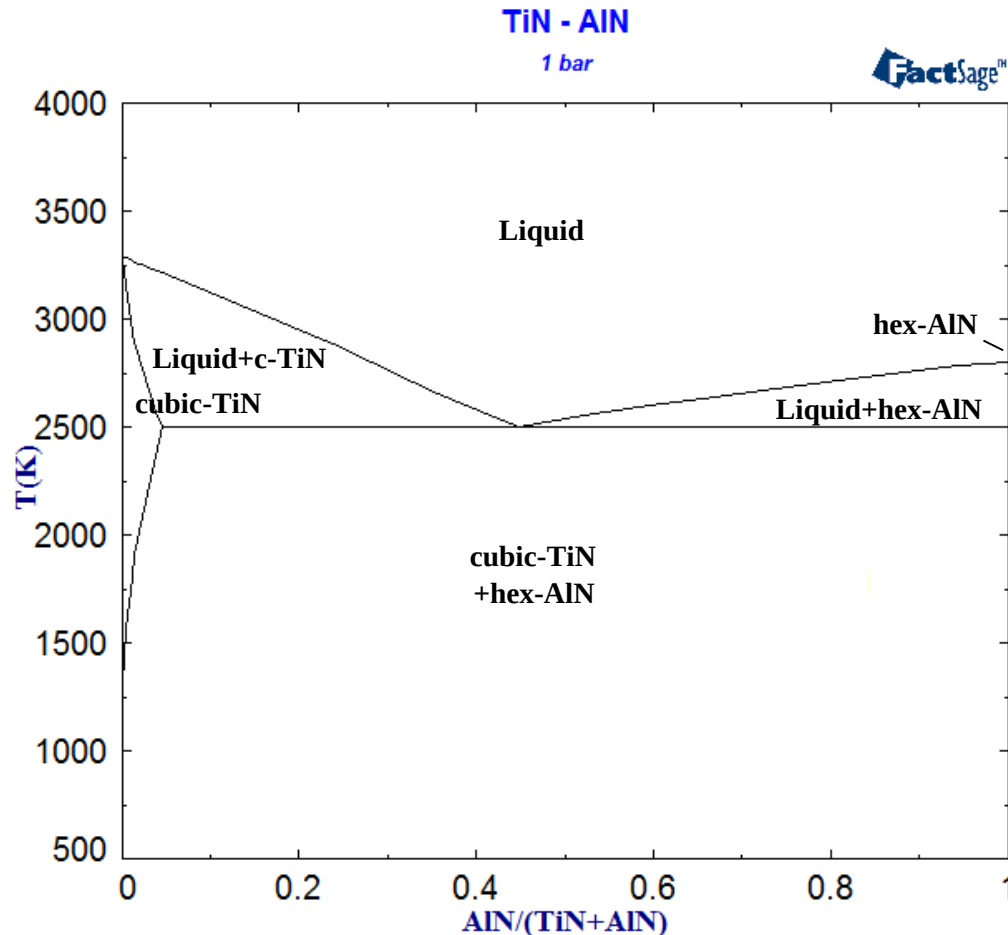
NOTHING AT ALL!?

Wait: Please sketch the $G(x)$
curves at $T = 250^\circ\text{C}$.



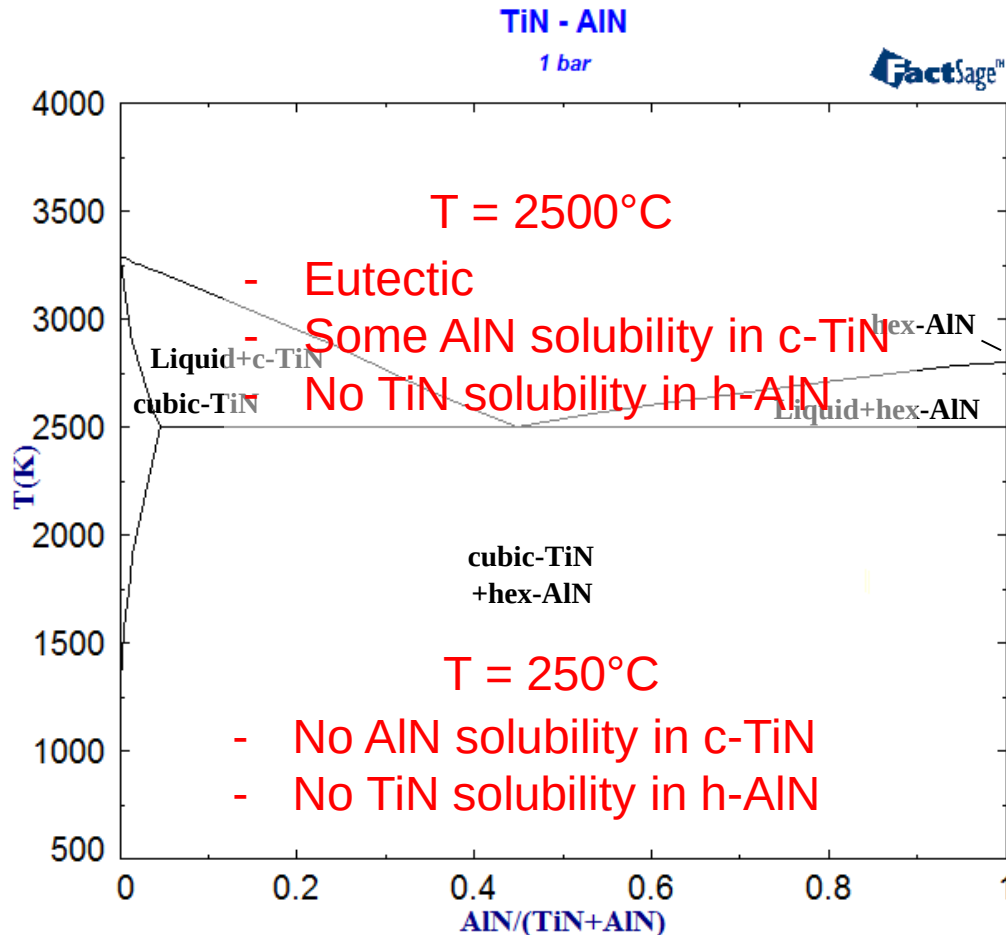
From metal vapour to solid within a fraction of $1\ \mu\text{s}$
→ Extreme quenching rates ($\gg 10^{10}\ ^\circ\text{C/s}$)!

Draw $G(x)$ @ 250°C and 2500°C



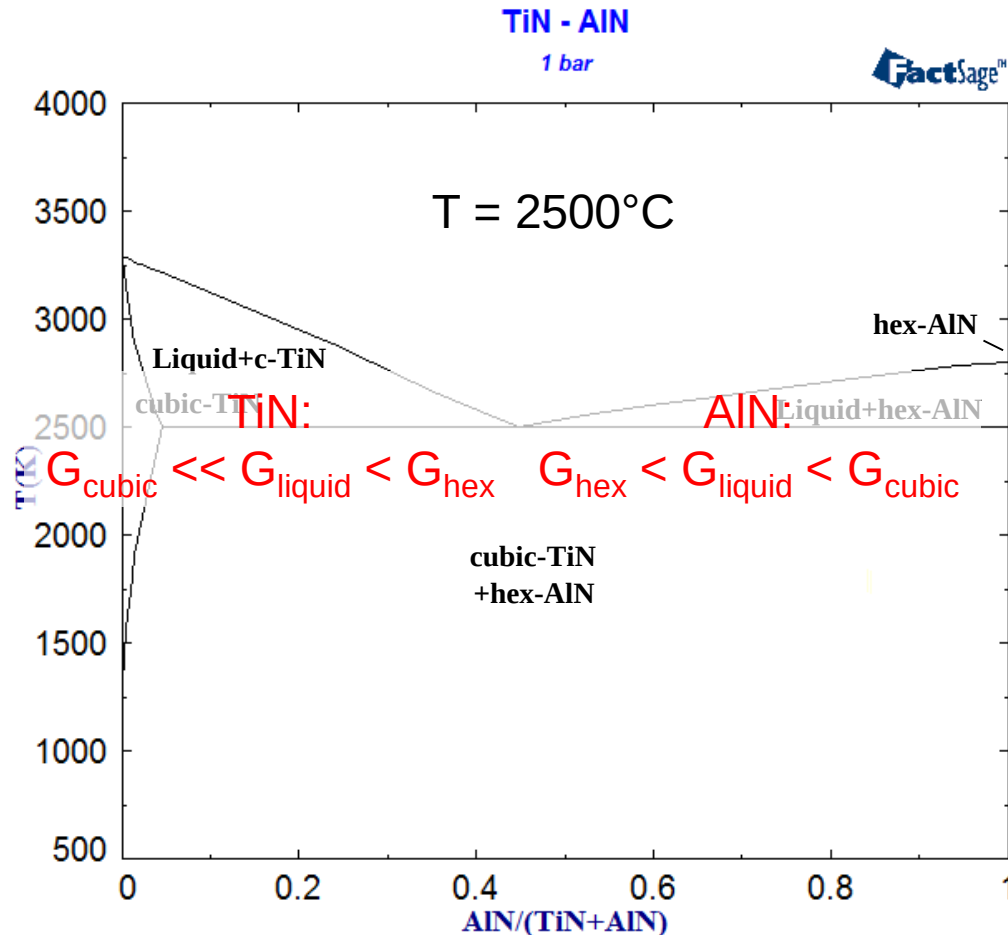
1. Choose the temperature at which you find more information in the phase diagram!
2. Order the Gibbs energy of the pure components in the different phases.
3. Think about Ω for solid phases (cubic and hex): Do you expect $\Omega_{c/h} < 0$ or $\Omega_{c/h} > 0$? If you cannot judge Ω for one phase, assume $\Omega_c = \Omega_h$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
5. Draw ΔH_{mix} , $-T\Delta S_{\text{mix}}$ and ΔG_{mix} for all phases. Assume $\Delta H_{\text{mix}}(\text{liquid}) \approx 0$.
6. Draw $G(x)$ for the solid phases.
7. Draw $G(x)$ for the liquid phase, taking into account position of the eutectic. Eventually adjust $G(x)$ for the solid phases to match solubility limits.
8. Repeat the steps for the other temperature.

Draw $G(x)$ @ 250°C and 2500°C



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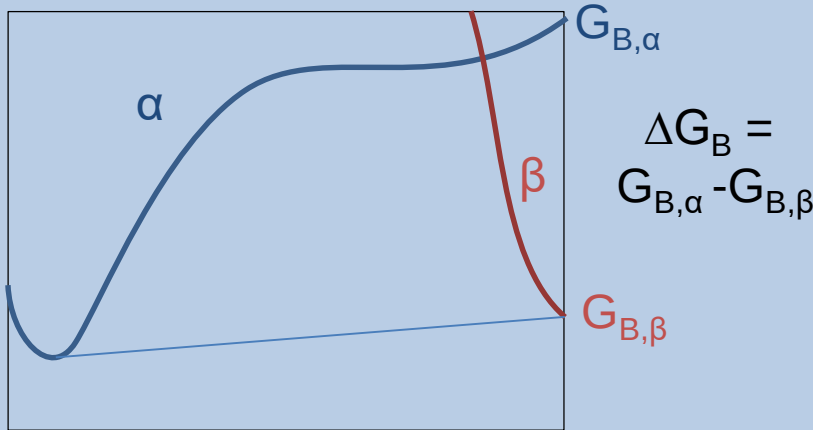
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TiN - AlN



$$X_{\text{solubility}} = \exp \left\{ -\frac{\Delta G_B + \Omega}{RT} \right\}$$

small solubility limit $\rightarrow$ either ΔG_B or $\Omega > 0$
 virtually no solubility limit $\rightarrow$ both ΔG_B or $\Omega > 0$
 $\rightarrow \Omega_{\text{cubic}}$ **or** $\Delta G_{\text{AlN}} > 0$
 $\rightarrow \Omega_{\text{hex}}$ **and** $\Delta G_{\text{TiN}} > 0$

TiN:

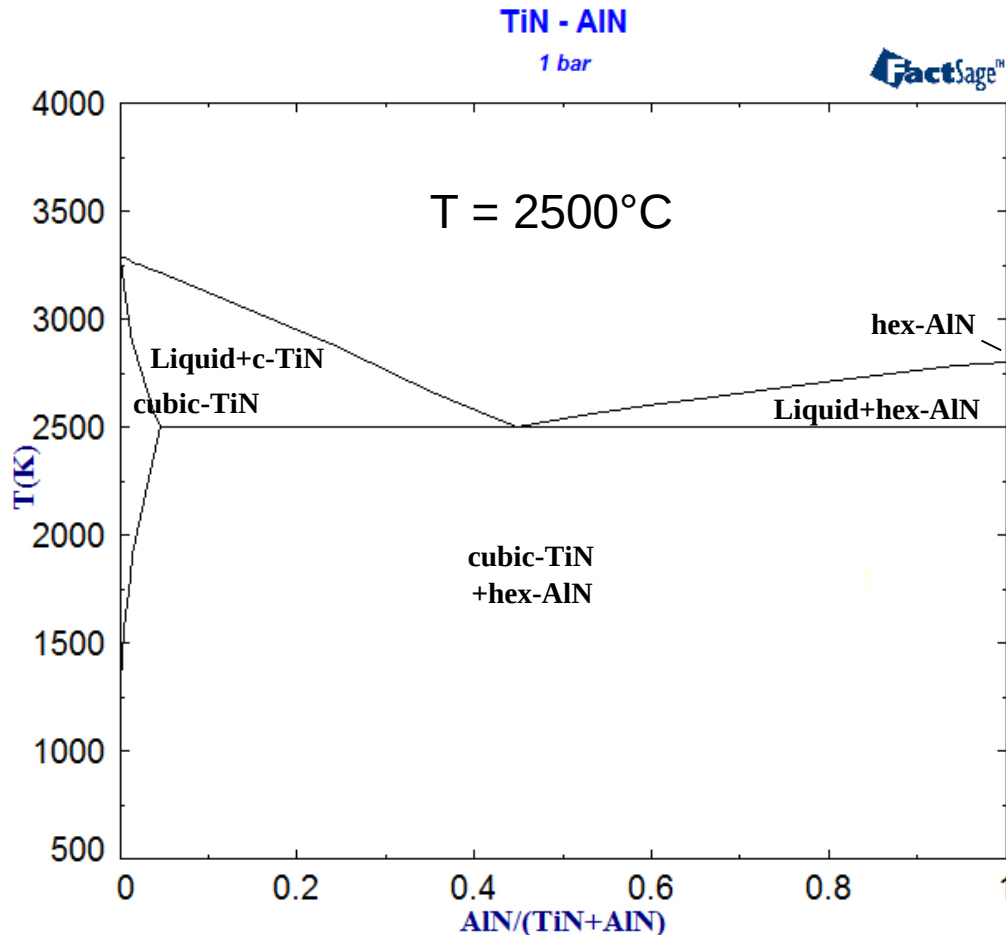
$\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$
 $\Delta G_{\text{TiN}} > \Delta G_{\text{AlN}}$

AlN:

$G_{\text{hex}} < G_{\text{liquid}} < G_{\text{cubic}}$

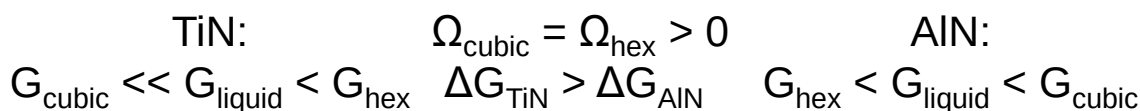
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Draw $G(x)$ @ 250°C and 2500°C

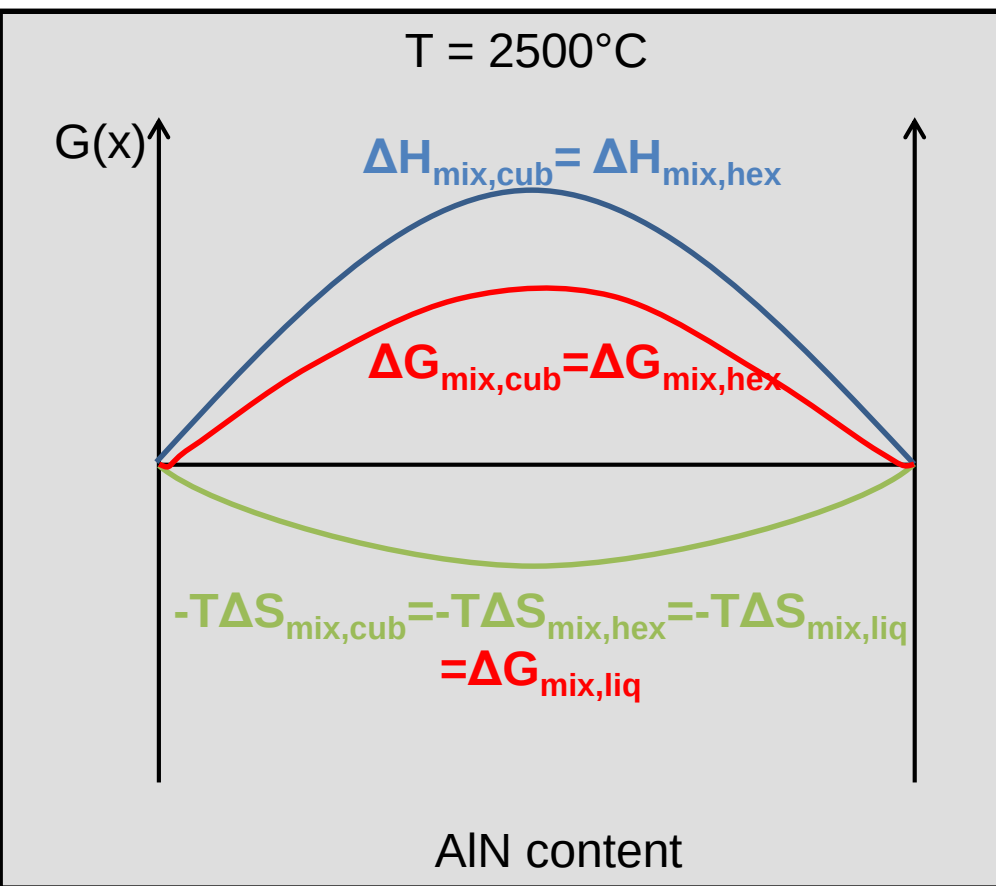


1. Choose the temperature at which you find more information in the phase diagram!
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8. Repeat the steps for the other temperature.

Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$

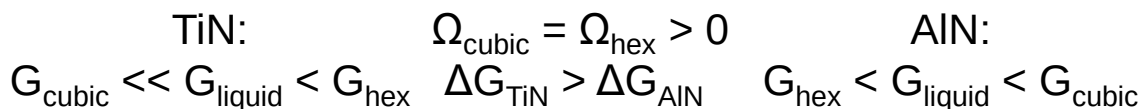


Draw $G(x)$ @ 250°C and 2500°C

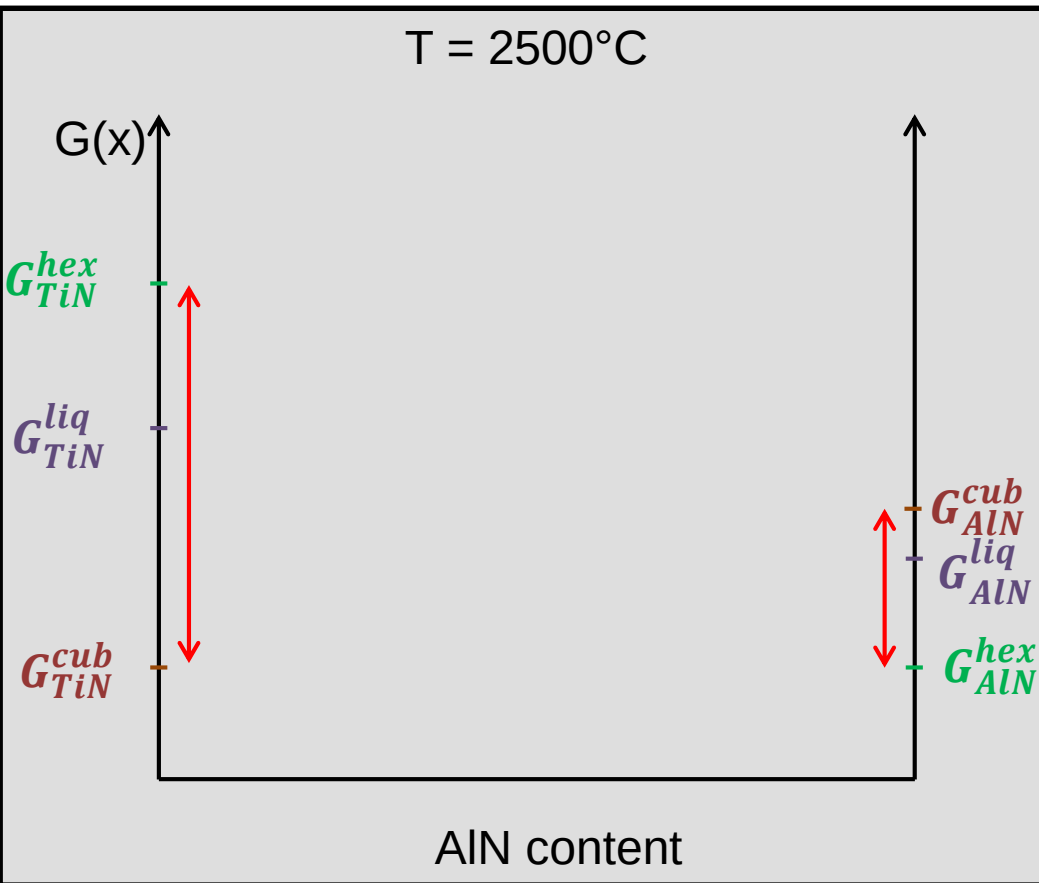


Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$

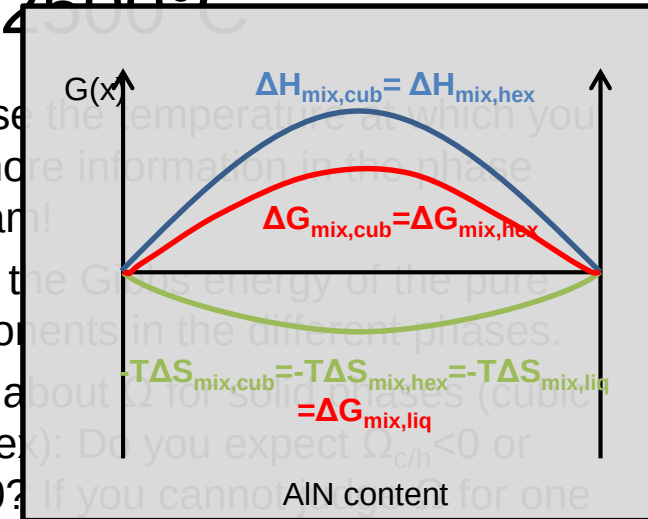
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Draw $G(x)$ @ 250°C and 2500°C



Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$



1. Choose the temperature at which you find more information in the phase diagram!
2. Order the components in the different phases.
3. Think about the entropy of mixing and heat of mixing: Do you expect $\Omega_{\text{c/h}} < 0$ or $\Omega_{\text{c/h}} > 0$? If you cannot decide for one phase, assume $\Omega_{\text{c}} = \Omega_{\text{h}}$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
5. Draw ΔH_{mix} , $-T\Delta S_{\text{mix}}$ and ΔG_{mix} for all phases. Assume $\Delta H_{\text{mix}}(\text{liquid}) \approx 0$.
6. Draw $G(x)$ for the solid phases.
7. Draw $G(x)$ for the liquid phase, taking into account position of the eutectic. Eventually adjust $G(x)$ for the solid phases to match solubility limits.
8. Repeat the steps for the other temperature.

TiN:

$$G_{\text{cubic}} \ll G_{\text{liquid}} < G_{\text{hex}}$$

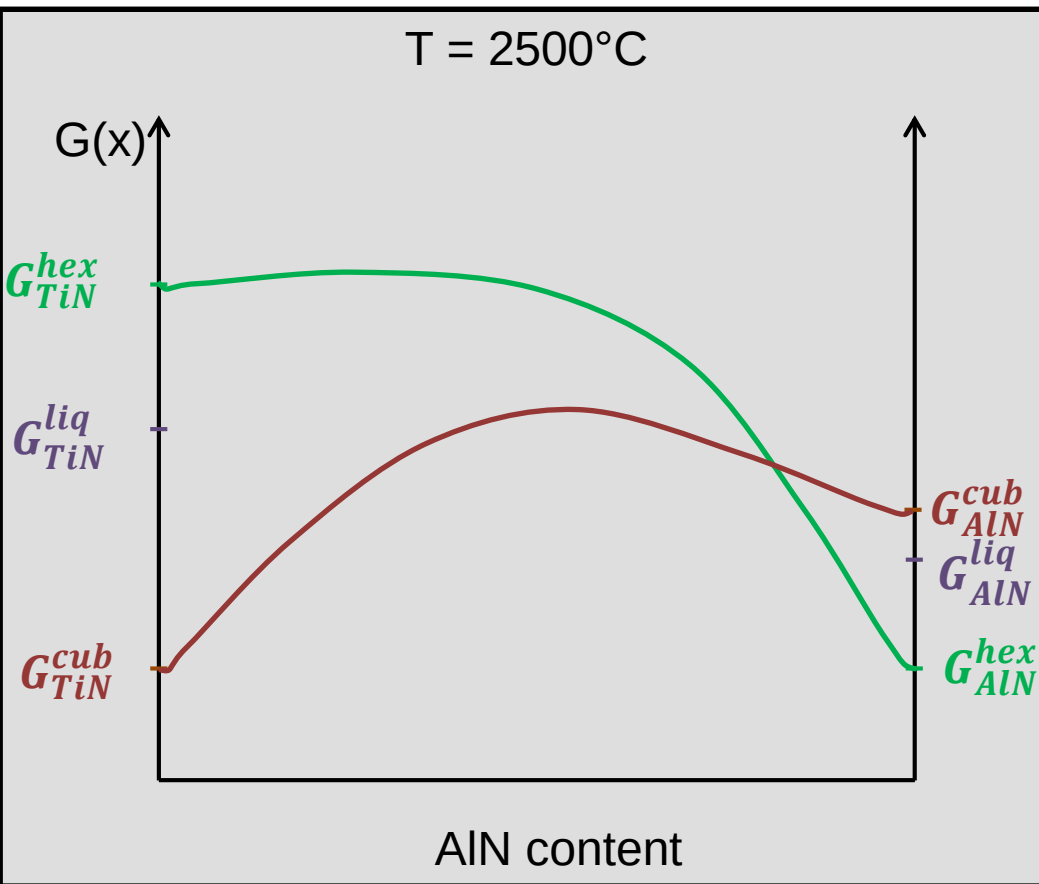
$\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$

$$\Delta G_{\text{TiN}} > \Delta G_{\text{AlN}}$$

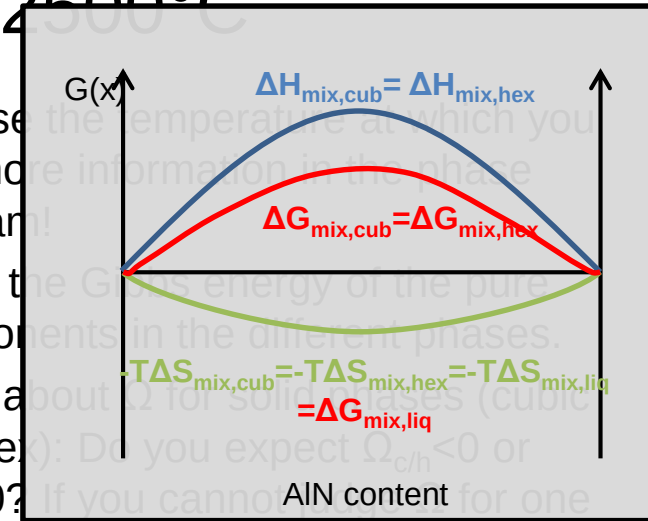
AlN:

$$G_{\text{hex}} < G_{\text{liquid}} < G_{\text{cubic}}$$

Draw $G(x)$ @ 250°C and 2500°C



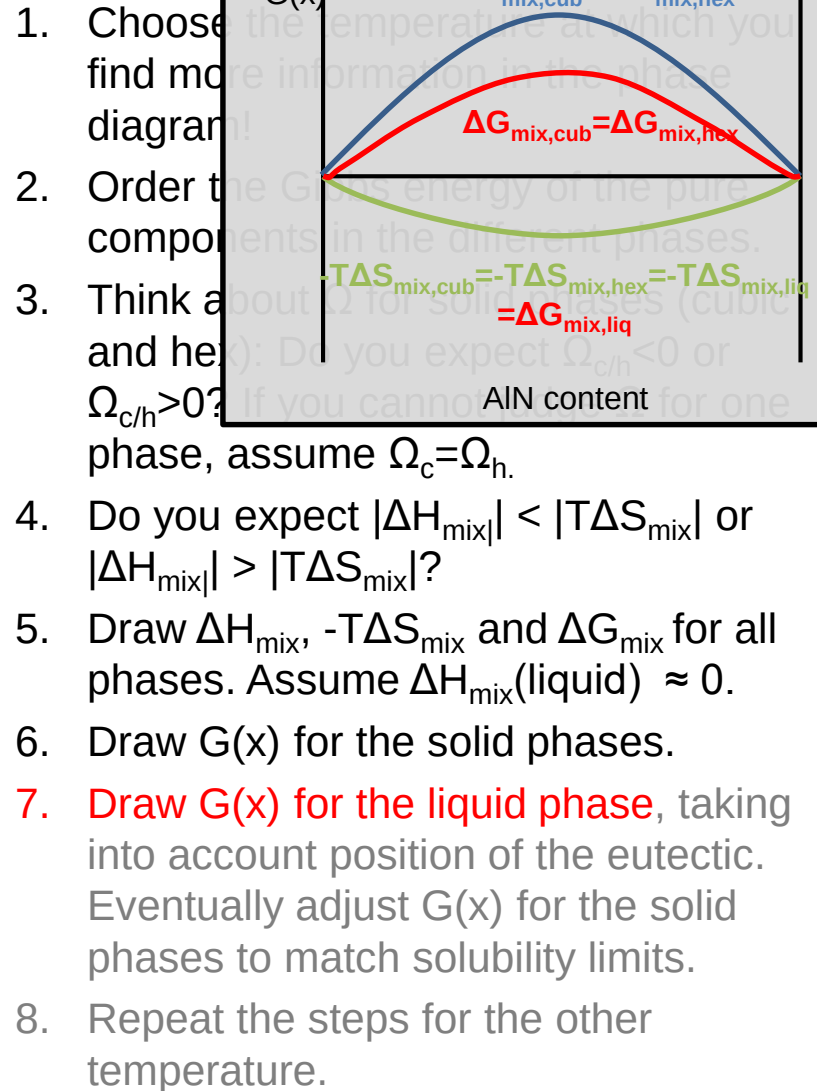
Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$

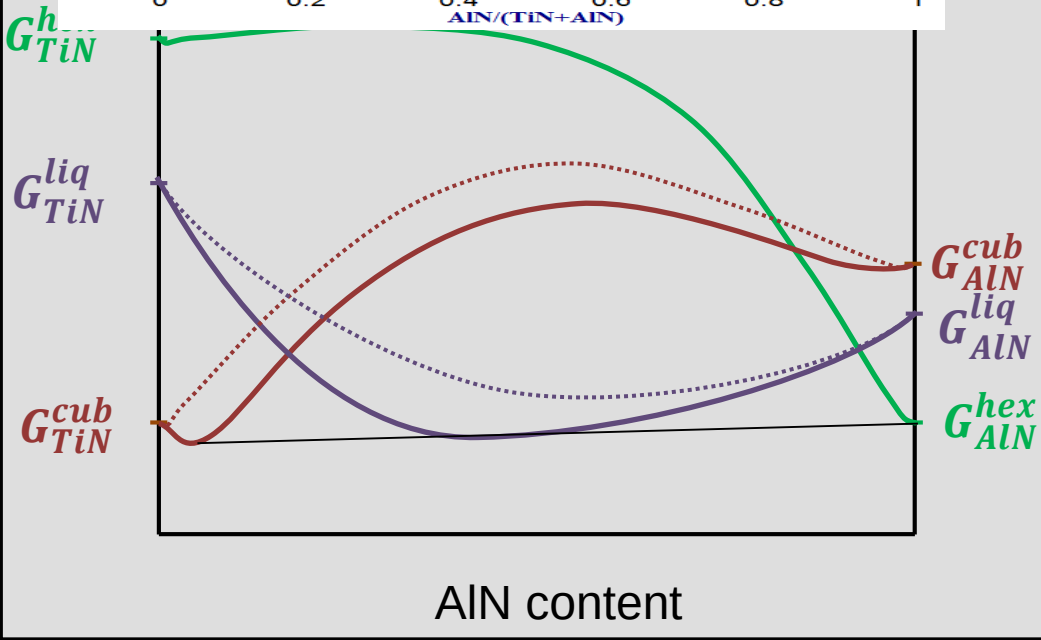
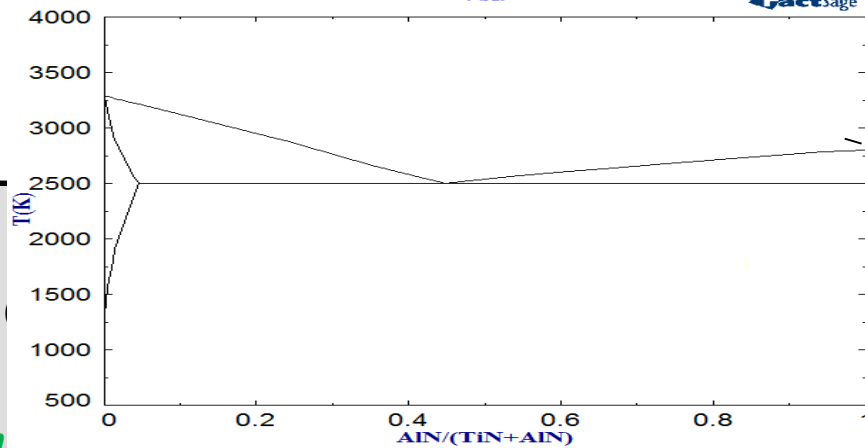


1. Choose the temperature at which you find more information in the phase diagram!
2. Order the components in the different phases.
3. Think about the phase and hexagonal phase, assume $\Omega_{\text{c/h}} > 0$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
5. Draw ΔH_{mix} , $-T\Delta S_{\text{mix}}$ and ΔG_{mix} for all phases. Assume $\Delta H_{\text{mix}}(\text{liquid}) \approx 0$.
6. Draw $G(x)$ for the solid phases.
7. Draw $G(x)$ for the liquid phase, taking into account position of the eutectic. Eventually adjust $G(x)$ for the solid phases to match solubility limits.
8. Repeat the steps for the other temperature.

TiN: $\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$ AIN: $\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$

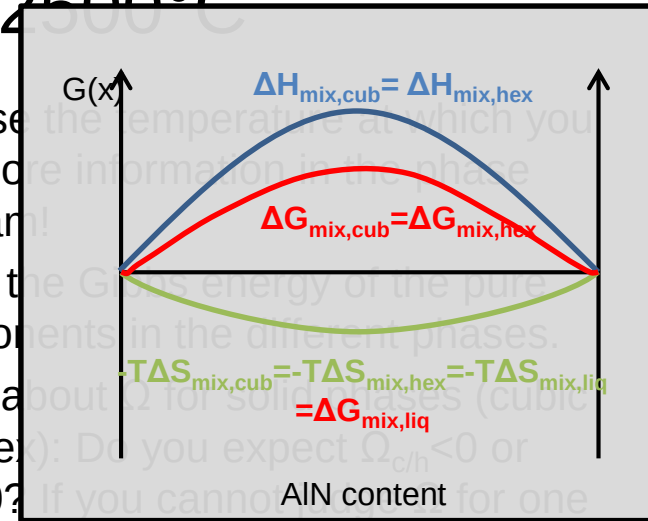
$G_{\text{cubic}} \ll G_{\text{liquid}} < G_{\text{hex}}$ $\Delta G_{\text{TiN}} > \Delta G_{\text{AlN}}$ $G_{\text{hex}} < G_{\text{liquid}} < G_{\text{cubic}}$

[illegible]
$$\begin{array}{ccc} \text{TiN:} & \Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0 & \text{AlN:} \\ G_{\text{cubic}} \ll G_{\text{liquid}} < G_{\text{hex}} & \Delta G_{\text{TiN}} > \Delta G_{\text{AlN}} & G_{\text{hex}} < G_{\text{liquid}} < G_{\text{cubic}} \end{array}$$



Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$

50°C and 2500°C



1. Choose the temperature at which you find more information in the phase diagram!
2. Order the components in the different phases.
3. Think about the relative magnitudes of ΔH_{mix} and $T\Delta S_{\text{mix}}$ for the different phases. Do you expect $\Omega_{\text{c/h}} < 0$ or $\Omega_{\text{c/h}} > 0$? If you cannot decide for one phase, assume $\Omega_{\text{c}} = \Omega_{\text{h}}$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
5. Draw ΔH_{mix} , $-T\Delta S_{\text{mix}}$ and ΔG_{mix} for all phases. Assume $\Delta H_{\text{mix}}(\text{liquid}) \approx 0$.
6. Draw $G(x)$ for the solid phases.
7. Draw $G(x)$ for the liquid phase, taking into account position of the eutectic. Eventually adjust $G(x)$ for the solid phases to match solubility limits.
8. Repeat the steps for the other temperature.

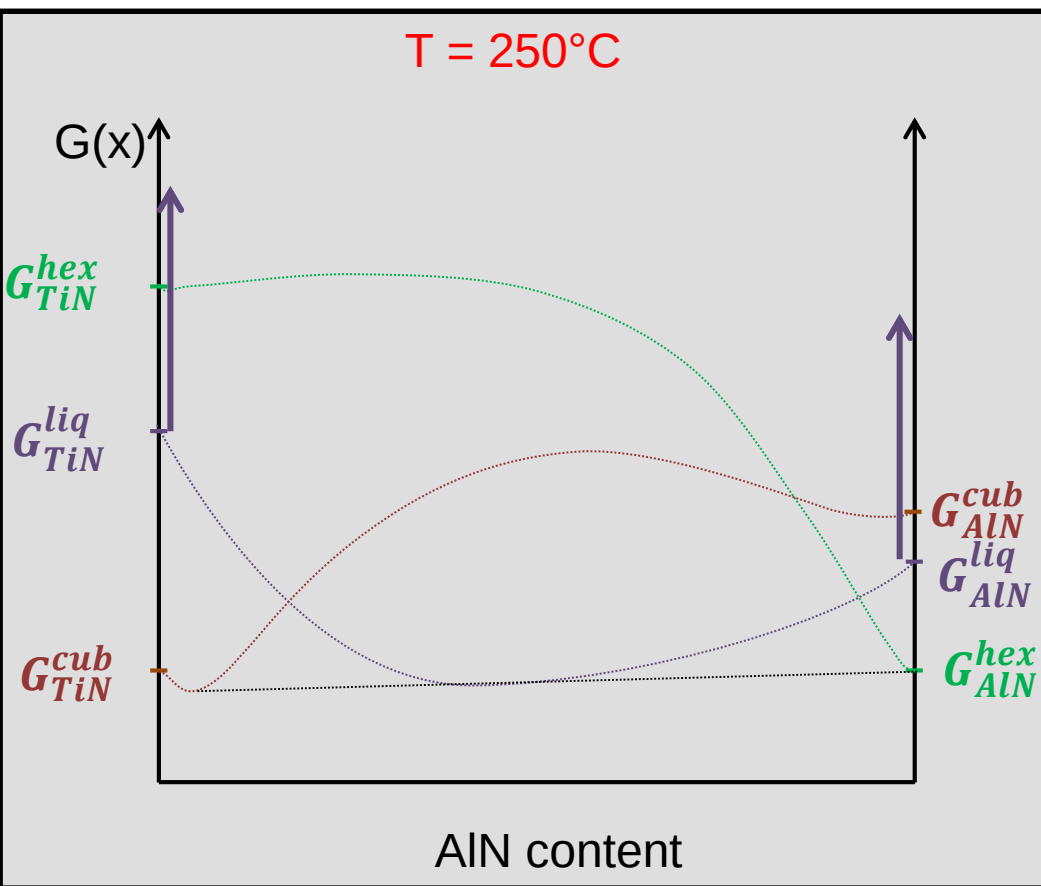
TiN:

$\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$

AlN:

$G_{\text{cubic}} \ll G_{\text{liquid}} < G_{\text{hex}}$ $\Delta G_{\text{TiN}} > \Delta G_{\text{AlN}}$ $G_{\text{hex}} < G_{\text{liquid}} < G_{\text{cubic}}$

Draw $G(x)$ @ 250°C and 2500°C



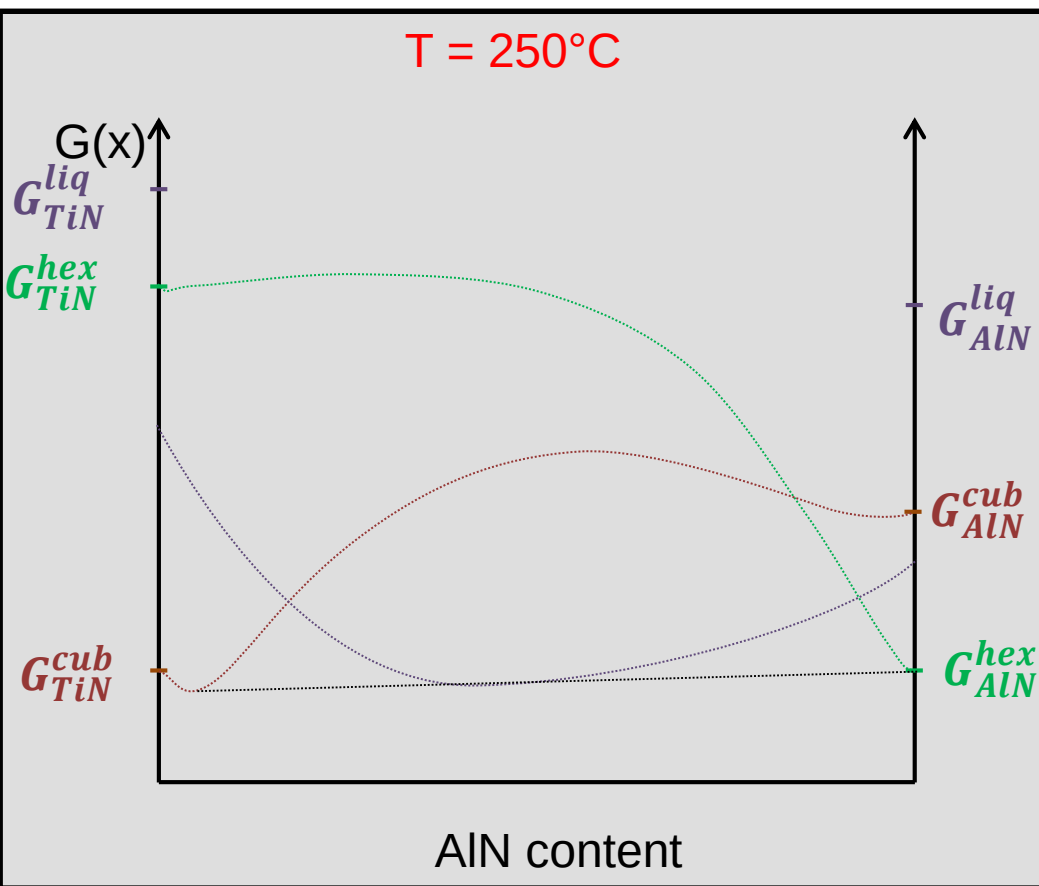
1. Choose the temperature at which you find more information in the phase diagram!
2. Order the Gibbs energy of the pure components in the different phases.
3. Think about Ω for solid phases (cubic and hex): Do you expect $\Omega_{c/h} < 0$ or $\Omega_{c/h} > 0$? If you cannot judge Ω for one phase, assume $\Omega_c = \Omega_h$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
5. Draw ΔH_{mix} , $-T\Delta S_{\text{mix}}$ and ΔG_{mix} for all phases. Assume $\Delta H_{\text{mix}}(\text{liquid}) \approx 0$.
6. Draw $G(x)$ for the solid phases.
7. Draw $G(x)$ for the liquid phase, taking into account position of the eutectic. Eventually adjust $G(x)$ for the solid phases to match solubility limits.

8. Repeat the steps for the other temperature.

Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$

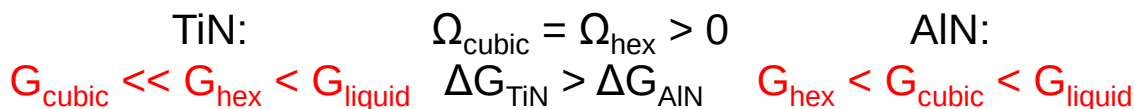
TiN:	$\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$	AlN:
$G_{\text{cubic}} \ll G_{\text{liquid}} < G_{\text{hex}}$	$\Delta G_{\text{TiN}} > \Delta G_{\text{AlN}}$	$G_{\text{hex}} < G_{\text{liquid}} < G_{\text{cubic}}$

Draw $G(x)$ @ 250°C and 2500°C

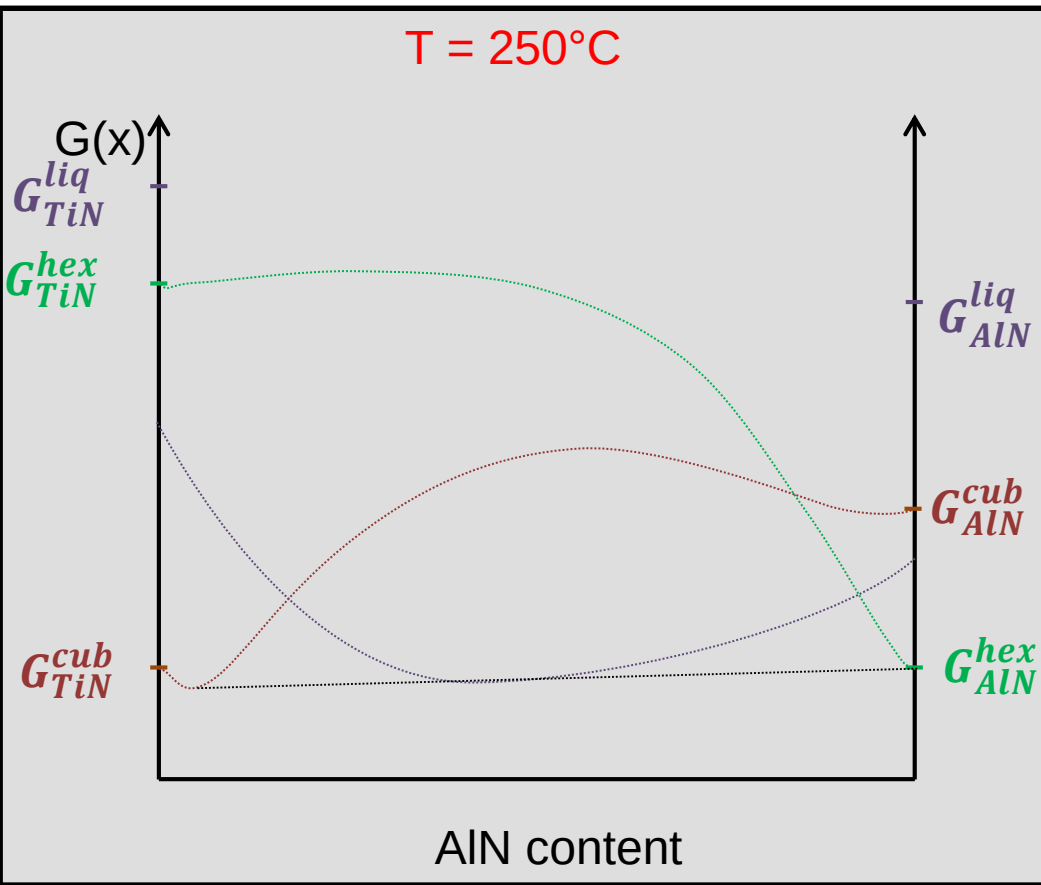


1. Choose the temperature at which you find more information in the phase diagram!
2. Order the Gibbs energy of the pure components in the different phases.
3. Think about Ω for solid phases (cubic and hex): Do you expect $\Omega_{c/h} < 0$ or $\Omega_{c/h} > 0$? If you cannot judge Ω for one phase, assume $\Omega_c = \Omega_h$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
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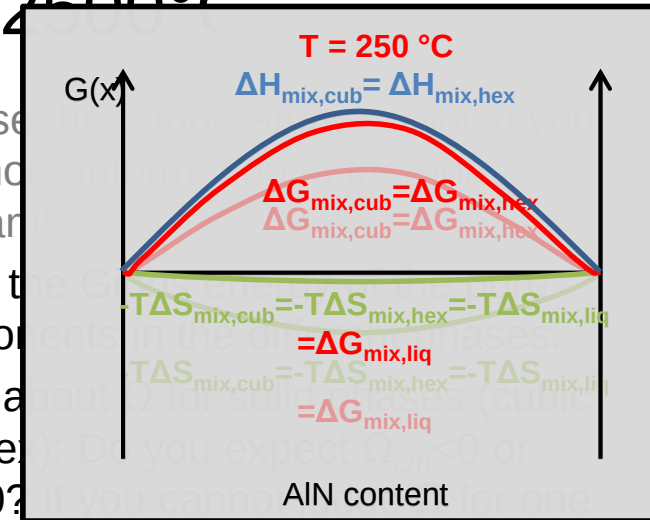
Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$



Draw $G(x)$ @ 250°C and 2500°C



Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$



1. Choose T and find ΔH_{mix} and ΔS_{mix} diagram.
2. Order the components in the diagram (cubic, hexagonal, liquid).
3. Think about the solubility and heat of mixing. Do you expect $\Omega_{\text{c/h}} > 0$? If you cannot decide for one phase, assume $\Omega_{\text{c}} = \Omega_{\text{h}}$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
5. Draw ΔH_{mix} , $-T\Delta S_{\text{mix}}$ and ΔG_{mix} for all phases. Assume $\Delta H_{\text{mix}}(\text{liquid}) \approx 0$.
6. Draw $G(x)$ for the solid phases.
7. Draw $G(x)$ for the liquid phase, taking into account position of the eutectic. Eventually adjust $G(x)$ for the solid phases to match solubility limits.
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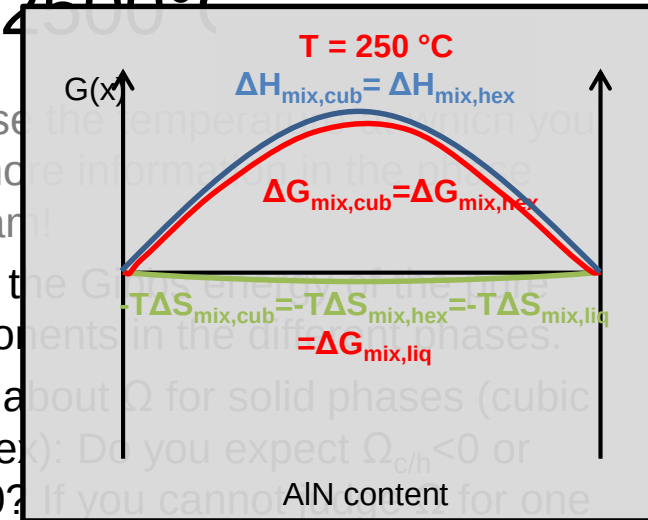
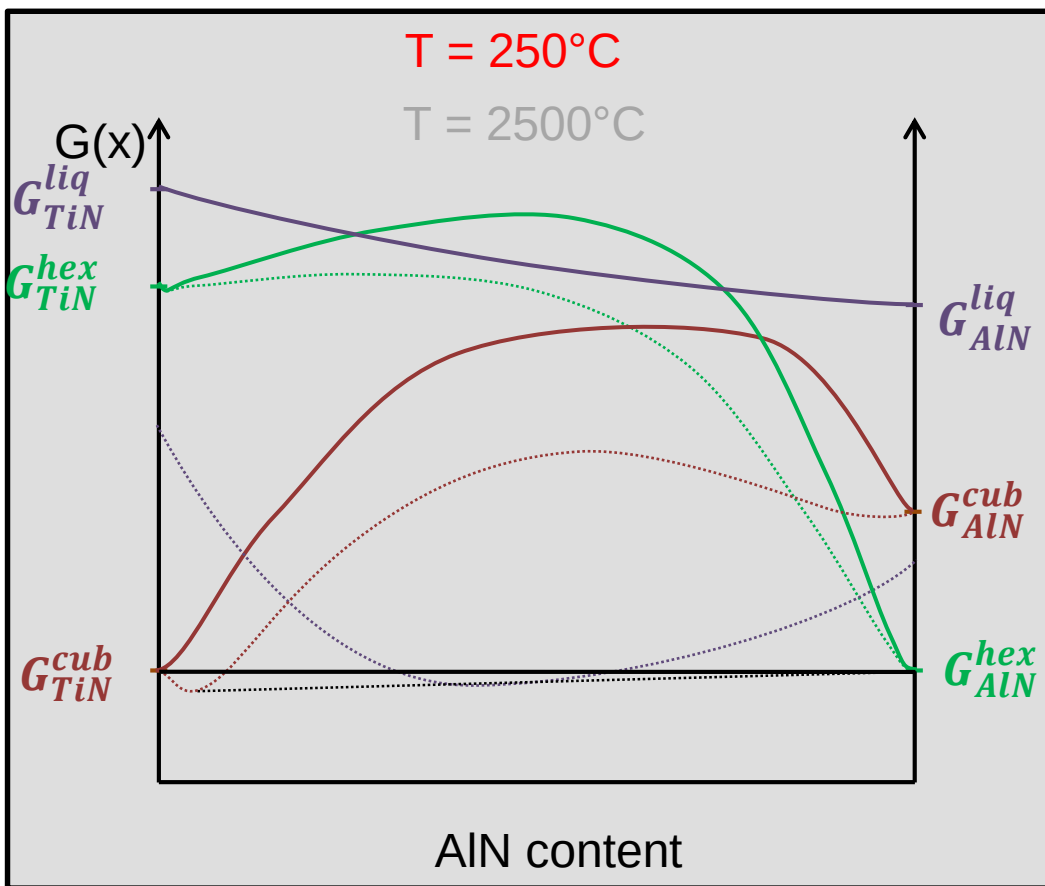
TiN:

$$\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$$

AlN:

$$G_{\text{cubic}} \ll G_{\text{hex}} < G_{\text{liquid}} \quad \Delta G_{\text{TiN}} > \Delta G_{\text{AlN}} \quad G_{\text{hex}} < G_{\text{cubic}} < G_{\text{liquid}}$$

Draw $G(x)$ @ 250°C and 2500°C



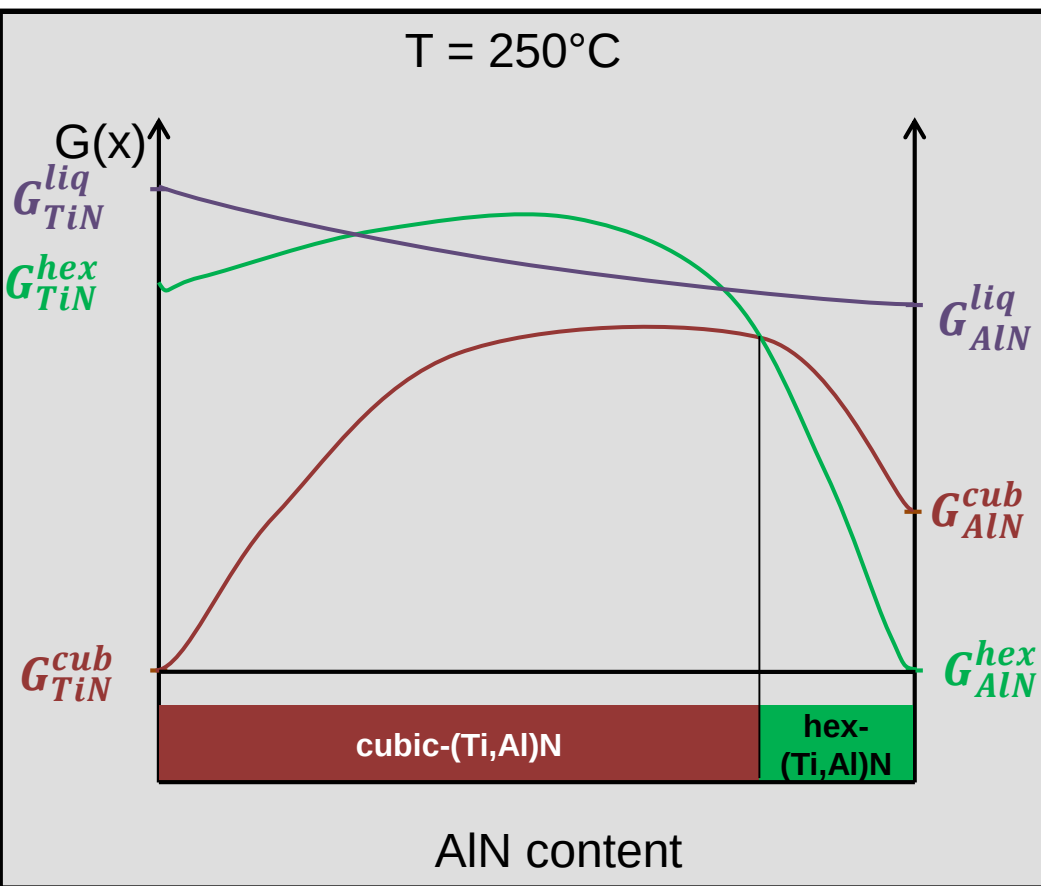
1. Choose the temperature at which you find more information in the phase diagram!
2. Order the components in the different phases.
3. Think about Ω for solid phases (cubic and hex): Do you expect $\Omega_{\text{c/h}} < 0$ or $\Omega_{\text{c/h}} > 0$? If you cannot decide for one phase, assume $\Omega_{\text{c}} = \Omega_{\text{h}}$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
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Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$

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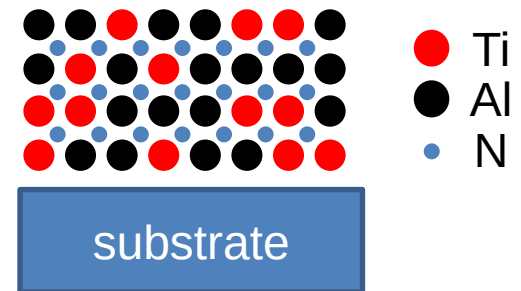
Vapour phase condensation



Atoms cannot form two phases
TiN+AlN because of limited mobility
(non-equilibrium processing).

Therefore, only a single (Ti,Al)N
phase can form.

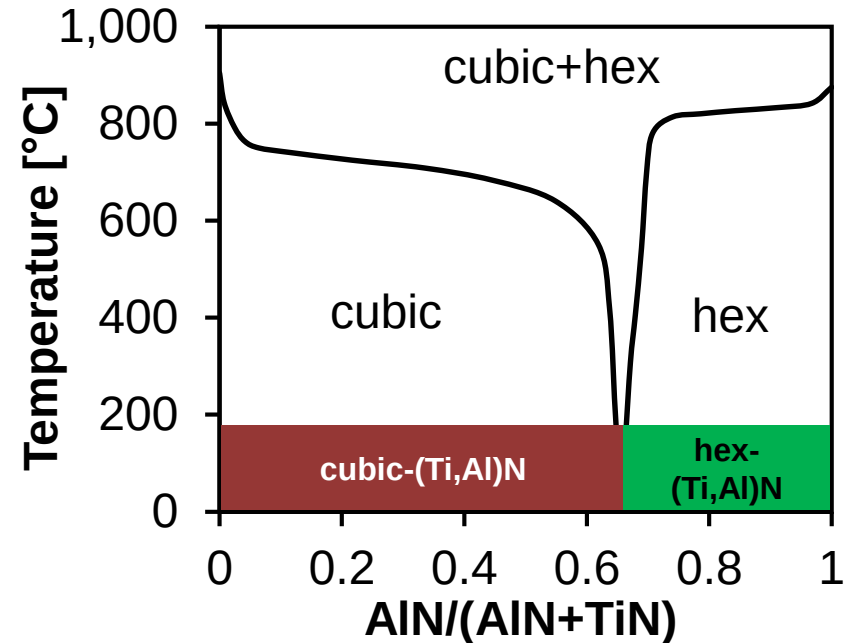
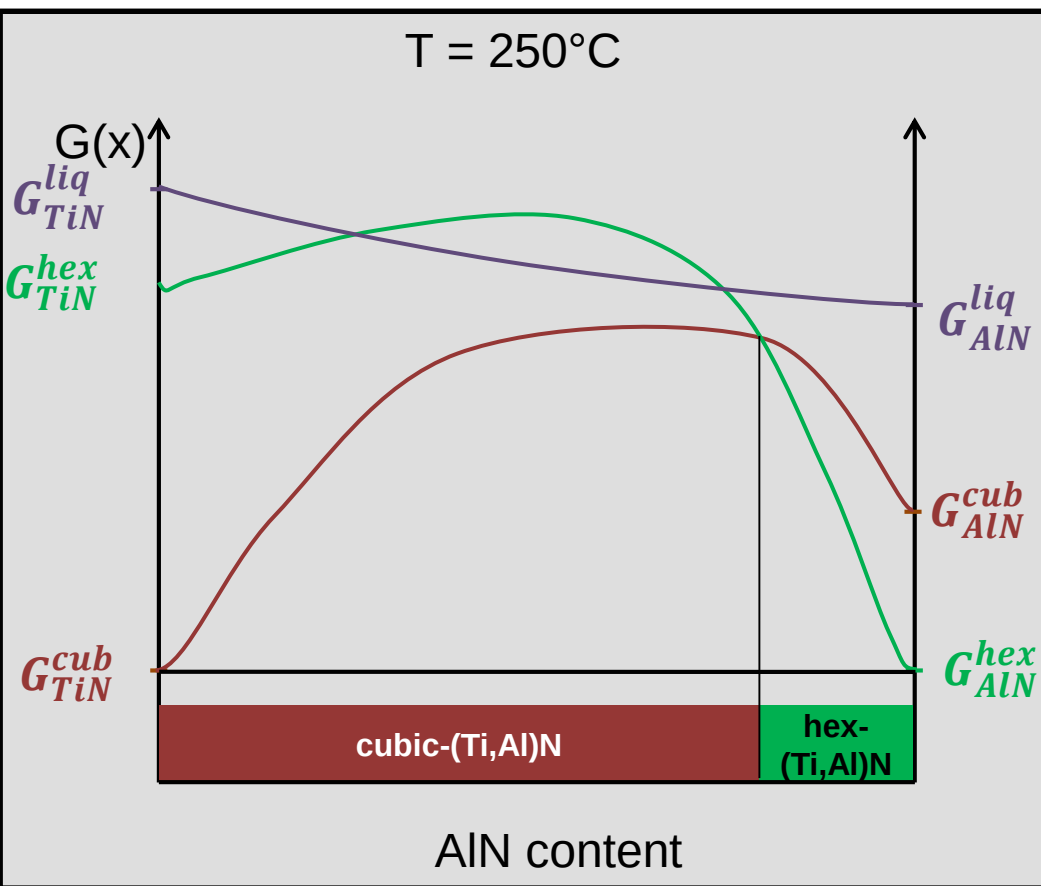
→ What is the single phase with
lowest energy?



From metal vapour to solid within a fraction of $1 \mu\text{s}$

→ Extreme quenching rates ($\gg 10^{10} \text{ }^\circ\text{C/s}$)!

Vapour phase condensation



Experimental non-equilibrium (metastable) TiN-AlN phase diagram [Spencer, Z. Metallk. 92 (2001) 10]

→ $G(x)$ curves can predict metastable phase formation!

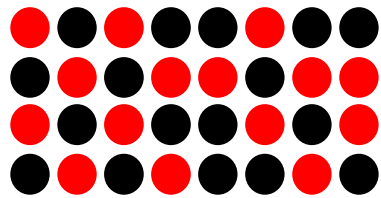
From metal vapour to solid within a fraction of $1\ \mu\text{s}$
 → Extreme quenching rates ($\gg 10^{10}\ ^\circ\text{C/s}$)!

Ti_{0.5}Al_{0.5}N: A real solution

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}}$$

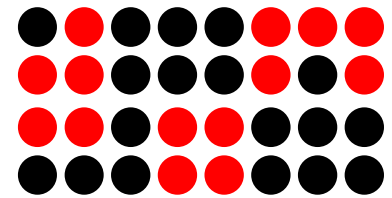
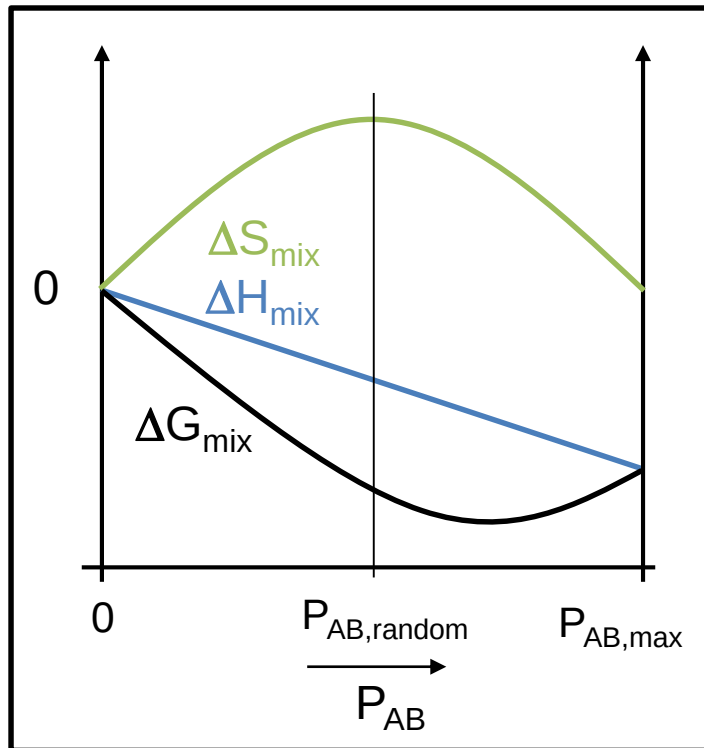
Think about **bonds** & **configurations**

REAL SOLUTIONS



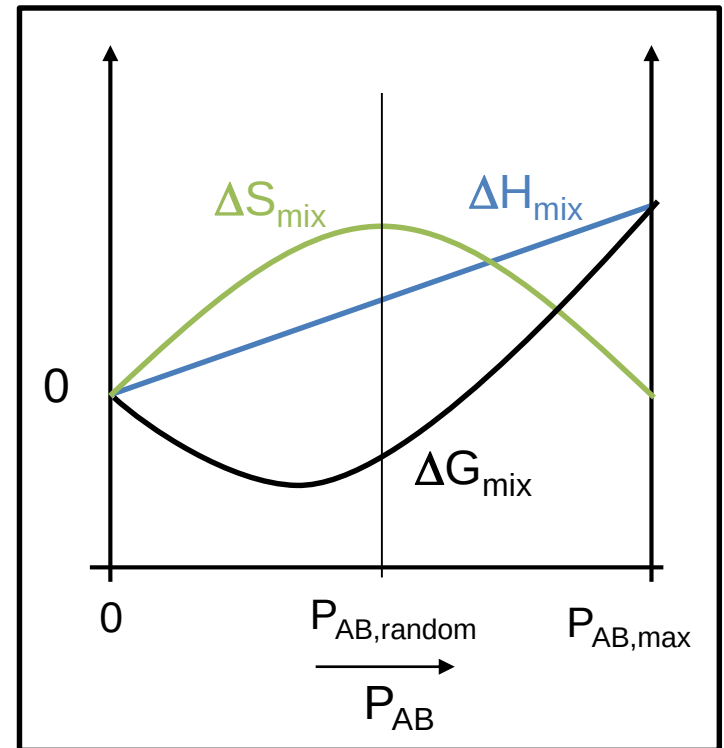
$$\Omega < 0$$

Ordering



$$\Omega > 0$$

Clustering



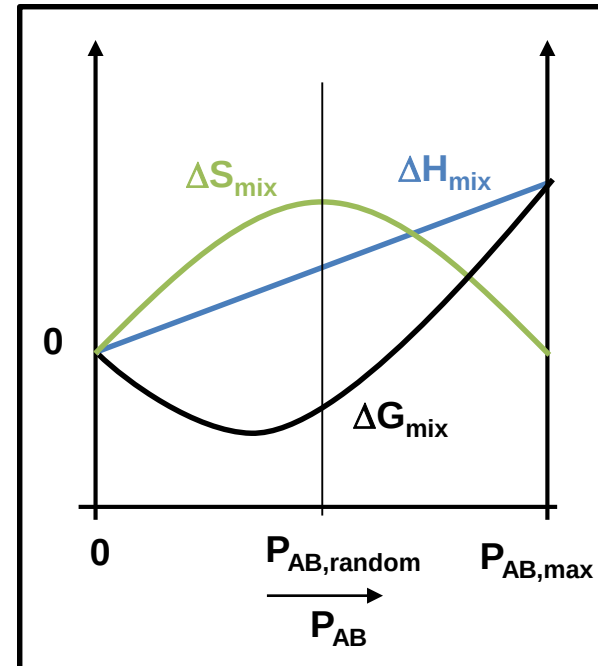
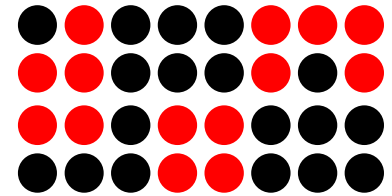
Ti_{0.5}Al_{0.5}N: A real solution

Visualizing atomic composition in 3D:
3D atom probe tomography



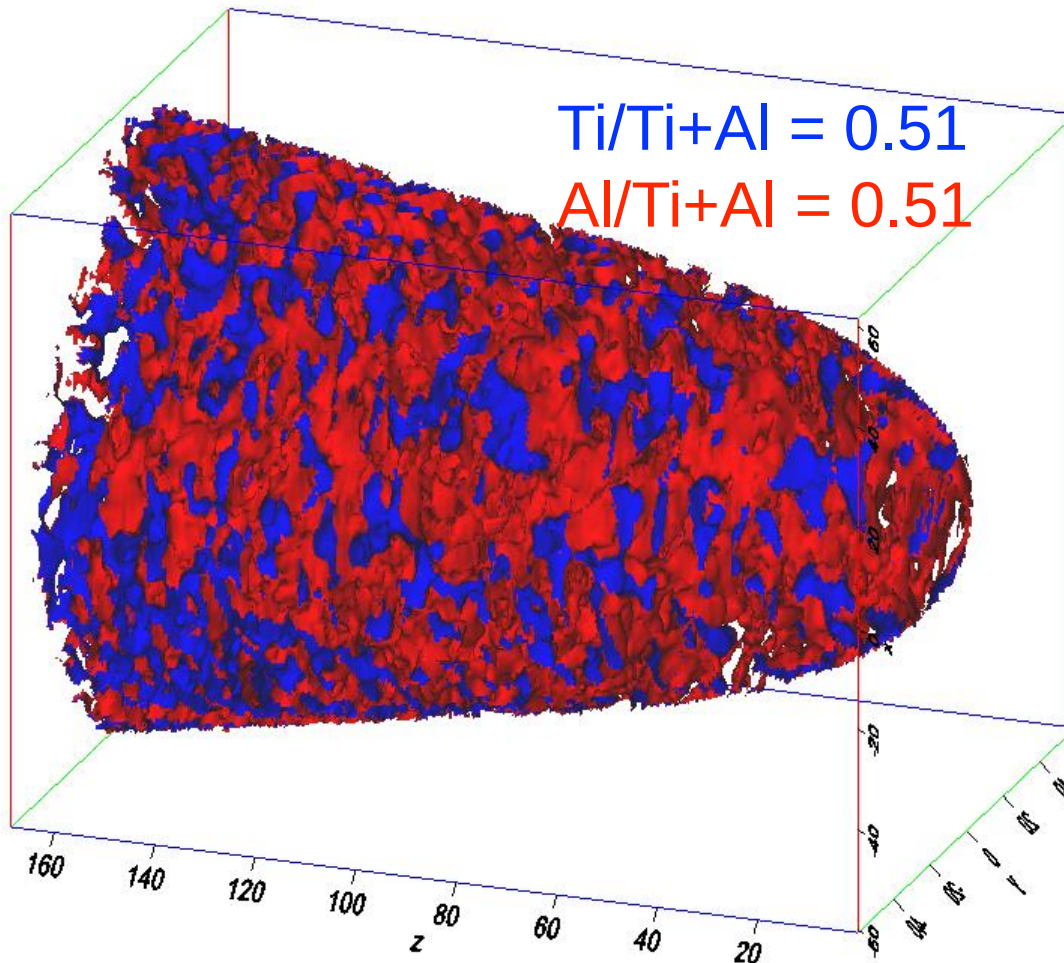
REAL SOLUTIONS

↓ Clustering ↓



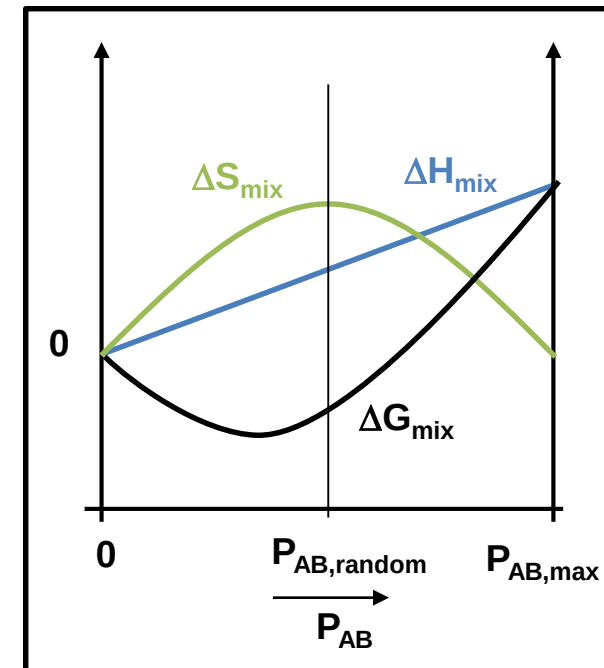
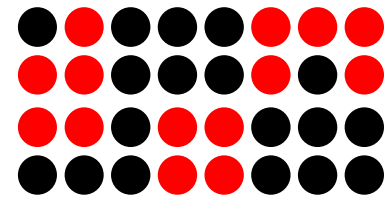
Ti_{0.5}Al_{0.5}N: A real solution

Visualizing atomic composition in 3D:
3D atom probe tomography



REAL SOLUTIONS

↓ Clustering ↓



Concepts, key ideas

Strategy for predicting metastable phase formation in vapour phase condensation:

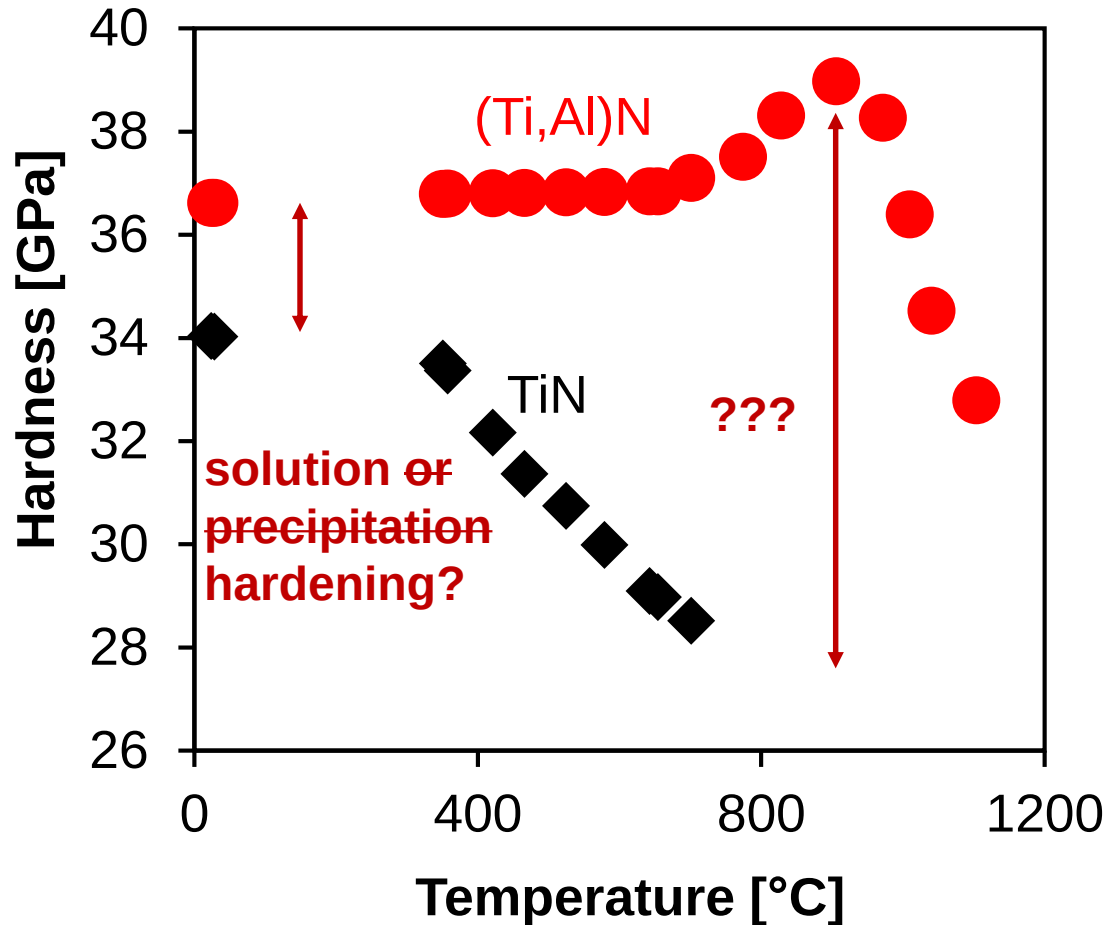
1. Derive $G(x)$ curves from the stable phase diagram.
2. For each composition, the single phase with lowest Gibbs energy forms during vapour phase condensation.

In real solutions, atoms form short-range order to minimize G :

clustering in case of $\Omega > 0$ or
ordering in case of $\Omega < 0$.

This ordering can be observed!

Application: (Ti,Al)N coatings for cutting tools

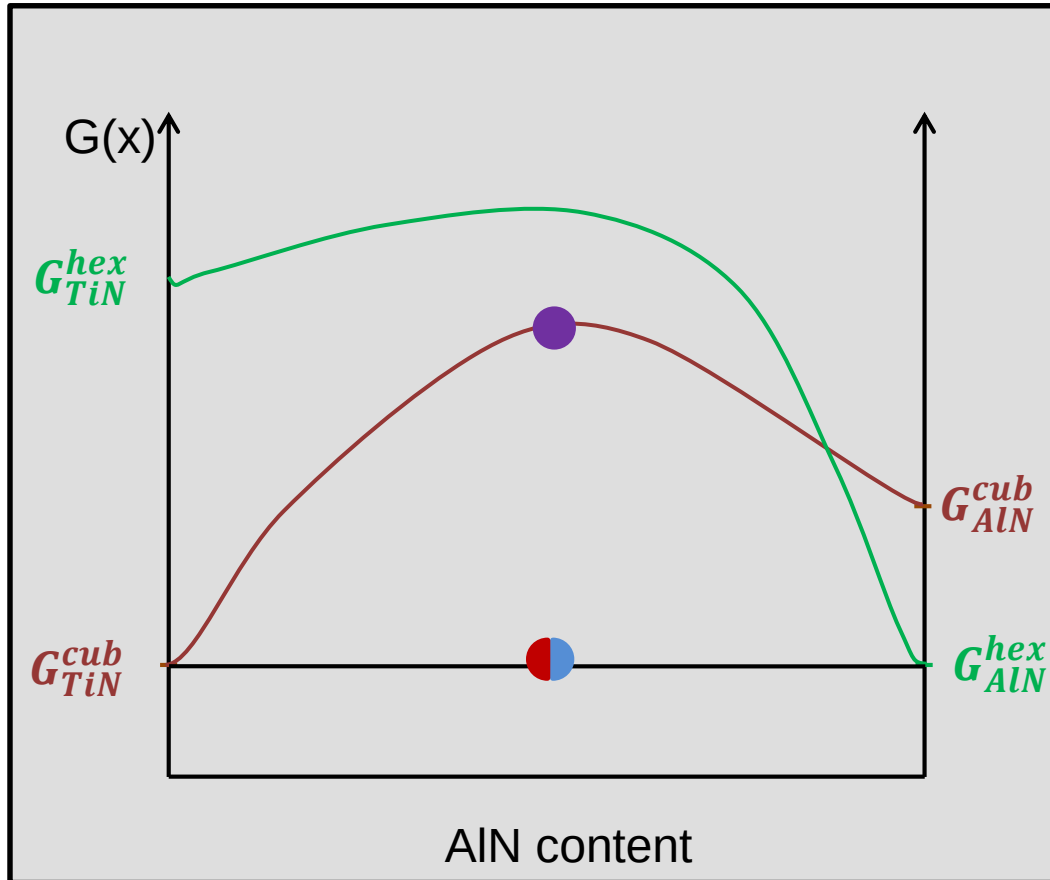


H increases by Al addition!

But WHY?

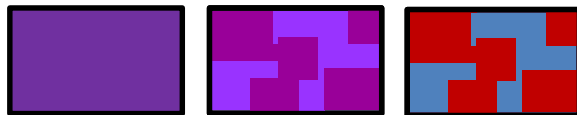
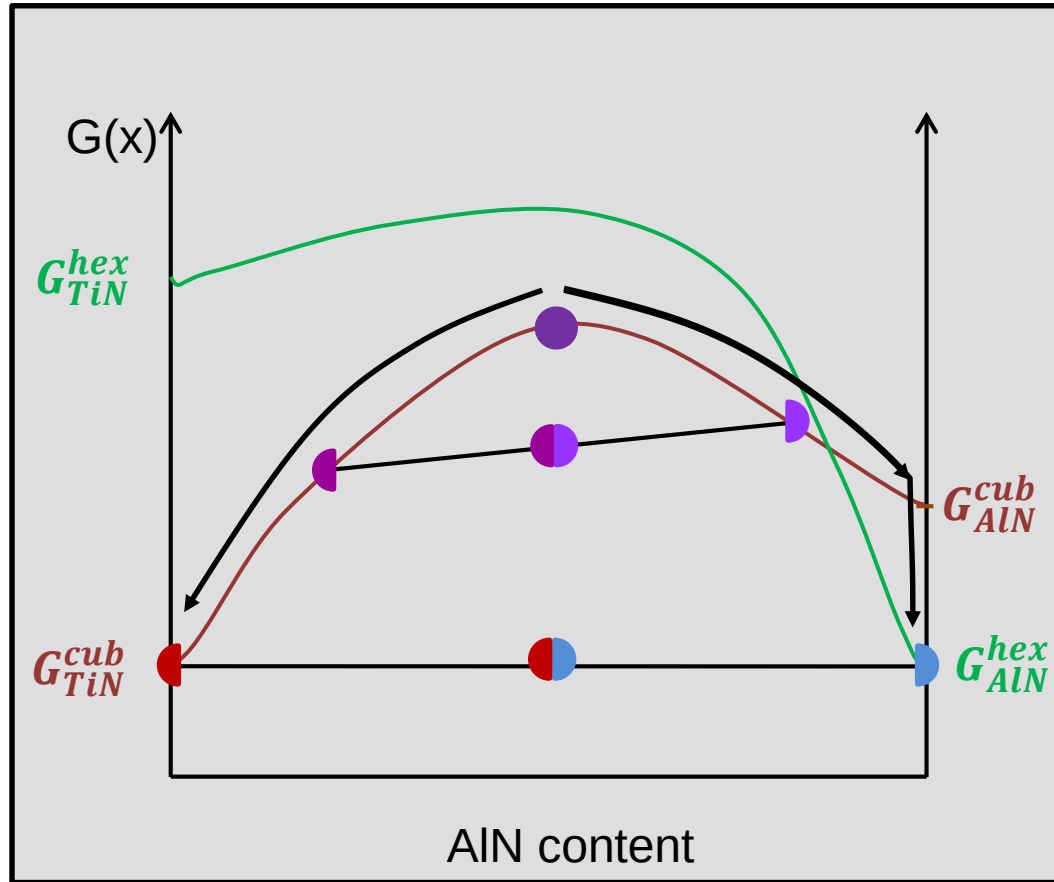
Let's look at $G(x)$ curves!

Annealing of a metastable phase: How can the Gibbs energy be lowered?

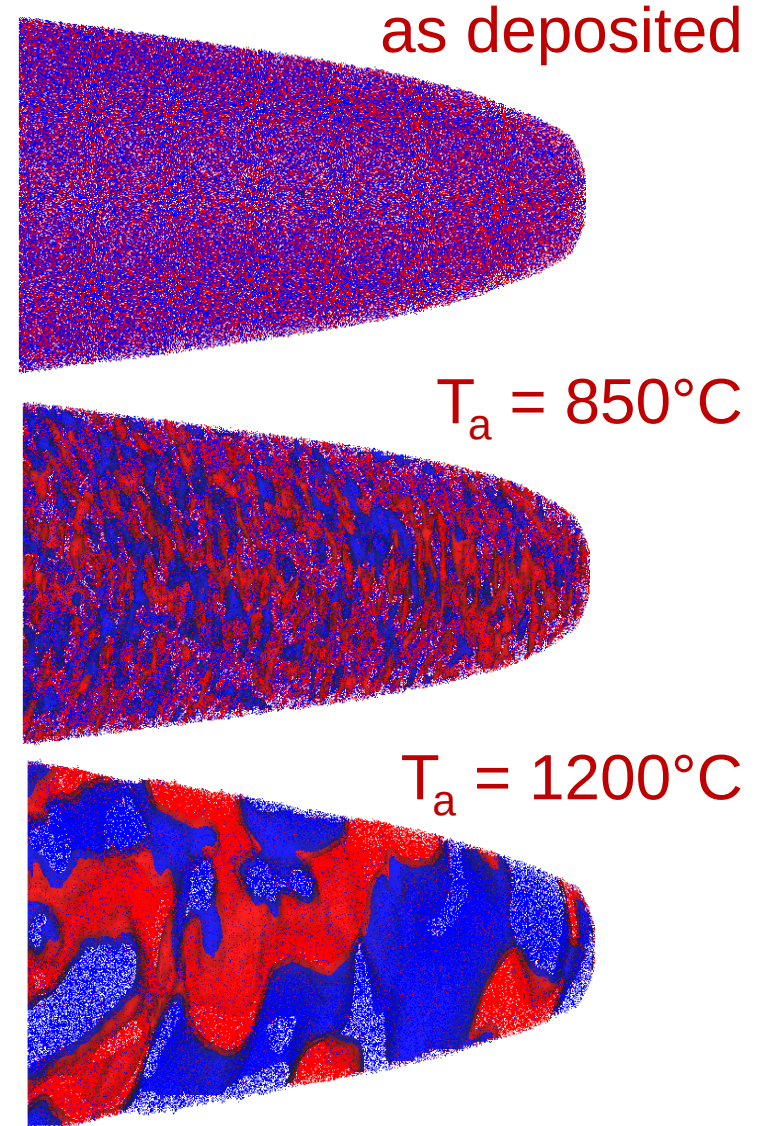


1. What is the stable state for $Ti_{0.5}Al_{0.5}N$?
→ cub-TiN + hex-AlN

Annealing of a metastable phase: How can the Gibbs energy be lowered?

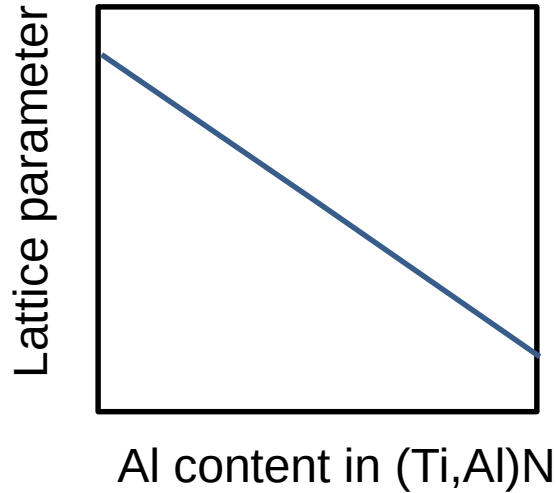


$$E_A(\text{de-mixing}) = E_A(\text{diffusion})$$



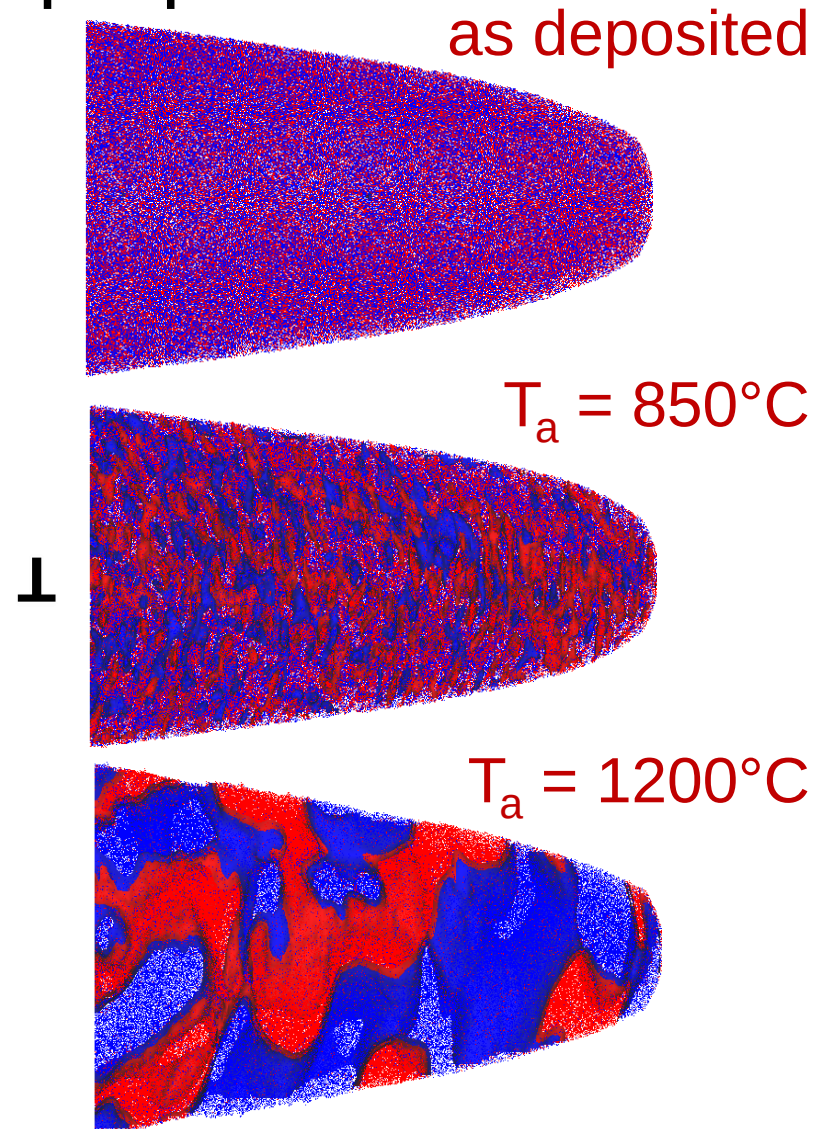
to Baben et al., Materials Research Letters (2016).

Annealing of a metastable phase: Implications on mechanical properties

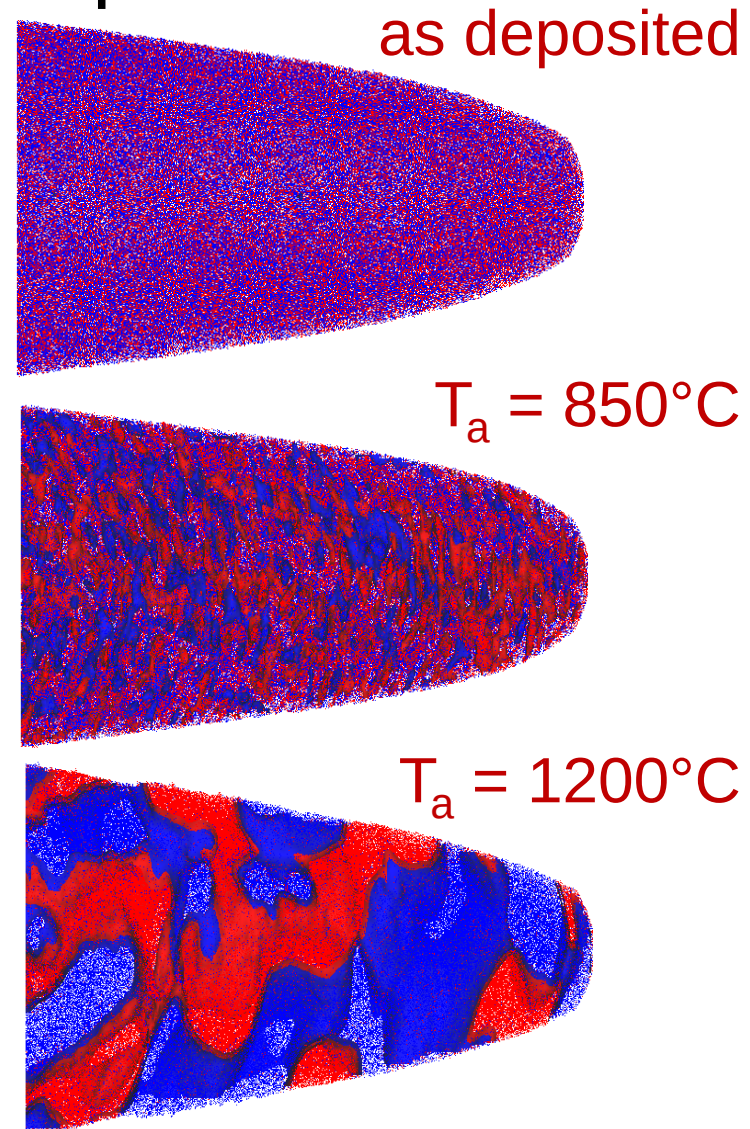
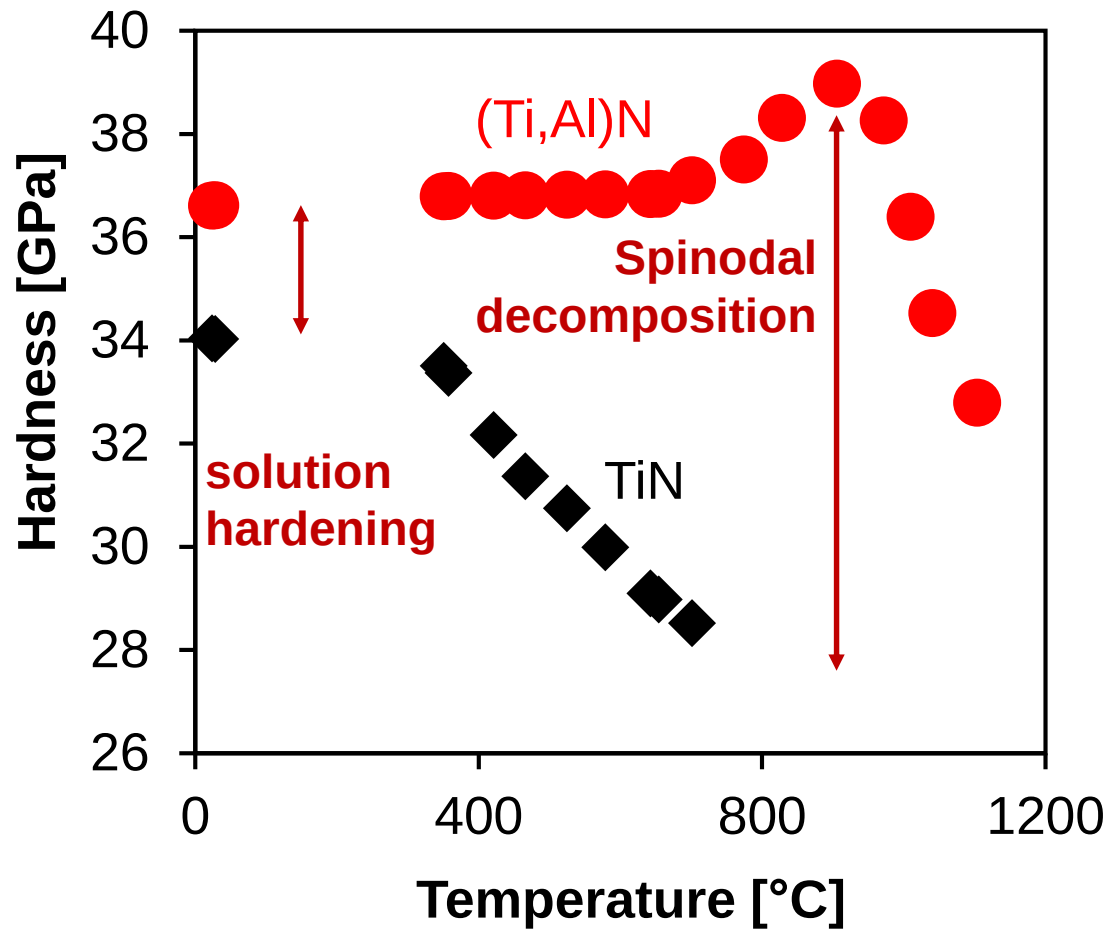


→ Composition variation leads to variation of lattice parameter.

→ Strain field!



Annealing of a metastable phase: Implications on mechanical properties



Outline

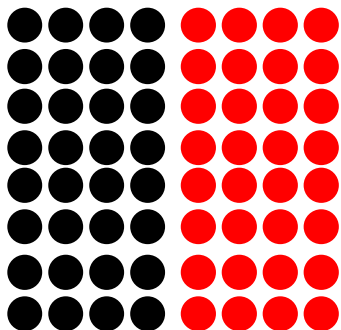
1. Understanding processes&materials based on $G(x,T,p)$
QUALITATIVE APPLICATION OF MC II
2. Modelling $G(x,T,p)$ based on theory&experiment
QUALITATIVE $\rightarrow$ QUANTITATIVE
3. Modelling processes&materials based on $G(x,T,p)$
QUANTITATIVE APPLICATION OF MC II

Strategy:

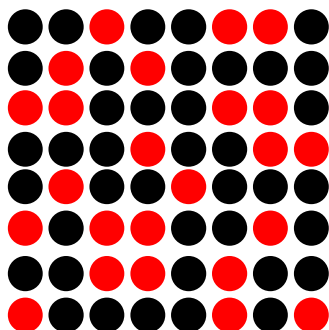
$$\begin{aligned}
 G_{\text{total}} &= X_A G_A + X_B G_B \\
 &= X_A(H_A - TS_A) + X_B(H_B - TS_B) \\
 &\quad - T\Delta S_{\text{mix}}
 \end{aligned}$$

$$+ \Delta H_{\text{mix}}$$

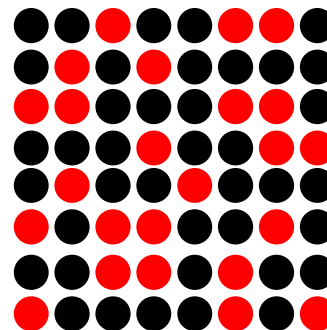
$$+ \Delta G_{\text{excess}}$$



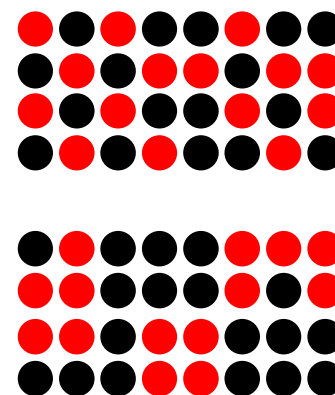
mechanical mixture
(two powders)



ideal solution
randomly mixed
 $A-A+B-B = 2A-B$



regular solution
randomly mixed
 $A-A+B-B \approx 2A-B$



real solution
ordering/clustering
 $A-A+B-B \ll 2A-B$
 $A-A+B-B \gg 2A-B$

What thermodynamic property describes the temperature dependence of the enthalpy?

A) entropy

B) thermal expansion coefficient

C) heat capacity

D) volume

What thermodynamic property describes the temperature dependence of the enthalpy?

A) entropy

B) thermal expansion coefficient

C) heat capacity

D) volume

$$C_P = dH/dT$$

$$H(T) = H^{298K} + \int_{298K}^T C_P dT$$

What expression describes the temperature dependence of the entropy?

A) $dS/dT = C_p$

B) $dS/dT = T^*C_p$

C) $dS/dT = C_p/T$

D) $dS/dT = T^*\ln(C_p)$

What expression describes the temperature dependence of the entropy?

A) $dS/dT = C_p$

B) $dS/dT = T^*C_p$

C) $dS/dT = C_p/T$

$$S(T) = S^{298K} + \int_{298K}^T \frac{C_p}{T} dT$$

D) $dS/dT = T^*\ln(C_p)$

CalPhaD: Modelling $G(T)$

$$G(T) = H(T) - TS(T)$$

$$= H^{298K} + \int_{298K}^T C_P dT - T \left[S^{298K} + \int_{298K}^T \frac{C_P}{T} dT \right]$$

What thermodynamic data is needed to model $G(T)$?

→ H^{298K} , S^{298K} , $C_P(T)$

CalPhaD: Modelling $G(T)$

In 1991, the SGTE (Scientific Group Thermodata Europe, a large consortium of groups working on thermodynamic databases), agreed on a set of

$$H^{298K}, S^{298K}, C_p(T)$$

for the elements in different crystal structures

→ Dinsdale, CALPHAD 15 (1991) 317.

What thermodynamic property describes the pressure dependence of the Gibbs energy?

A) entropy

B) thermal expansion coefficient

C) heat capacity

D) volume

What thermodynamic property describes the pressure dependence of the Gibbs energy?

A) entropy

B) thermal expansion coefficient

C) heat capacity

D) volume

$$V = dG/dp$$

CalPhaD: Modelling $G(p)$

$$dG/dp = V$$

What thermodynamic data is needed to model $G(p)$?

→ molar volume and compressibility or bulk modulus

→ i.e. $V(p)$

Strategy:

$$G_{\text{total}} = X_A G_A + X_B G_B$$

$$= X_A(H_A - TS_A) + X_B(H_B - TS_B) \quad \checkmark$$

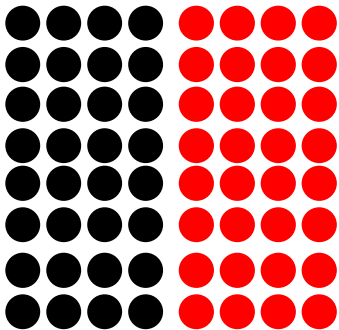
$$- T\Delta S_{\text{mix}} \quad \checkmark$$

$$+ RT \sum X_i \ln X_i$$

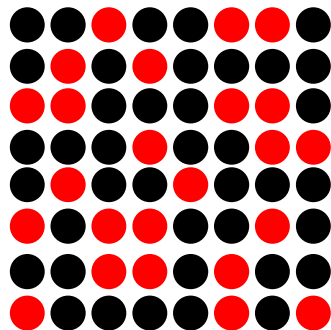
$$+ \Delta H_{\text{mix}} \quad \checkmark$$

$$+ \Omega X_A X_B$$

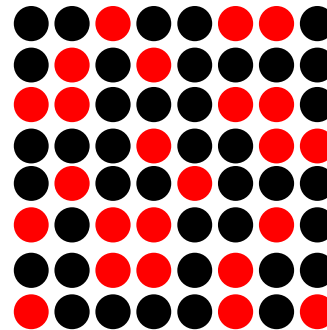
$$+ \Delta G_{\text{excess}} \quad ?$$



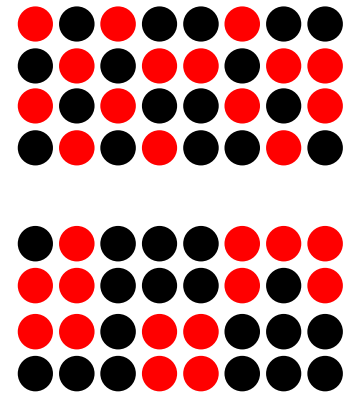
mechanical mixture
(two powders)



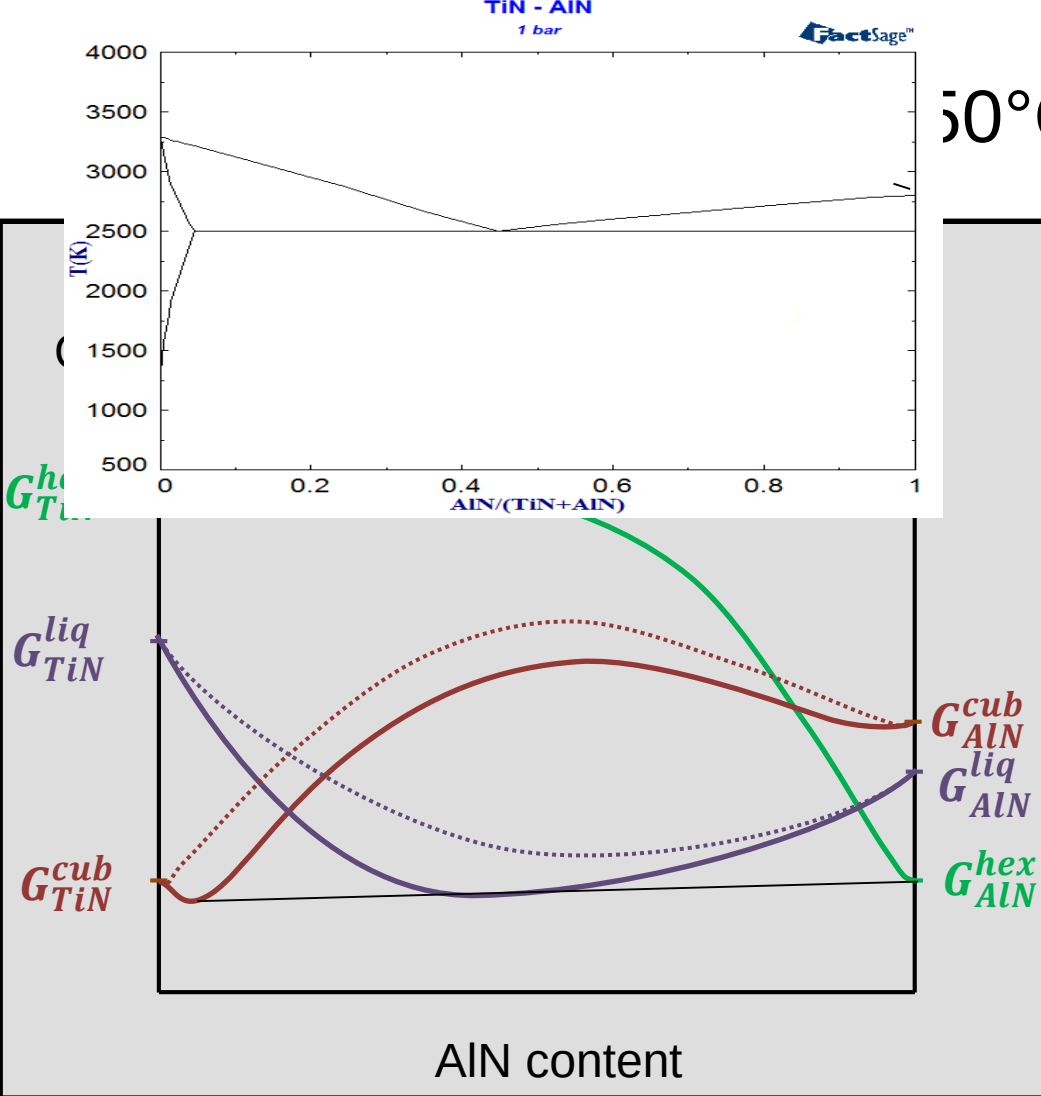
ideal solution
randomly mixed
 $A-A+B-B = 2A-B$



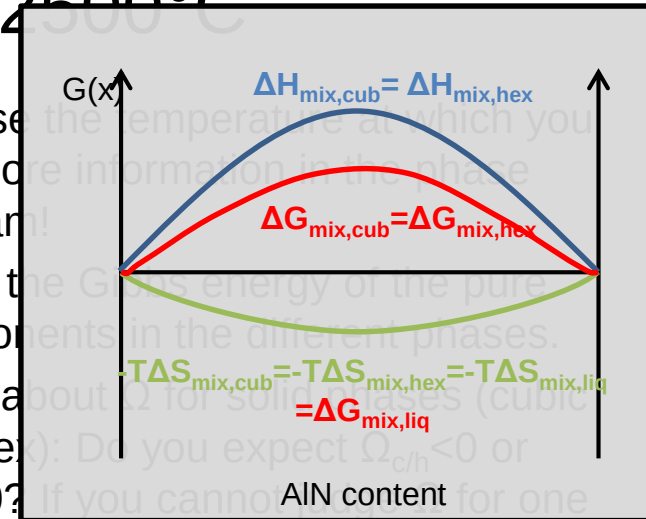
regular solution
randomly mixed
 $A-A+B-B \approx 2A-B$



real solution
ordering/clustering
 $A-A+B-B \ll 2A-B$
 $A-A+B-B \gg 2A-B$



50°C and 2500°C



1. Choose the temperature at which you find more information in the phase diagram!
2. Order the components in the different phases.
3. Think about the phase and hexagonal phase, assume $\Omega_c = \Omega_h$.
4. Do you expect $|\Delta H_{\text{mix}}| < |T\Delta S_{\text{mix}}|$ or $|\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$?
5. Draw ΔH_{mix} , $-T\Delta S_{\text{mix}}$ and ΔG_{mix} for all phases. Assume $\Delta H_{\text{mix}}(\text{liquid}) \approx 0$.
6. Draw $G(x)$ for the solid phases.
7. Draw $G(x)$ for the liquid phase, taking into account position of the eutectic. Eventually adjust $G(x)$ for the solid phases to match solubility limits.
8. Repeat the steps for the other temperature.

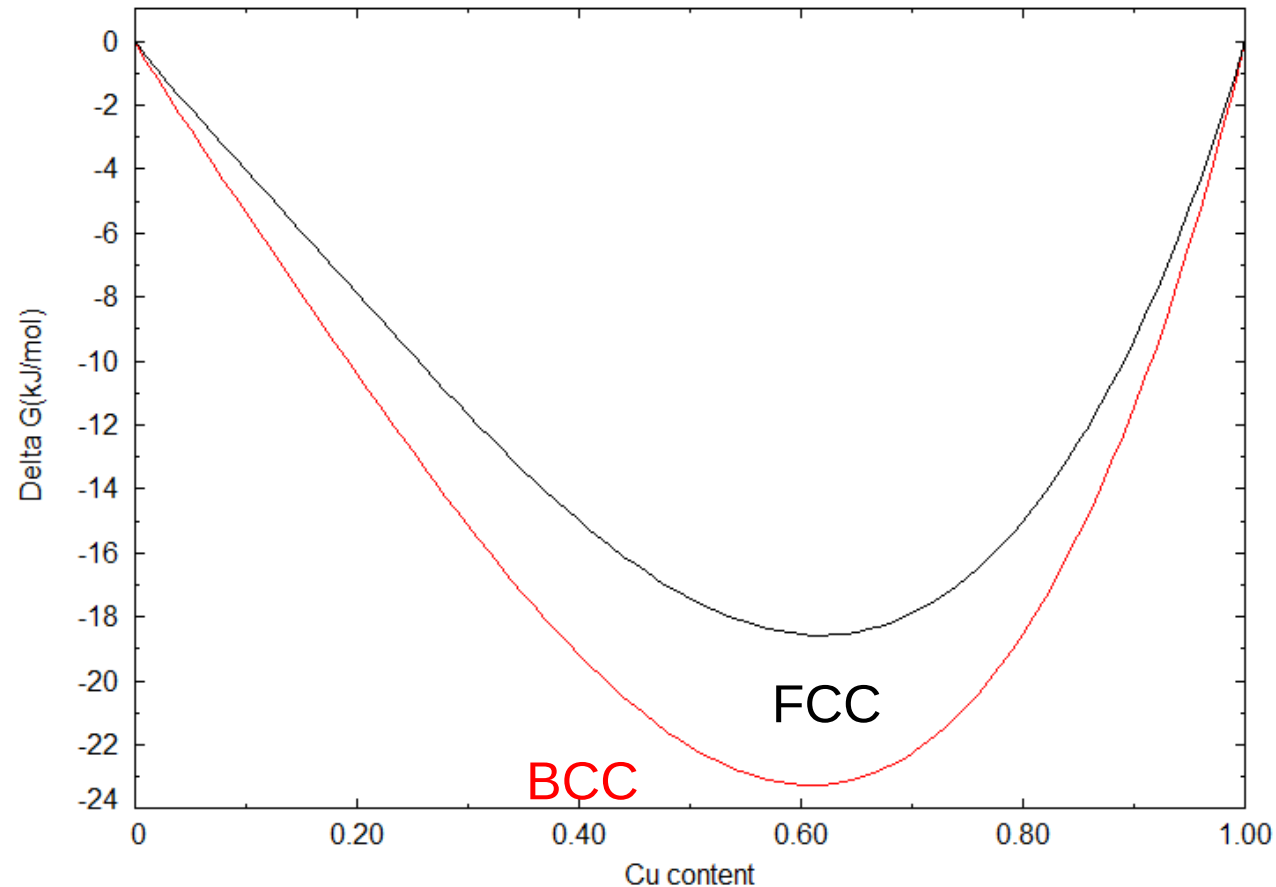
Low/virtually no solubility $\rightarrow |\Delta H_{\text{mix}}| > |T\Delta S_{\text{mix}}|$

TiN: $\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$ AIN: $\Omega_{\text{cubic}} = \Omega_{\text{hex}} > 0$
 $G_{\text{cubic}} \ll G_{\text{liquid}} < G_{\text{hex}}$ $\Delta G_{\text{TiN}} > \Delta G_{\text{AlN}}$ $G_{\text{hex}} < G_{\text{liquid}} < G_{\text{cubic}}$

What information can be extracted from the Al-Cu phase diagram?

A) $\Omega_{\text{fcc}} < \Omega_{\text{bcc}}$

B) $\Omega_{\text{fcc}} > \Omega_{\text{bcc}}$



Strategy:

$$G_{\text{total}} = X_A G_A + X_B G_B$$

$$= X_A(H_A - TS_A) + X_B(H_B - TS_B) \quad \checkmark$$

$$- T\Delta S_{\text{mix}} \quad \checkmark$$

$$+ RT \sum X_i \ln X_i \quad \checkmark$$

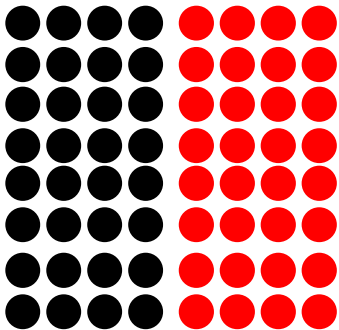
$$+ \Delta H_{\text{mix}} \quad \checkmark$$

$$+ X_A X_B \Omega \quad \checkmark$$

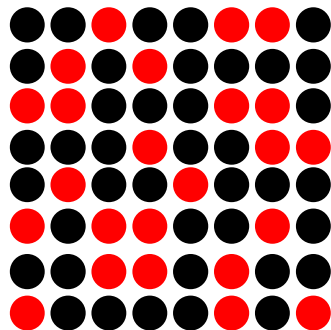
$$\text{e.g. Redlich-Kister} \quad \checkmark$$

$$+ X_A X_B \Omega_v (X_A - X_B)^v$$

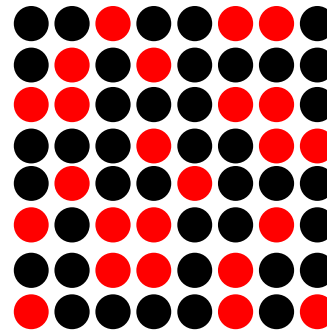
$$+ \Delta G_{\text{excess}}$$



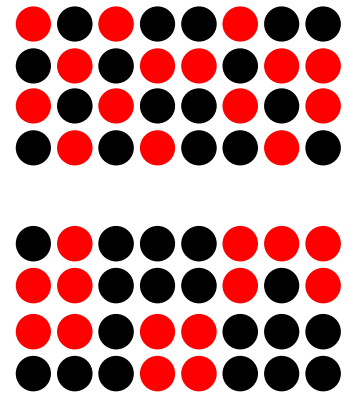
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ideal solution
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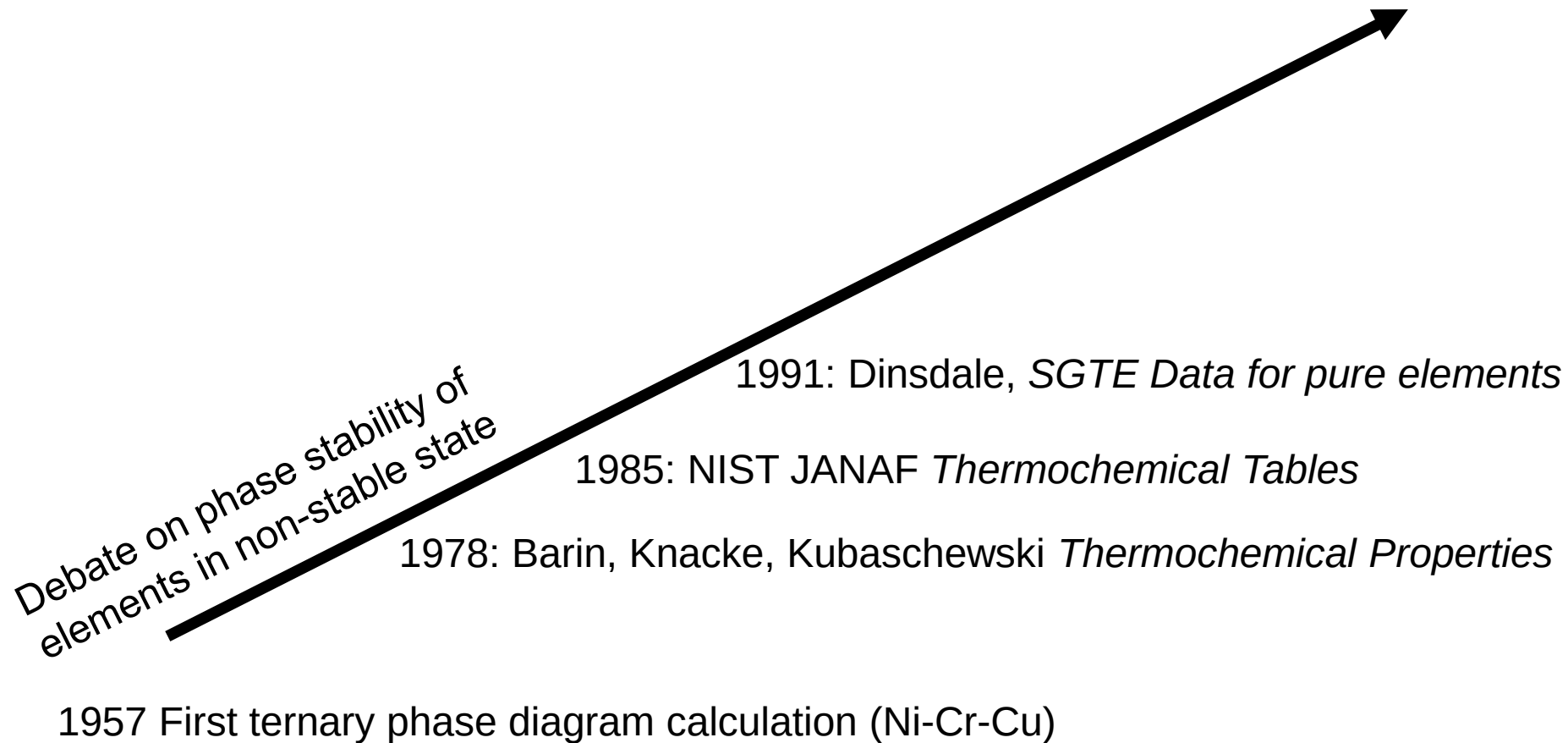


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ordering/clustering
 $A-A+B-B < 2A-B$
 $A-A+B-B > 2A-B$

History of computational thermodynamics and thermodynamic databases



Strategy:

$$G_{\text{total}} = X_A G_A + X_B G_B$$

$$= X_A(H_A - TS_A) + X_B(H_B - TS_B) \quad \checkmark$$

$$- T\Delta S_{\text{mix}} \quad \checkmark$$

$$+ RT \sum X_i \ln X_i \quad \checkmark$$

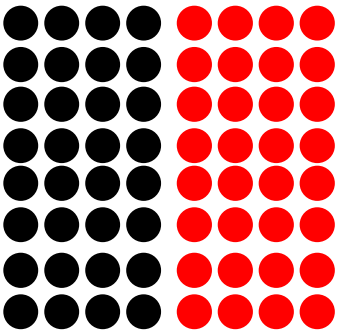
$$+ \Delta H_{\text{mix}} \quad \checkmark$$

$$+ X_A X_B^* \Omega \quad \checkmark$$

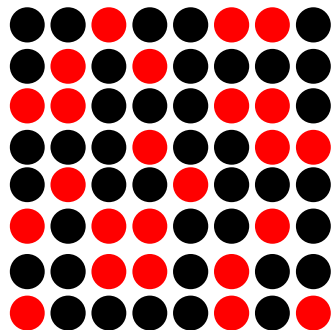
$$\text{e.g. Redlich-Kister} \quad \checkmark$$

$$+ X_A X_B^* \Omega_v^* (X_A - X_B)^v$$

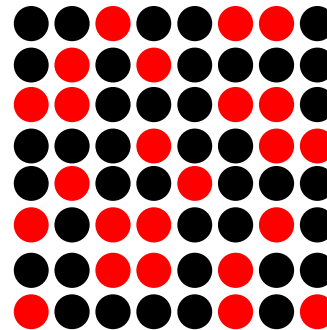
$$+ \Delta G_{\text{excess}}$$



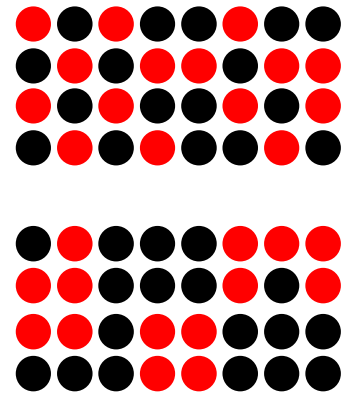
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History of computational thermodynamics and thermodynamic databases

Today: SGTE Solution database contains 79 elements, 317 solution phases, 1166 stoichiometric phases

1980s-1990s: Founding of several companies specializing in computational thermodynamics

1990s-2000s: growth of solution databases

Debate on phase stability of elements in non-stable state

1991: Dinsdale, *SGTE Data for pure elements*

1985: NIST JANAF *Thermochemical Tables*

1978: Barin, Knacke, Kubaschewski *Thermochemical Properties*

1957 First ternary phase diagram calculation (Ni-Cr-Cu)

History of computational thermodynamics and thermodynamic databases

Today: SGTE Solution database contains 79 elements,
317 solution phases, 1166 stoichiometric phases

*Allows description of
577 binary systems,
141 ternary systems,
15 higher order systems*

H	15 higher order systems																He
Li	Be											B	C	N	O	F	Ne
Na	Mg											Al	Si	P	S	Cl	Ar
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
Rb	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
Cs	Ba	La	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi	Po	At	Rn
Fr	Ra	Ac	Rf	Db	Sg	Bh	Hs	Mt	Ds								

~70 non-radioactive, non-noble gas elements

→ $70 \times 69 / 2 = 2415$ binary systems

→ $70 \times 69 \times 68 / 6 = 54740$ ternary systems

Materials Genome Initiative (MGI) launched in 2011



Executive Summary

Vision: *Advanced materials are essential to economic security and human well-being and have applications in multiple industries, including those aimed at addressing challenges in clean energy, national security, and human welfare. To meet these challenges, the Materials Genome Initiative will enable discovery, development, manufacturing, and deployment of advanced materials at least twice as fast as possible today, at a fraction of the cost.*



Materials Genome Initiative (MGI) launched in 2011

Achieving this vision requires successfully addressing four key challenges:

- (1) Leading a culture shift in materials research to encourage and facilitate an integrated team approach that **links computation, data, and experiment** and crosses boundaries between academia, National and Federal laboratories, and industry;
- (2) Integrating experiment, computation, and theory and **equipping the materials community with the advanced tools and techniques to work across materials classes** and along the materials development continuum from research to industrial application; = MC II
- (3) **Making digital data accessible** inc = www.materialsproject.org, www.oqmd.org, to a searchable materials data infrast www.aflowlib.org, www.nomad-coe.eu... able to others;
- (4) Creating a **world-class materials workforce** that is trained for careers in academia or industry, including high-tech manufacturing jobs.

= you!





of elements

excluded elements

Material Tags

Band Gap (eV)

Energy Above Hull

Formation Energy

unit cell sites

Density

Volume

Crystal Systems

Spacegroup Number

<https://materialsproject.org/>

530,243

NANOPOROUS MATERIALS

16,128

CONVERSION ELECTRODES

$$G(T, X_i)$$

*Allows description of
577 binary systems,
141 ternary systems,
15 higher order systems*

H	15 higher order systems															He	
Li	Be											B	C	N	O	F	Ne
Na	Mg											Al	Si	P	S	Cl	Ar
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
Rb	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
Cs	Ba	La	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi	Po	At	Rn
Fr	Ra	Ac	Rf	Db	Sg	Bh	Hs	Mt	Ds								

→ $70 \cdot 69 = 4830$ binary systems

→ $70 \cdot 69 \cdot 68 = 328440$ ternary systems

Newsflash: OQMD v1.1 is out! (Download it [here](#).)

Welcome to the Open Quantum Materials Database

The OQMD is a database of DFT-calculated thermodynamic and structural properties. This online interface is for convenient, small-scale access; for a more powerful utilization of the data, we recommend downloading the entire database and the API for interfacing with it, from the link below.

You can...

- Search** for materials by composition,
- Create** phase diagrams using the thermochemical data in OQMD,
- Determine** ground state compounds at any composition,
- Visualize** crystal structures, or
- Download** the entire database (and the API) for your own use!

Tweet @TheOQMD to ask what is stable at a composition, or to get a simple phase diagram!

The OQMD was created in [Chris Wolverton's group](#) at Northwestern University.

Contact us by [e-mail](#)

If you are using any results from this website, please reference this work as shown [here](#)

Current status

OQMD v1.1 has been released! Download it [here](#).

The database now contains **563247** entries. In addition, calculations of new structures are constantly ongoing! Recently added compounds include: [EuPaBe](#) [PrPaFe](#) [PaReHg](#) [AcLaPa](#) [KPaMo](#)

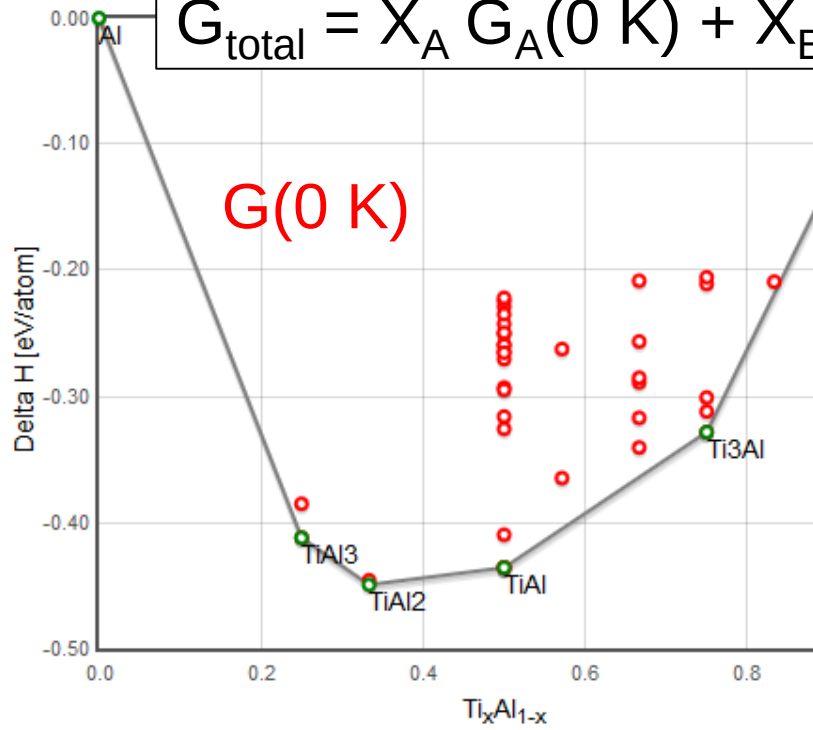
G(0 K)

<http://oqmd.org/>

Phase diagram creation

Specify a region of phase space:

$$G_{\text{total}} = X_A G_A(0 \text{ K}) + X_B G_B(0 \text{ K})$$



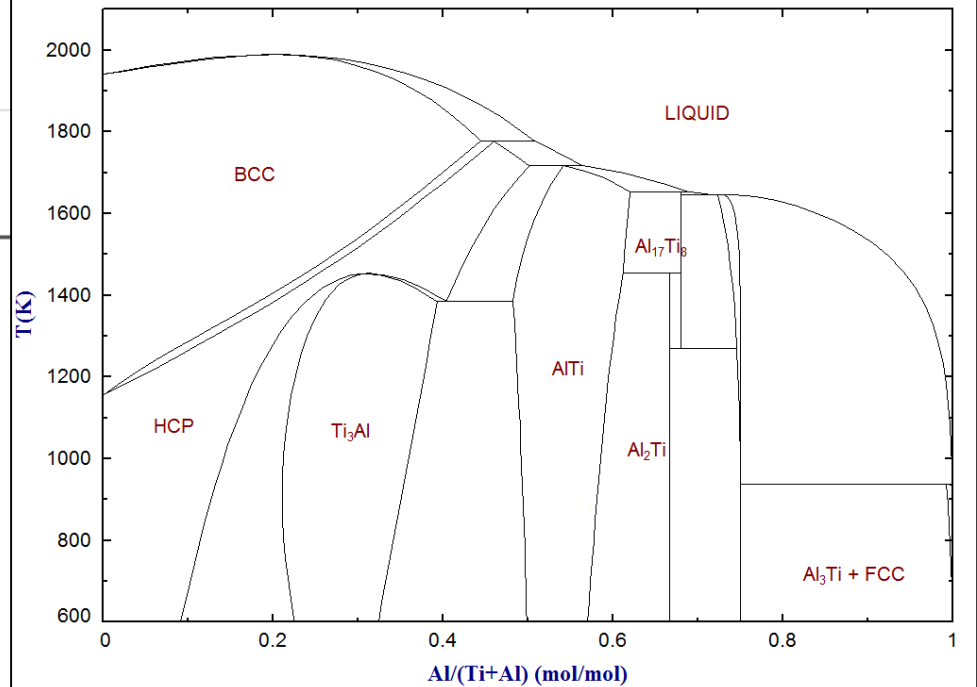
$$- T \Delta S_{\text{mix}}$$

$$+ \Delta H_{\text{mix}}$$

$$+ \Delta G_{\text{excess}}$$

Ti - Al
1 bar

FactSage™



AB2 -3.0

<http://oqmd.org/>

Welcome to the AFLOW distributed materials property repository: share with us your passion for innovation and technology.

Aflow is a globally available data **2.118.033** material compounds - with over **147.010.000** calculated properties (and growing).

G(0 K)

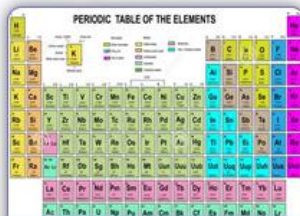
Try our Materials Database Search, use our online apps, consult our wiki and publications.

Enter a Compound Name, ICSD Number, [Aflowlib Unique Identifier](#) or advanced search string (ie. Mg & Sn & Cu).

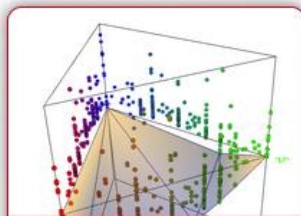
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Interview



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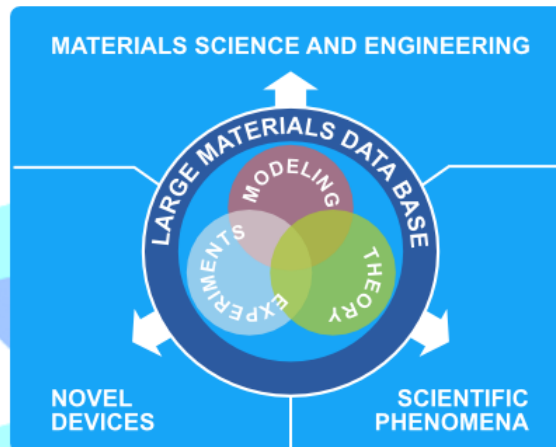
Enter Search...



The Novel Materials Discovery (NOMAD)

Laboratory develops a *Materials Encyclopedia* and *Big-Data Analytics* and *Advanced Graphics Tools* for materials science and engineering.

Eight complementary computational materials science groups and four high-performance computing centers form the synergetic core of this Centre of Excellence.



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Jan 12, 2017

[NOMAD presented at Tianjin University](#)

Jan 3, 2017

[NOMAD Hackathon, 18 - 20 Jan 2017](#)



MATERIALS ENCYCLOPEDIA



BIG-DATA ANALYTICS



ADVANCED GRAPHICS



HPC INFRASTRUCTURE



OUTREACH



H2020 NOMAD

This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 676580. The material presented and views expressed here are the responsibility of the author(s) only. The EU Commission takes no responsibility for any use made of the information set out.

Application: (Ti,Al)N coatings for cutting tools



You are interested to learn something about thermodynamics of your material system during BSc/MSc/PhD thesis / at work: What do you do?

CHECK PHASE DIAGRAMS/MATERIALS DATA E.G. AT

www.springermaterials.com www.factsage.com

www.materialsproject.org www.oqmd.org

www.aflowlib.org www.nomad-coe.eu

...

History of computational thermodynamics and thermodynamic databases

Debate on phase stability of compounds based on experimental and *ab initio* methods

10/2017: first purely *ab initio* based thermodynamic database

Today: SGTE Solution database contains 79 elements,
317 solution phases, 1166 stoichiometric phases

1980s-1990s: Founding of several companies
specializing in computational thermodynamics

Debate on phase stability of
elements in non-stable state

EXCITING YEARS TO COME!!!

WILL WE SEE THE THERMODYNAMIC MATERIALS GENOME?

growth
databases

SGTE Data for pure elements

JANAF Thermochemical Tables

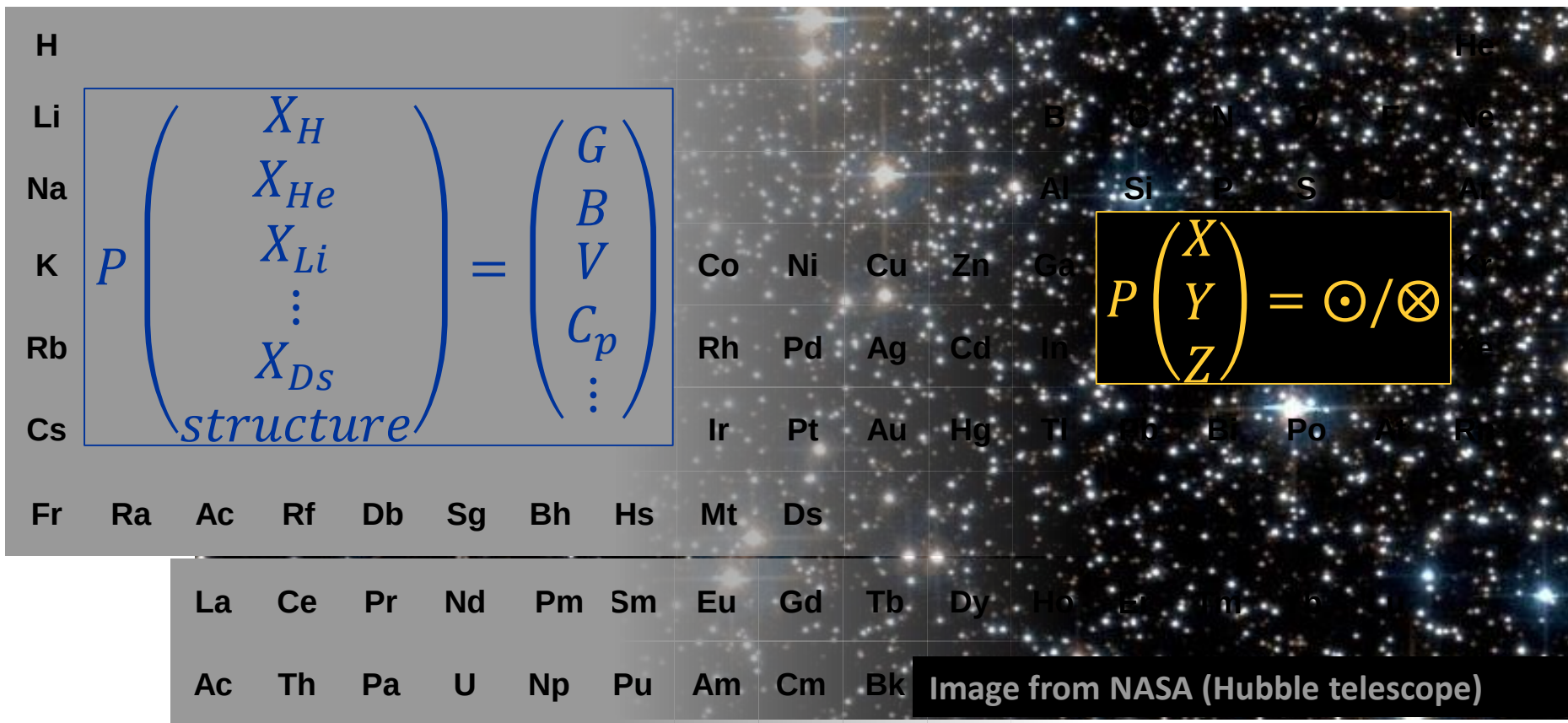
Knacke, Kubaschewski Thermochemical Properties

1957 First ternary phase diagram calculation (Ni-Cr-Cu)

Vision: Map of Chemical Space

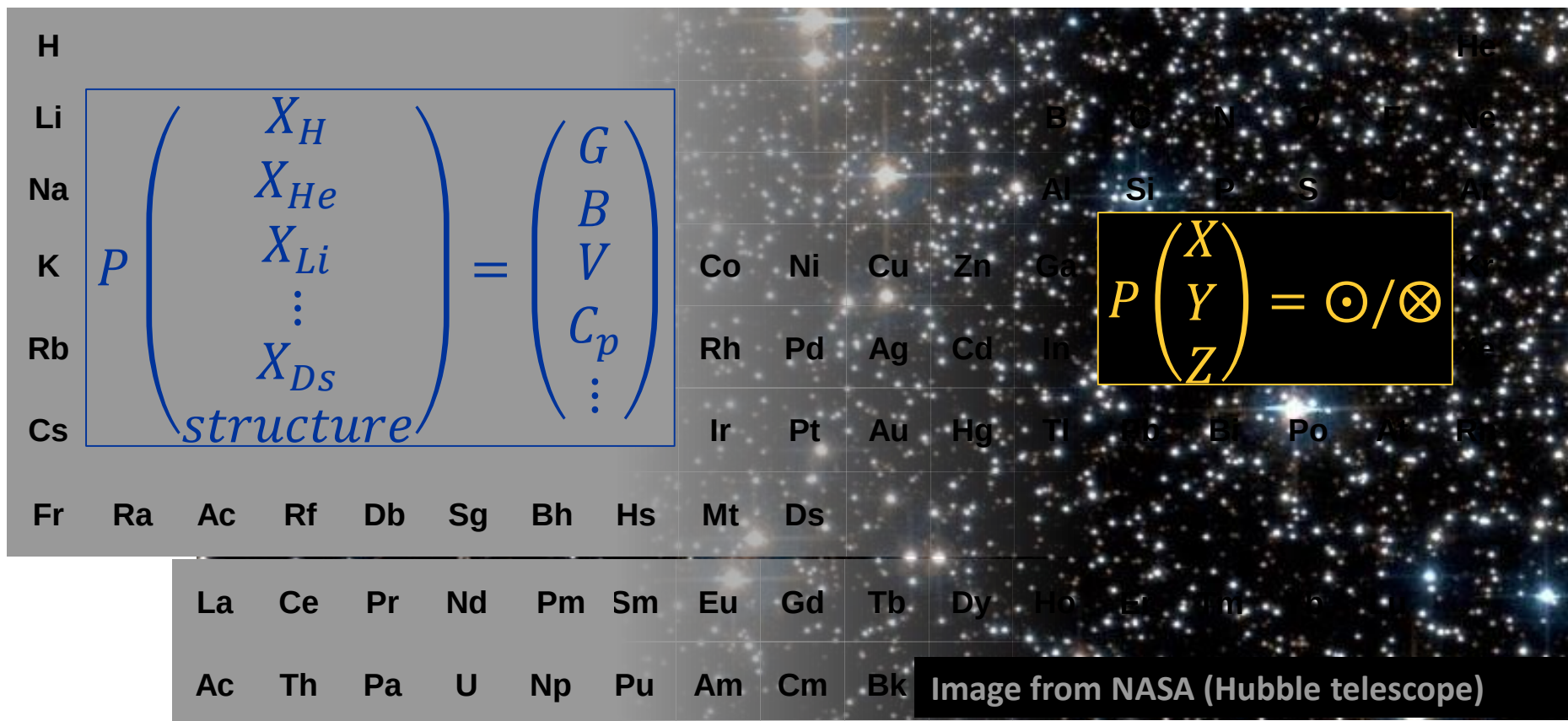
H																	He
Li	Be											B	C	N	O	F	Ne
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K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
Rb	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
Cs	Ba	La	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi	Po	At	Rn
Fr	Ra	Ac	Rf	Db	Sg	Bh	Hs	Mt	Ds								
		La	Ce	Pr	Nd	Pm	Sm	Eu	Gd	Tb	Dy	Ho	Er	Tm	Yb		
		Ac	Th	Pa	U	Np	Pu	Am	Cm	Bk	Image from NASA (Hubble telescope)						

Vision: Map of Chemical Space



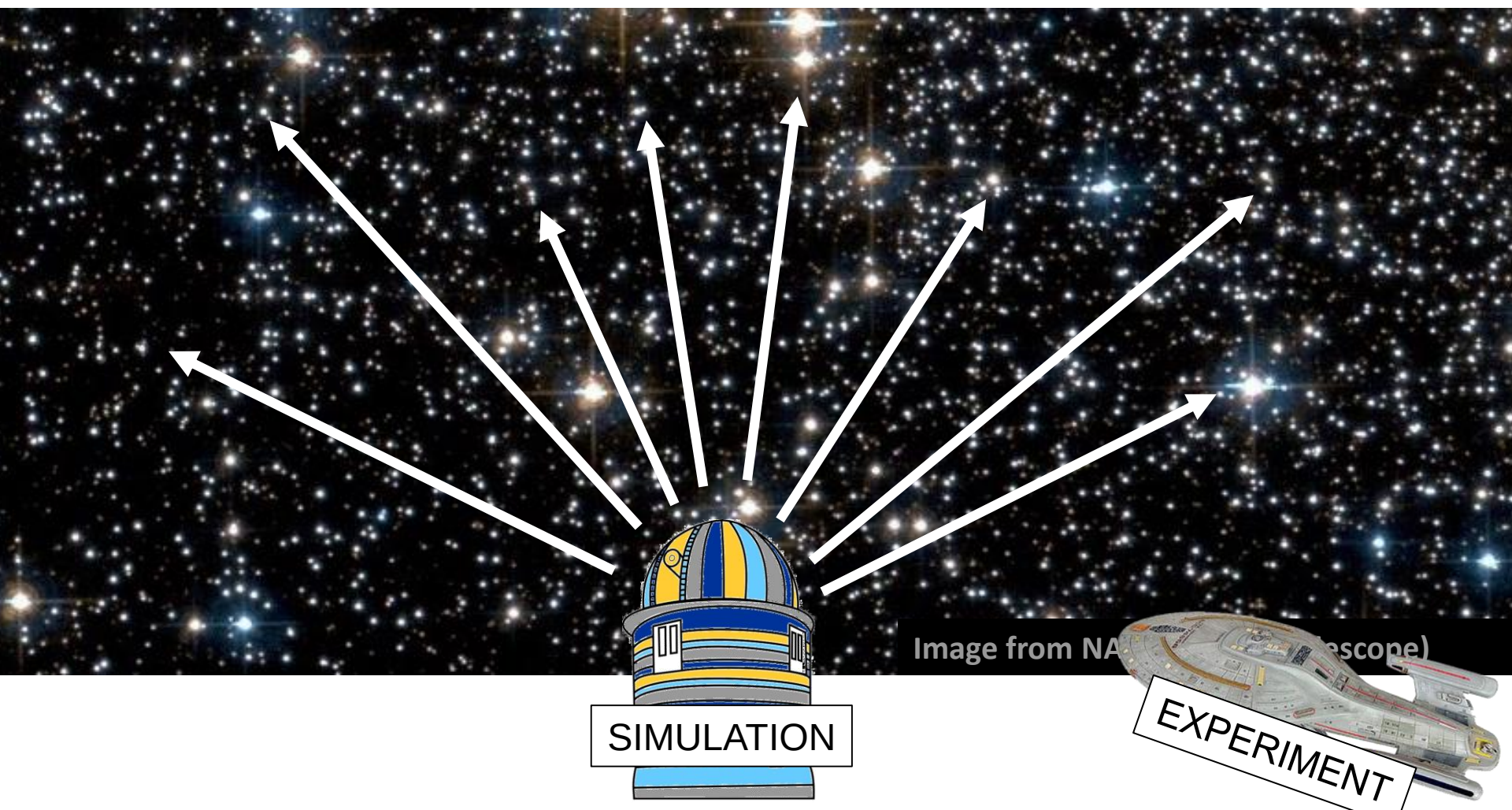
Vision: Map of Chemical Space

How do you navigate?



Vision: Map of Chemical Space

→ MATERIALS INFORMATICS



Thank you for your attention!

