

# Data Assessments for the ALLEE Project

M. Schick, K. Hack

GTT Workshop, Herzogenrath  
June 29<sup>th</sup> – July<sup>st</sup> 2016



# Outline:

## The binary system Al-Zr:

- $C_p(T)$ -curves of  $\text{Al}_3\text{Zr}$  &  $\text{AlZr}$  (Neumann-Kopp)
- Refinement of the Neumann-Kopp approach and comparison to exp. data
- Optimisation of the binary system Al-Zr using improved  $c_p$  functions

## Refinement procedure applied to further compounds

- $\text{Al}_3\text{Ni}$ , “ $\text{Al}_{13}\text{Fe}_4$ ” and “ $\text{Al}_{10}\text{Fe}_3\text{Ni}$ ”

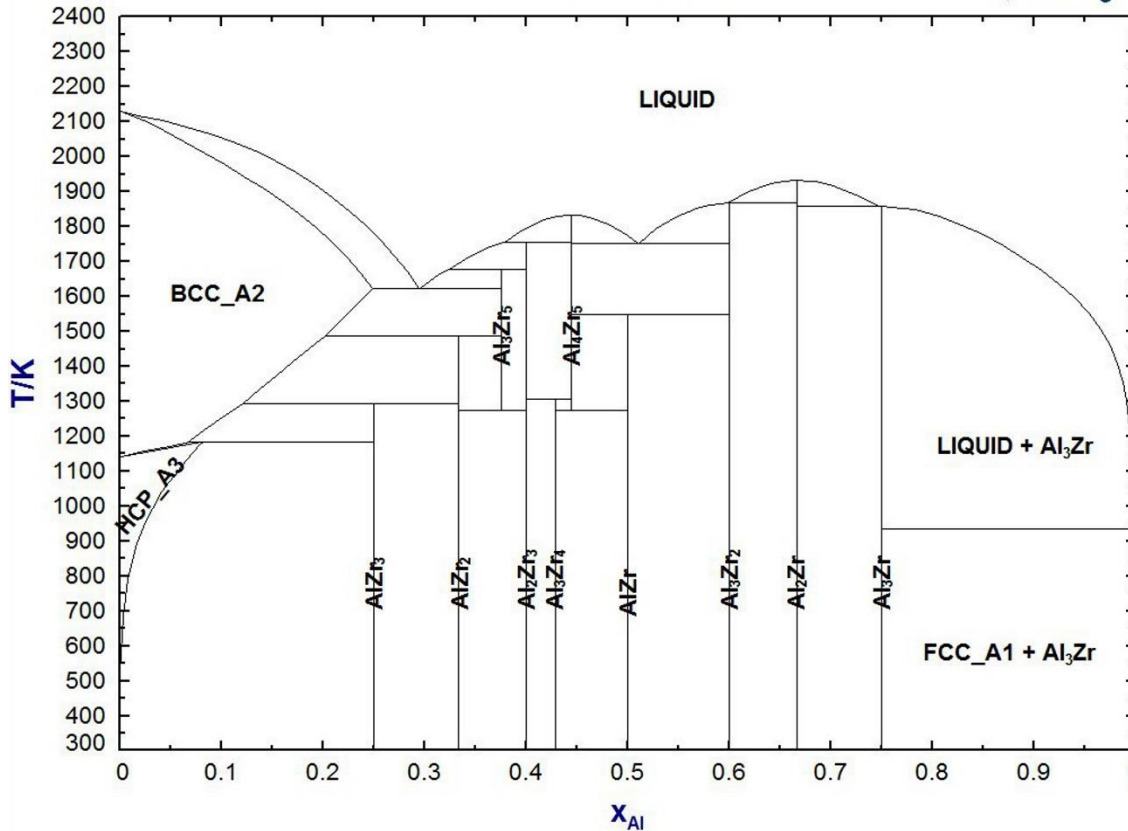
## Evaluation of recent publication by Q. Zhao et al.<sup>1</sup>:

*Influences of Fe, Si and homogenization on electrical conductivity and mechanical properties of dilute Al-Mg-Si alloy*



# The binary system Al-Zr:

Al - Zr  
1 bar, Wang et al. (2001)



**new thermodynamic assessment for binary Al-Zr from literature:**

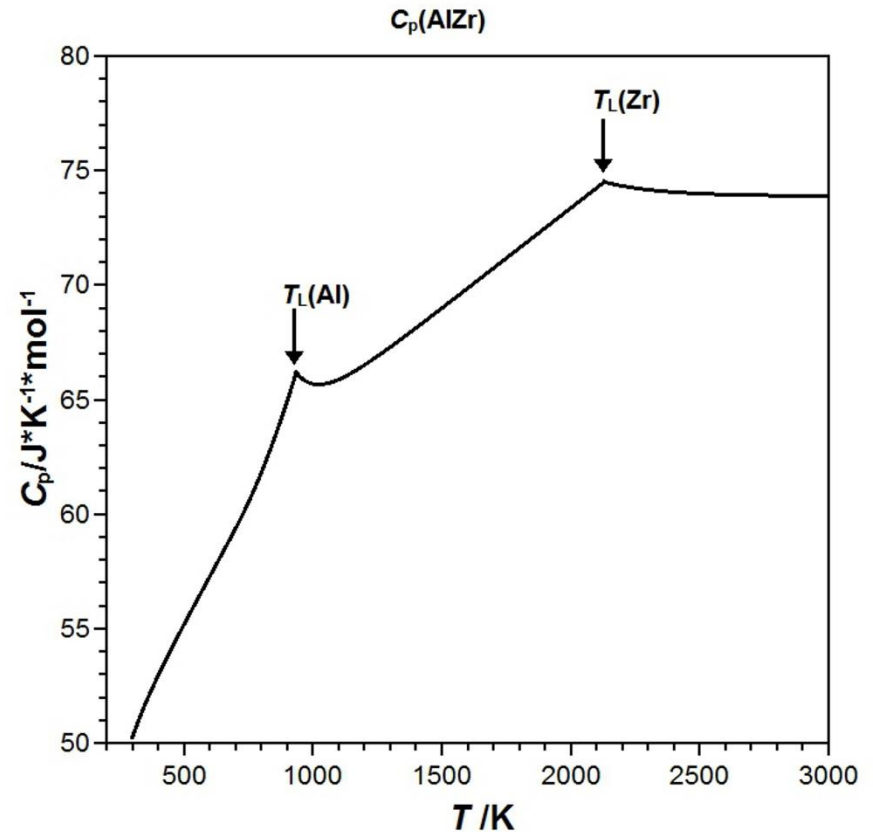
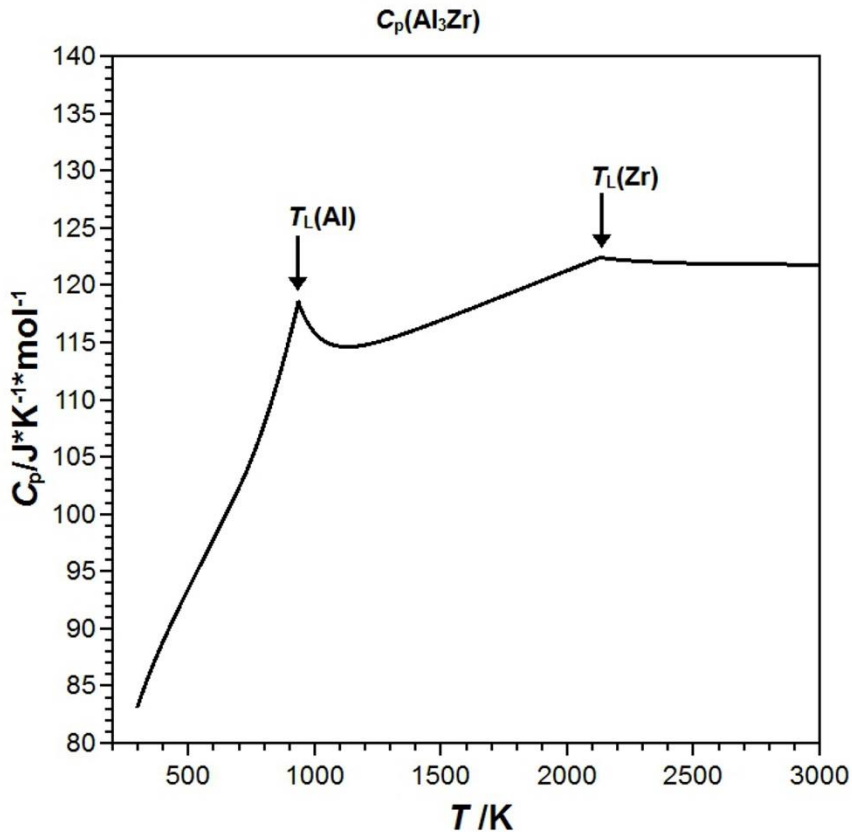
**T. Wang, Z. Jin, J.-C. Zhao, Journal of Phase Equilibria 22(5) (2001) 544**

**10 stoichiometric compounds,  $c_p(T)$  curves obtained with Neumann-Kopp approach**



# The binary system Al-Zr:

## $c_p(T)$ curves, examples ( $\text{Al}_3\text{Zr}$ , $\text{AlZr}$ ) :



melting points of pure elements  $\Rightarrow$  artefacts in  $c_p$  curves





# Refinement of Neumann-Kopp:

if no further data available:

procedure of refinement

1. refit  $c_p$ -curve with (standard) polynomial function:

$$c_p = a_0 + a_1 \cdot T + a_2 \cdot T^{-2} + a_3 \cdot T^2 + (a_4 \cdot T^3)$$

2. recalculate melting temp. (peritectic temp.) of compound (optimisation of  $\Delta H_f^{298}$  and  $S^{298}$ )
3. recalculate invariant equilibria where compound is involved

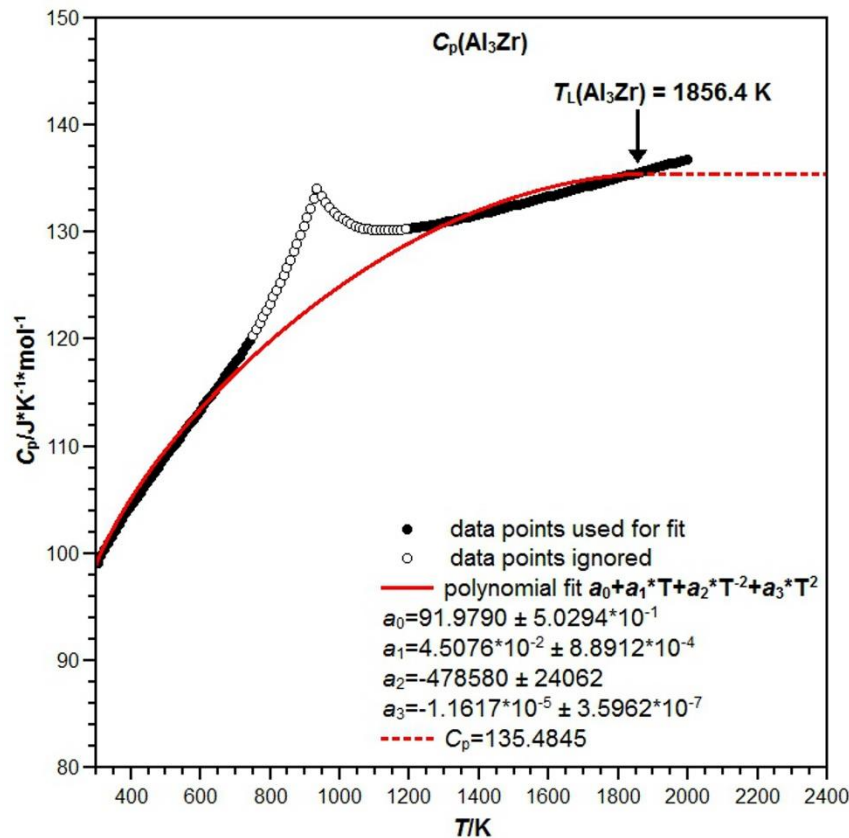


# Refinement of Neumann-Kopp:

GTT-Technologies

## $C_p$ refit for $\text{Al}_3\text{Zr}$ :

melting temperature:  $T_L = 1856.4$  K (Wang et al., N-K  $C_p$ )



2 temperature ranges for  $C_p$ :

polynomial function  
 $298.15 \text{ K} - T_L$

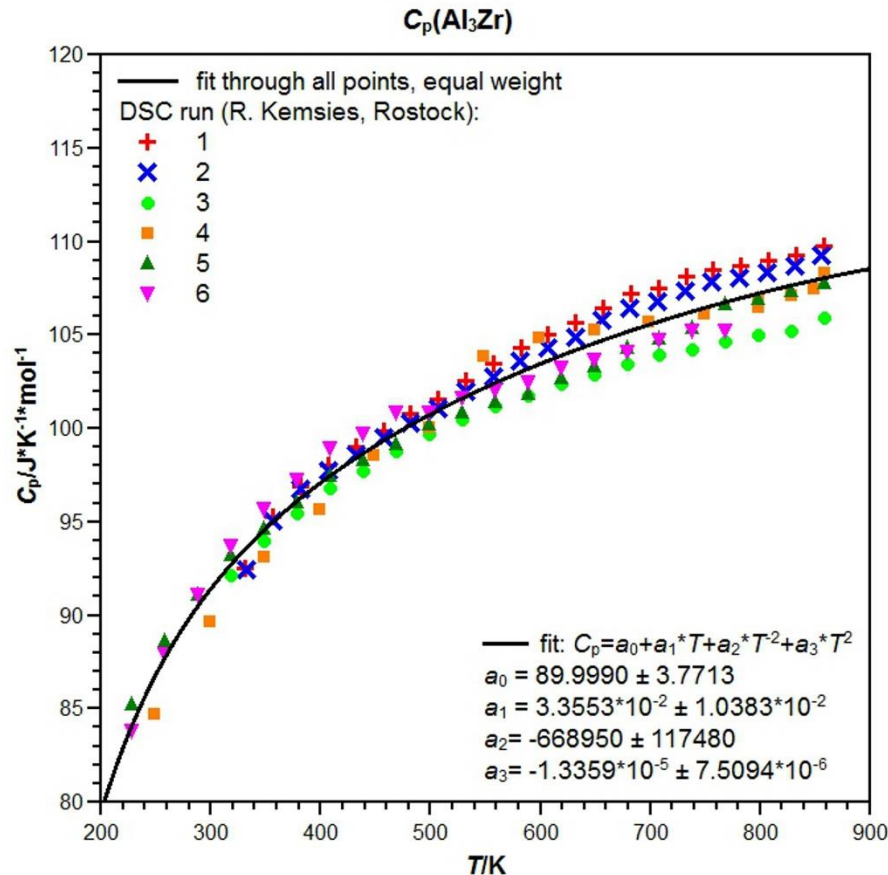
$C_p = \text{const. for } T > T_L$



# Experimental data for $C_p$ :

GTT-Technologies

$C_p$  measurements for  $\text{Al}_3\text{Zr}$  by R. Kemsies, Rostock:



exp. data fitted nicely  
by standard polynomial  
function for  $C_p$ , but:

maximum temperature for  
exp. data quite low  
( $T_{\text{max}} = 858 \text{ K}$ ),

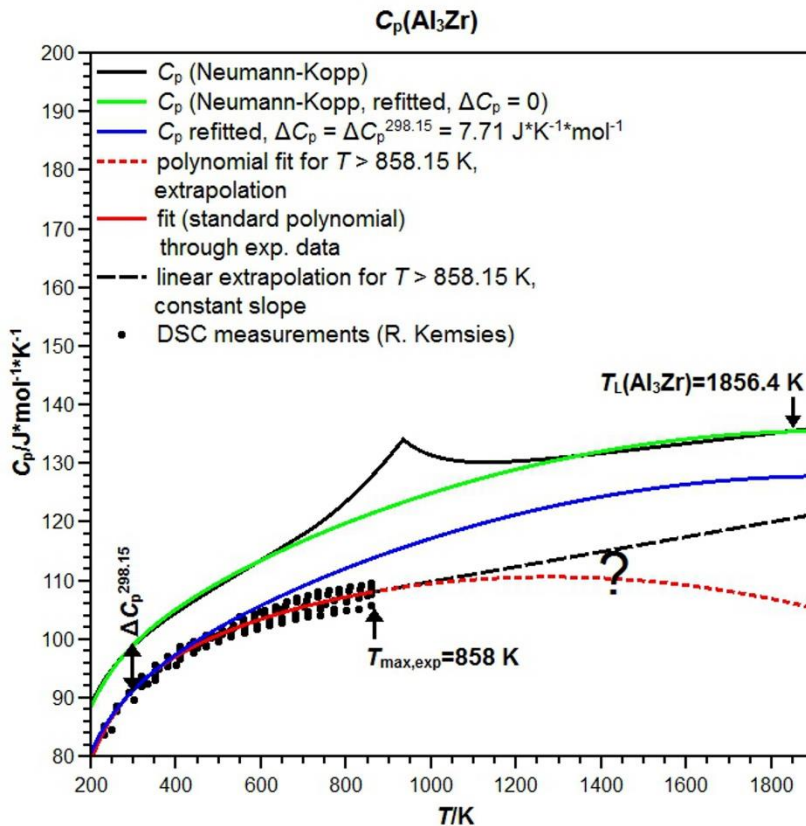
melting temperature rather  
high ( $T_L = 1856.4 \text{ K}$ )

no exp. data in the range  
between 858 – 1856 K !



# Experimental data for $C_p$ :

comparison between simple and refined Neumann-Kopp approach, and experimental data for  $C_p(\text{Al}_3\text{Zr})$



**problem:**

**no exp. data available in the range between 858 –1856 K !**

**possible way:**

**linear extrapolation of  $C_p(T)$  curve with constant slope**

$$\left( \frac{dC_p}{dT} \right) = \left( \frac{dC_p}{dT} \right)_{T=298.15} = \text{const.}$$

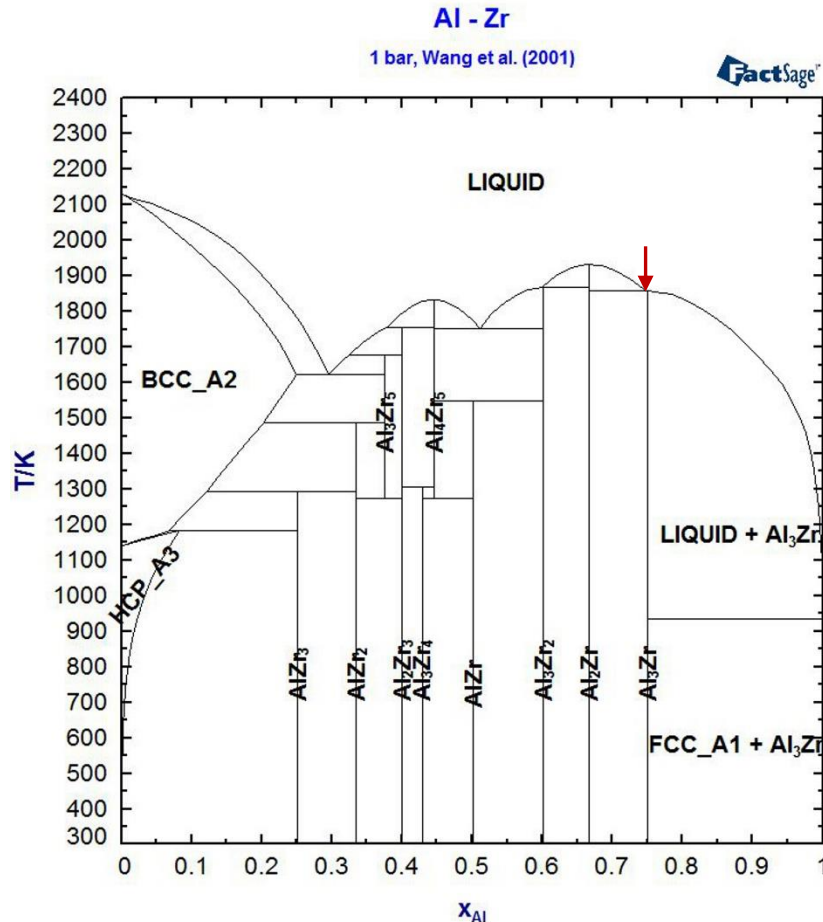
**another possible way:**

**use of *ab-initio* data (planned)**



# Optimisation:

optimisation of  $\Delta H_f^{298}$  and  $S^{298}$  for refitted function  $C_p(T)$ :



⇒ match melting temperature

⇒ match invariant equilibria, where  $\text{Al}_3\text{Zr}$  is involved

with  $C_p(T)$ ,  $\Delta H_f^{298}$ ,  $S^{298}$  fixed  
⇒ Gibbs energy is defined !



# Optimisation:

## Comparison of invariant equilibria involving Al<sub>3</sub>Zr:

<i>inv. equilibrium</i>	<i>T/K (Wang et al.)</i>	<i>T/K (after opt.)</i>
Liquid $\rightleftharpoons$ Al <sub>2</sub> Zr + Al <sub>3</sub> Zr	1856.2	1857.7
Liquid $\rightleftharpoons$ Al <sub>3</sub> Zr	1856.4	1858.6
Liquid + Al <sub>3</sub> Zr $\rightleftharpoons$ FCC_A1	933.8	933.8

## Comparison of $\Delta H_f^{298}$ values for Al<sub>3</sub>Zr<sup>1</sup> and Al<sub>2</sub>Zr<sup>1</sup>:

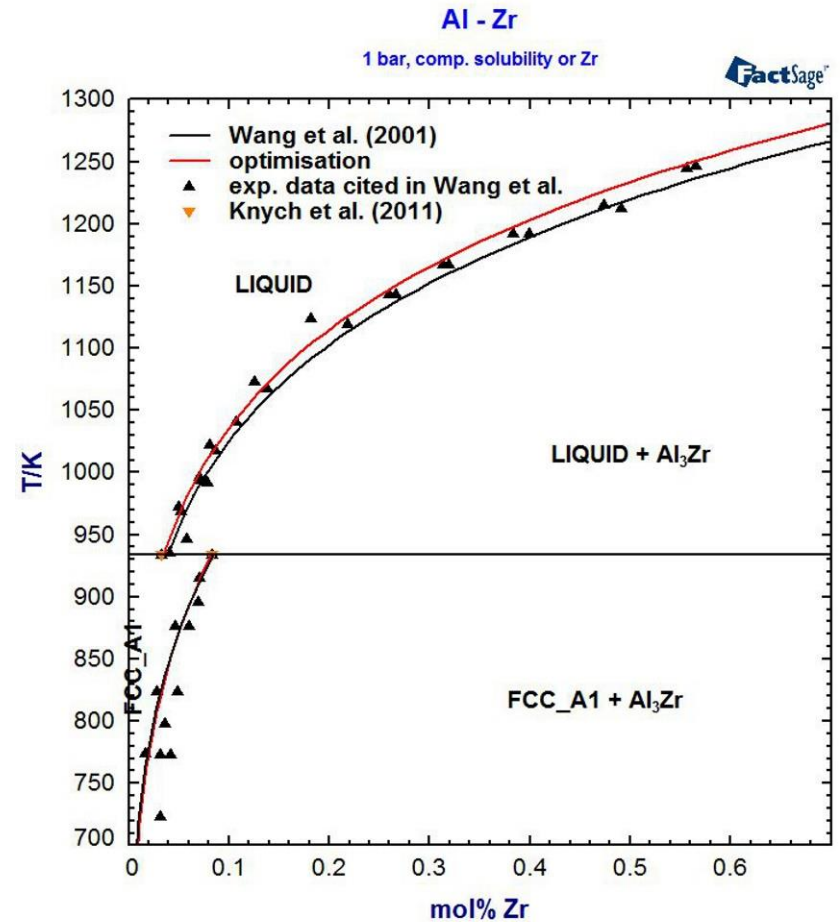
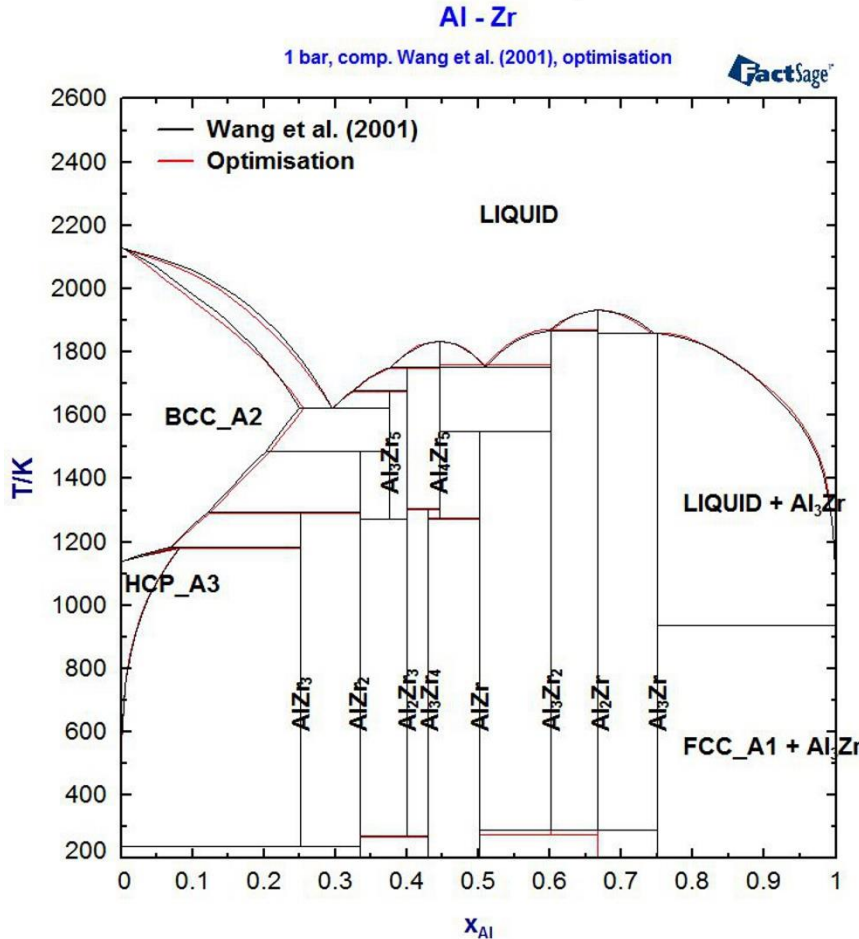
compound	optimised <i>kJ*mol(at)<sup>-1</sup></i>	Colinet <sup>1</sup>		
		<i>VASP</i>	<i>DSC</i>	<i>Calomtr.</i>
Al <sub>3</sub> Zr	-47.5	-46.97	-48.4	-44.4
Al <sub>2</sub> Zr	-55.3	-52.02	-52.1	-49.0





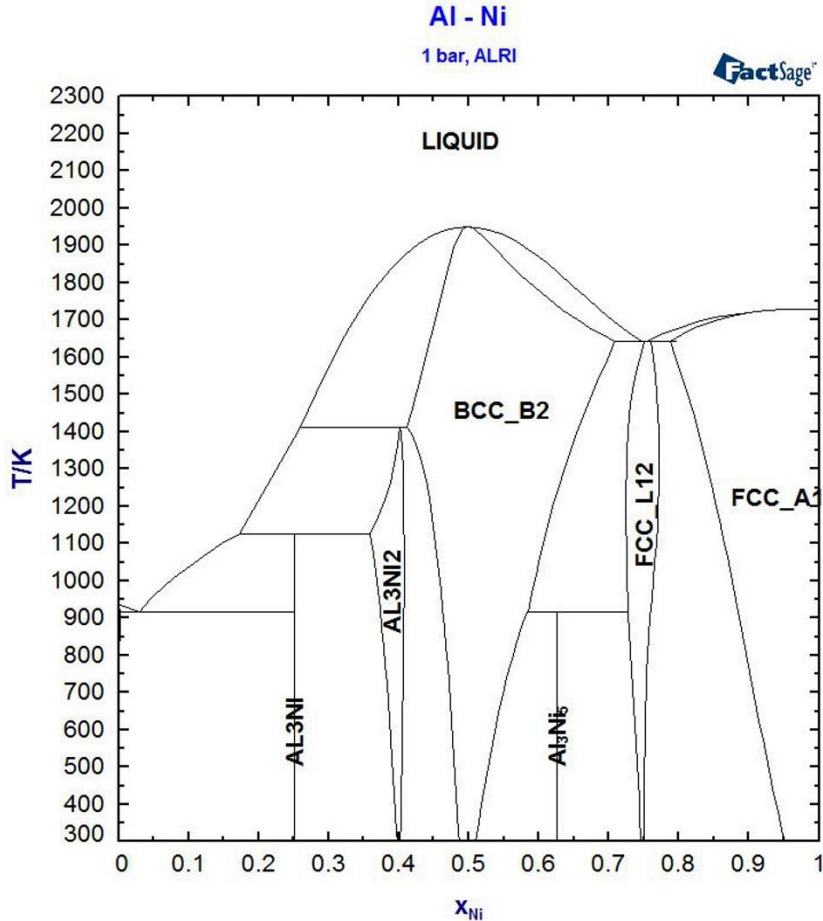
# Optimisation:

## binary system Al-Zr optimised with improved $c_p(\text{Al}_3\text{Zr})$ and solubility of Zr in Al(fcc) and LIQUID<sup>2</sup>

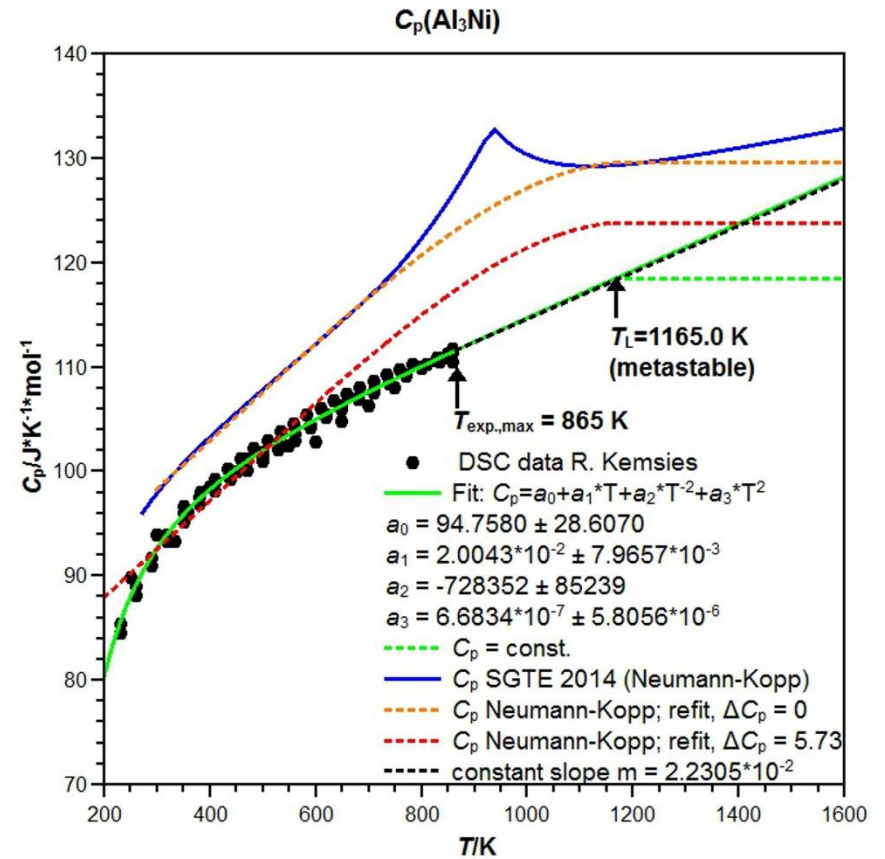


# The binary system Al-Ni:

## binary phase diagram:



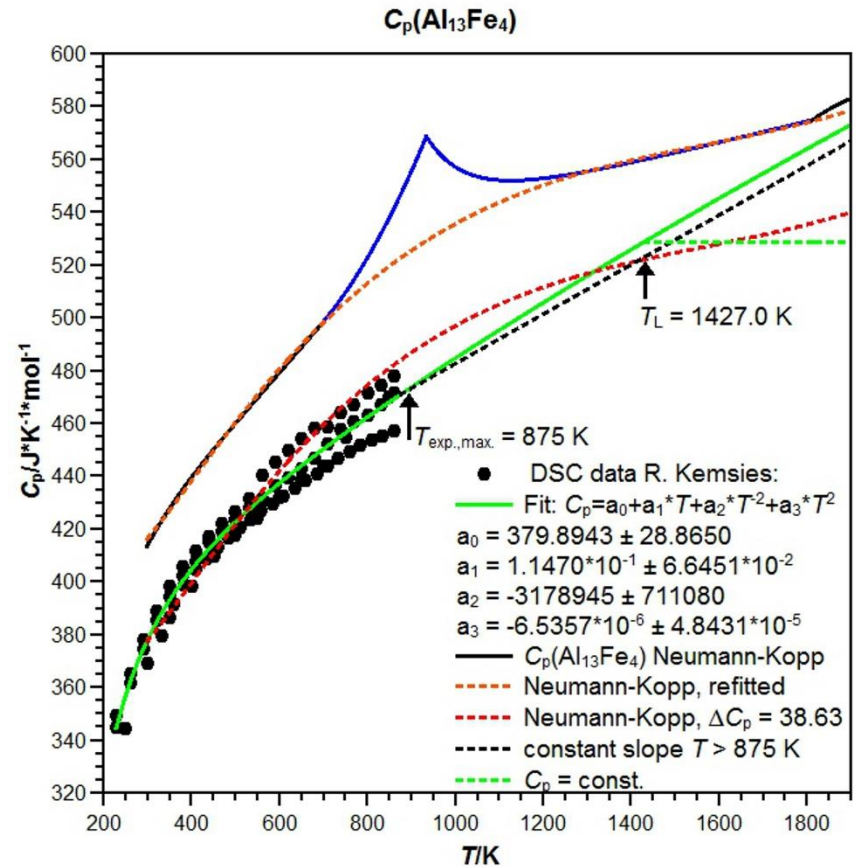
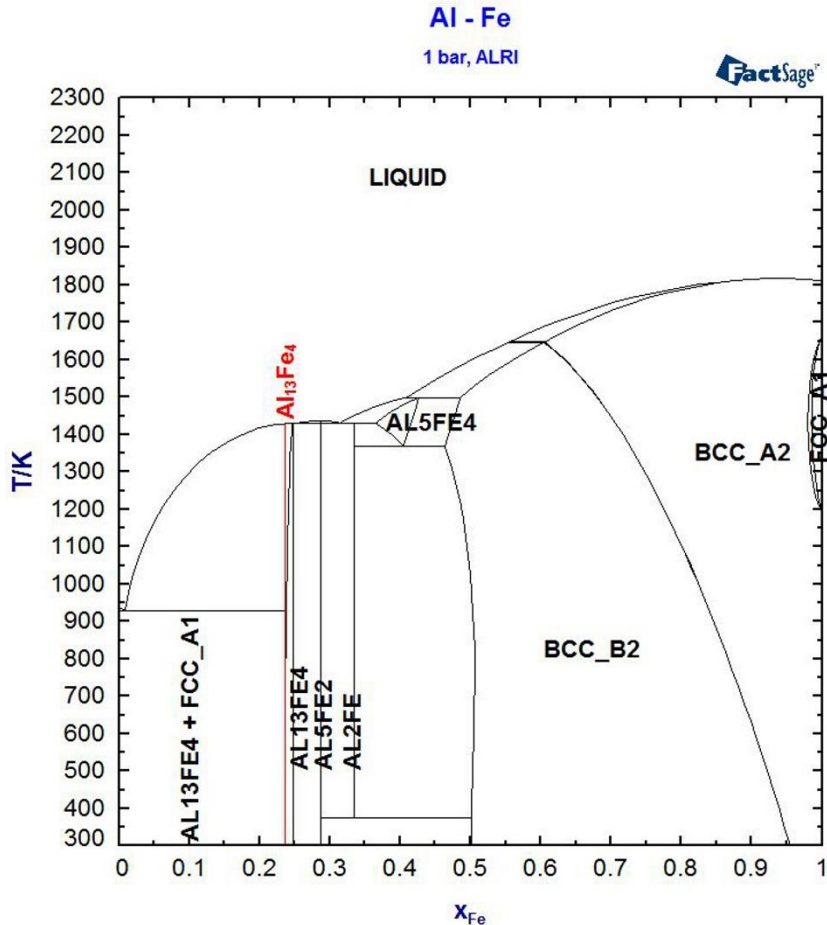
## heat capacity $c_p(\text{Al}_3\text{Ni})$ :





# The binary system Al-Fe:

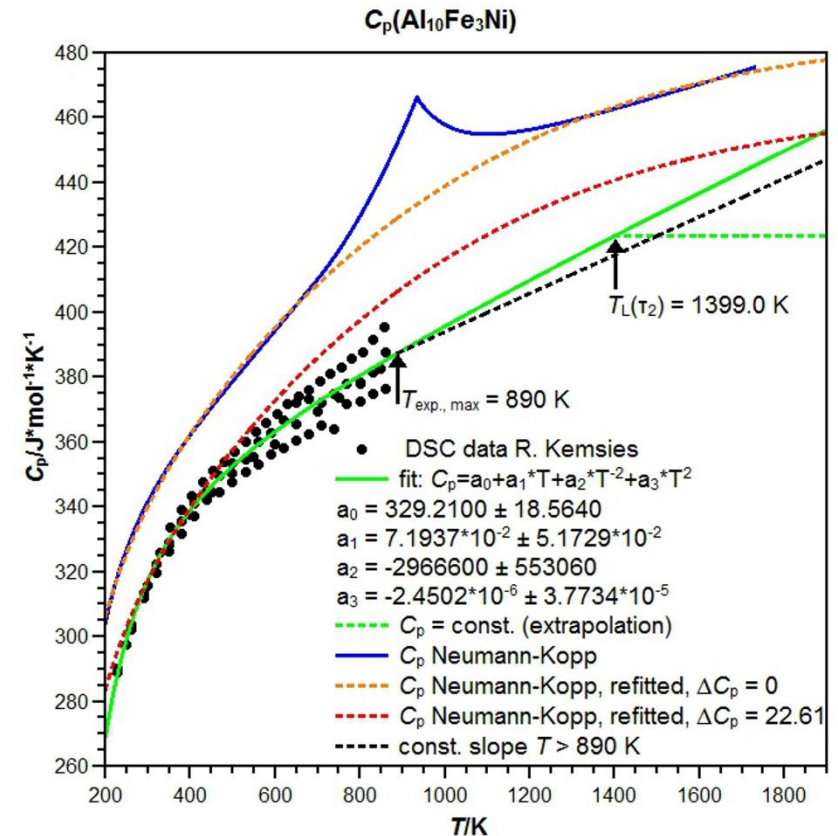
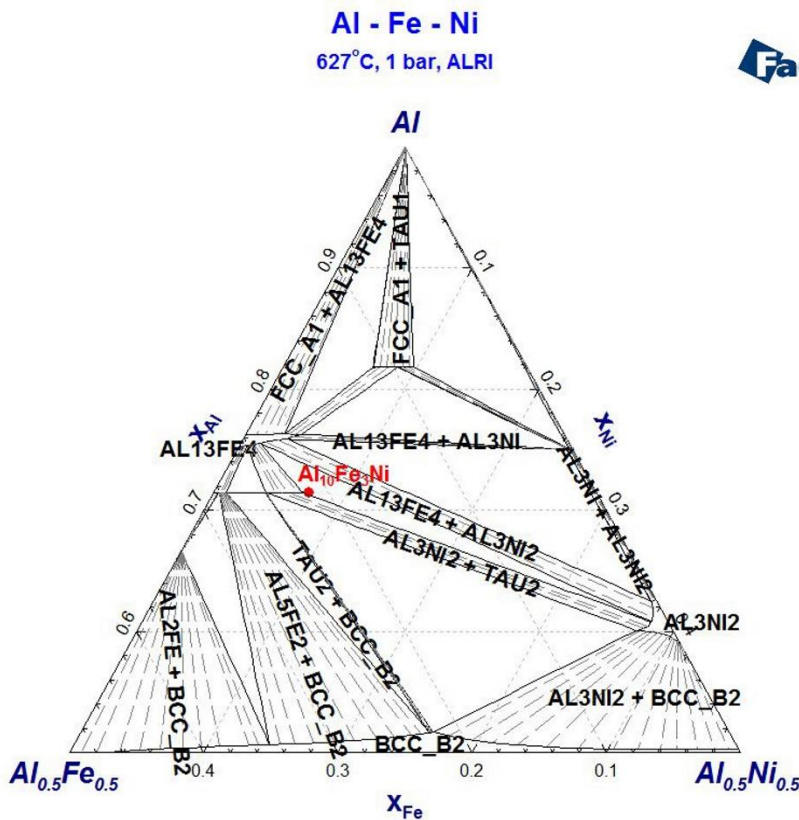
**AL13FE4 is non-stoichiometric (solution phase),  
modelled  $(Al)_{32}(Fe)_{12}(Al, Va)_7$**



# The ternary compound $\text{Al}_{10}\text{Fe}_3\text{Ni}$ :

GTT-Technologies

composition  $\text{Al}_{10}\text{Fe}_3\text{Ni}$  corresponds to non-stoichiometric phase  $\tau_2 = \text{Al}_5(\text{Fe,Ni})_2$  (line compound) in Al-Fe-Ni



# Data assessment: Fe in Al-Mg-Si:

## Publication found recently:

*Influences of Fe, Si and homogenization on electrical conductivity and mechanical properties of dilute Al-Mg-Si alloy*

Q. Zhao, Z. Qian, X. Cui, Y. Wu, X. Liu, JALCOM 666 (2016) 50

⇒ Of interest: influence of Fe on the solubility of Si in Al(fcc) and LIQUID

⇒ Authors argue:  
ternary eutectic phase  $\alpha\text{-Al}_8\text{Fe}_2\text{Si}$  is formed upon solidification, which leads to improved electrical & mechanical properties



# Data assessment: Fe in Al-Mg-Si:

## Sample preparation:

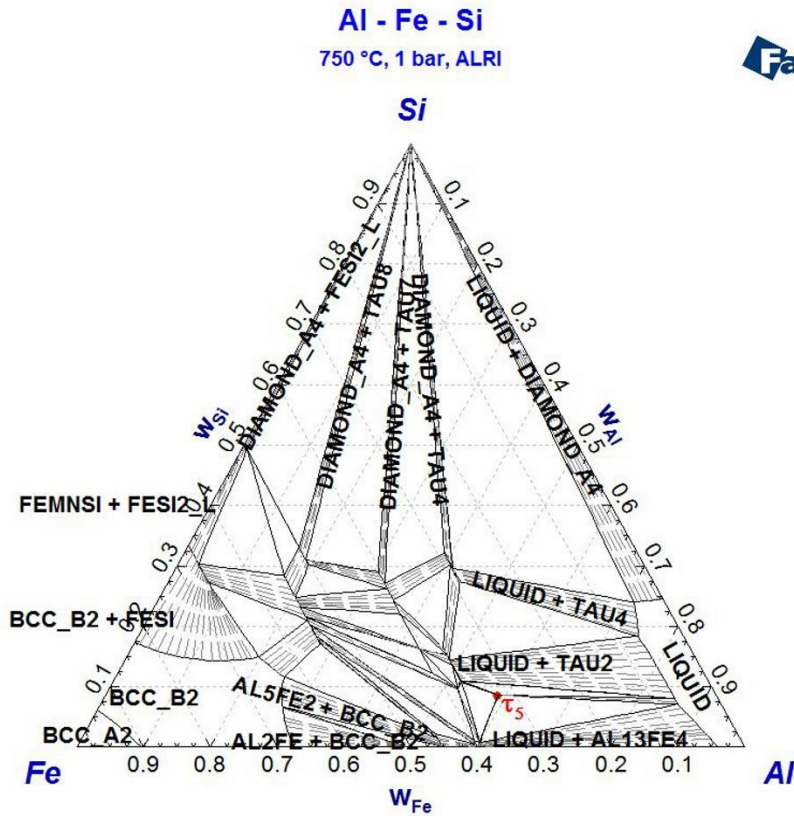
1. melting together pure elements,  $T = 750^{\circ}\text{C}$
2.  $T = 720^{\circ}\text{C}$ , 10 min., slag removing
3. casting, mould temp. ( $200^{\circ}\text{C}$ ), solidification
4. heating  $T = 510^{\circ}\text{C}$ , 2h, quenching (water)
5. “Ageing”:  $T = 175^{\circ}\text{C}$ , 9h, cooling (air)
6. “homogenisation”,  $T \approx T_{\text{L}}^{\text{Al}}$  ( $660^{\circ}\text{C}$ ), time ?

<i>sample</i>	$W_{\text{Al}}$	$W_{\text{Fe}}$	$W_{\text{Mg}}$	$W_{\text{Si}}$
1	0.9915	0.0000	0.0050	0.0035
2	0.9905	0.0010	0.0050	0.0035
3	0.9895	0.0020	0.0050	0.0035
4	0.9890	0.0020	0.0050	0.0040
5	0.9885	0.0020	0.0050	0.0045
6	0.9880	0.0020	0.0050	0.0050

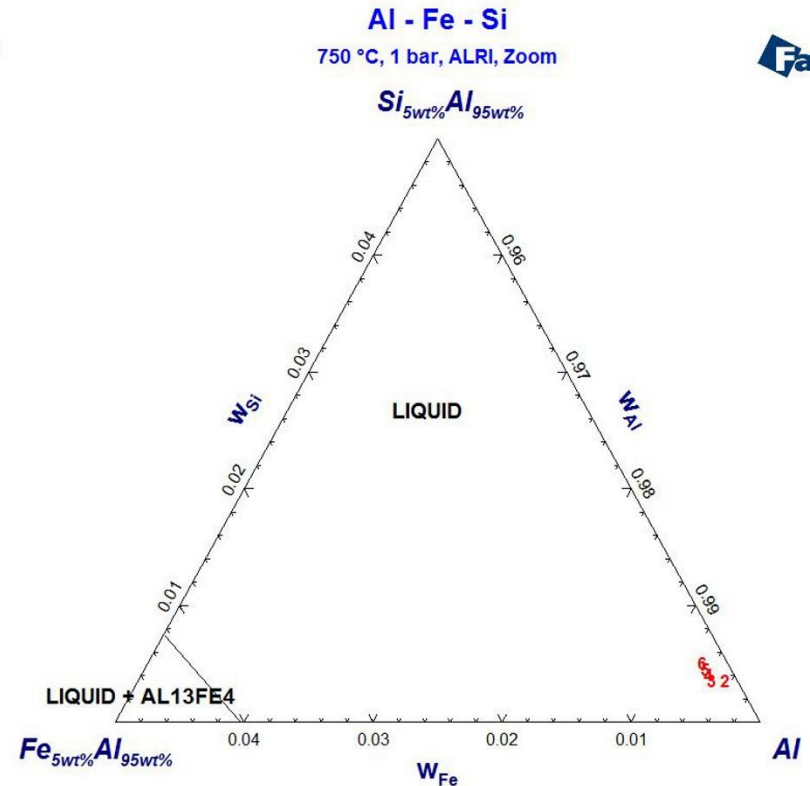
# Data assessment: Fe in Al-Mg-Si:

GTT-Technologies

ternary eutectic phase  $\alpha\text{-Al}_8\text{Fe}_2\text{Si}$  ( $\cong \tau_5$ )  
is stable at  $T = 750^\circ\text{C}$



FactSage™



FactSage™

compositions: samples 2-6,  
sample 1: Fe free





# Data assessment: Fe in Al-Mg-Si:

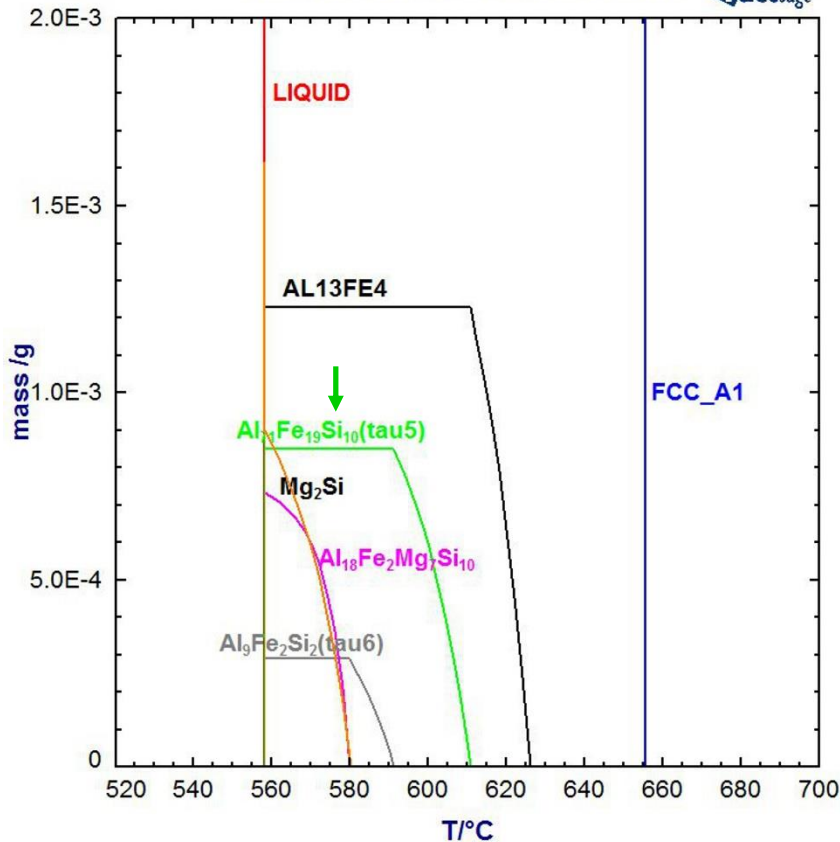
GTT-Technologies

does  $\alpha\text{-Al}_8\text{Fe}_2\text{Si}$  ( $\cong \tau_5$ ) form during casting & solidification?

Scheil cooling calculation ALRI, sample #2

0.9905g Al + 0.001g Fe + 0.005g Mg + 0.0035g Si

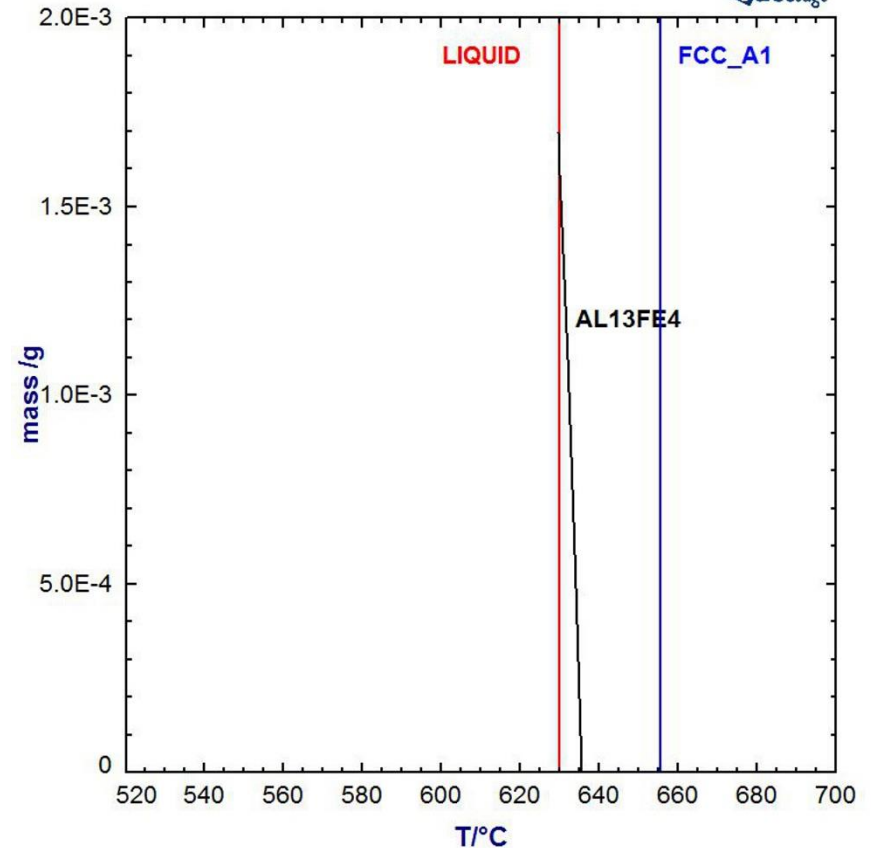
FactSage



Equilibrium cooling calculation, ALRI, sample #2

0.9905g Al + 0.001g Fe + 0.005g Mg + 0.0035g Si

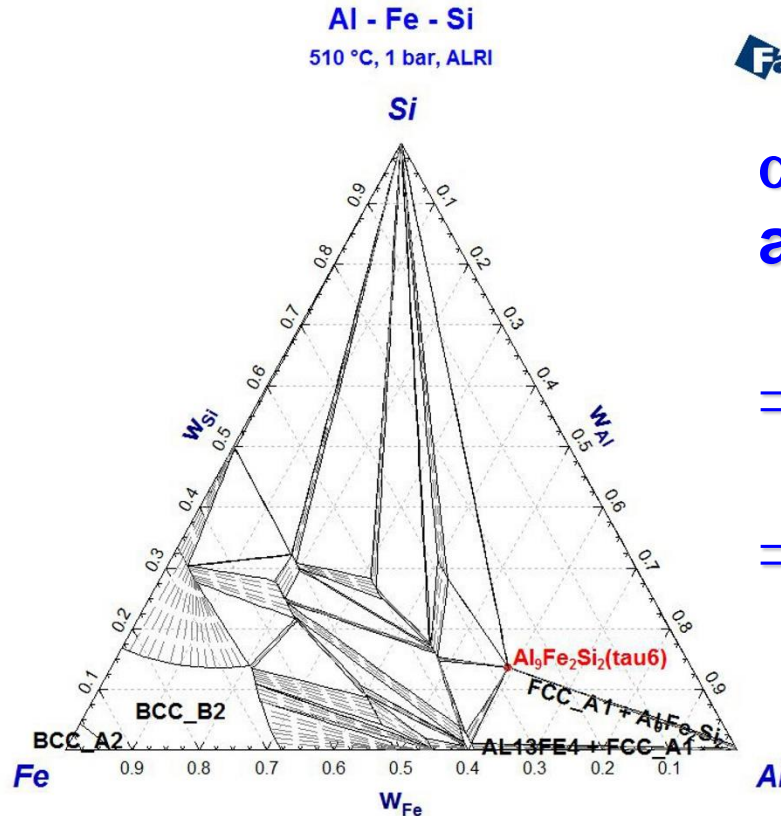
FactSage



# Data assessment: Fe in Al-Mg-Si:

GTT-Technologies

## Annealing at $T = 510^\circ\text{C}$ :



FactSage™

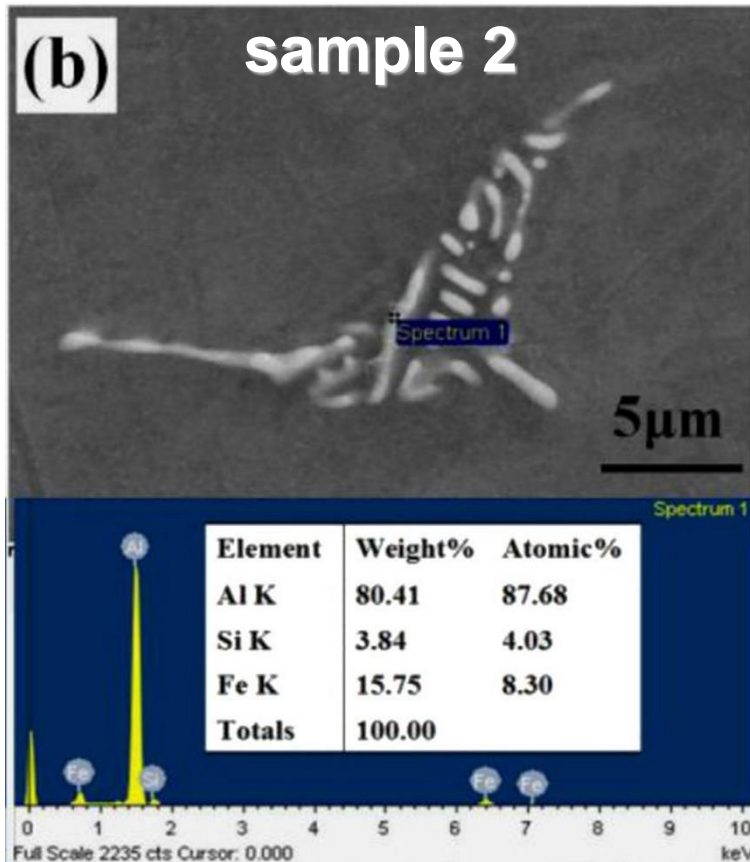
$\alpha\text{-Al}_8\text{Fe}_2\text{Si}$  ( $\cong \tau_5$ ) is not stable  
any more  $\Rightarrow \text{Al}_9\text{Fe}_2\text{Si}_2$  ( $\cong \tau_6$ ) !

$\Rightarrow$  upon annealing  $\tau_5$  may  
react to form stable phases  
 $\Rightarrow$  sample compositions in  
three phase region:  
DIAMOND\_A4 + FCC\_A1 +  $\tau_6$



# Data assessment: Fe in Al-Mg-Si:

The authors want to prove formation of phase  $\alpha\text{-Al}_8\text{Fe}_2\text{Si}$  by EDS:



composition of phase  $\alpha\text{-Al}_8\text{Fe}_2\text{Si}$  according to formula:

	Al	Fe	Si
mole%	72.73	18.18	9.10
weight%	60.69	31.40	7.90

**none of the EDS analyses matches nominal composition !  
⇒ no experimental proof for existence of  $\alpha\text{-Al}_8\text{Fe}_2\text{Si}$**



**Thanks for your attention !**

