

Thermodynamics of Lithium Battery Materials

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Institute for Applied Materials – Applied Materials Physics (IAM-AWP)



Thermodynamics of Lithium Battery Materials

- Introduction
- Why battery thermodynamics and phase diagrams?
Calculation of voltages, ...
- Calorimetry of lithium ion batteries
Isothermal and adiabatic calorimetry
- Li – Mn – O and Li – Fe – P – O materials systems

Electric vehicles - some examples



Mini E

(L.A., NY, Berlin; BMW / Vattenfall)
Operating range 250 km



Smart electric drive

(London, Berlin; Daimler / RWE)
Operating range 135 km

Electric vehicles - some examples



i MiEV, Mitsubishi

Capacity of Battery: 16 kWh (200kg)
150 km operating range

Per single cell: Energy density 218 Wh/l and
Specific energy 109 Wh/kg; Specific power 550 W/kg
Total of 176 Cells in Battery System

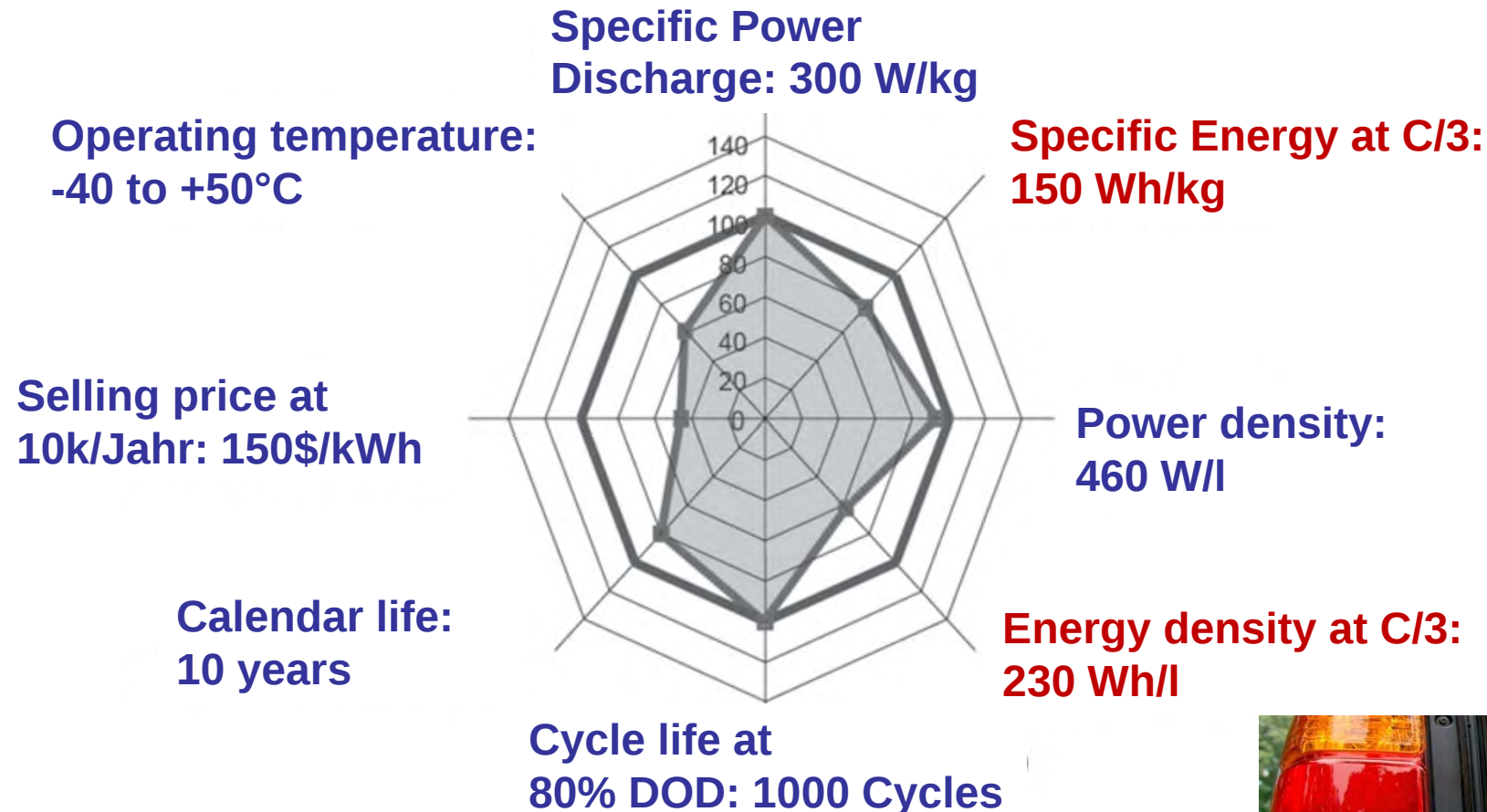
**Energy stored in 100 kg of best commercial batteries
good enough for just 100 km operating range**

**Batteries for Electric Vehicles have to be optimized to
high energy density (kWh), save thermal behavior and cycle life**

**Energy density (Wh/l) and
specific energy (Wh/kg)
determine for a given operating range
the volume and mass of battery**



Battery technology spider chart (USABC) for electrical vehicles (EV)



Sources:

- (1) D. Howell, Energy Storage Research and Development, Annual Progress Report 2006 (Washington, D.C.: Office of FreedomCAR and Vehicle Technologies, U.S. Department of Energy, 2007)
- (2) FreedomCAR and Fuel Partnership and **United States Advanced Battery Consortium (USABC)**, Electrochemical Energy Storage Technical Team Technology Development Roadmap (Southfield, MI: USCAR, 2006)



Why Battery Thermodynamics and Phase Diagrams?

Thermodynamics and phase diagrams govern battery performance

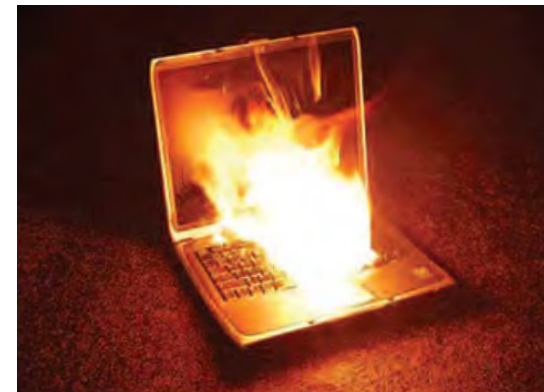
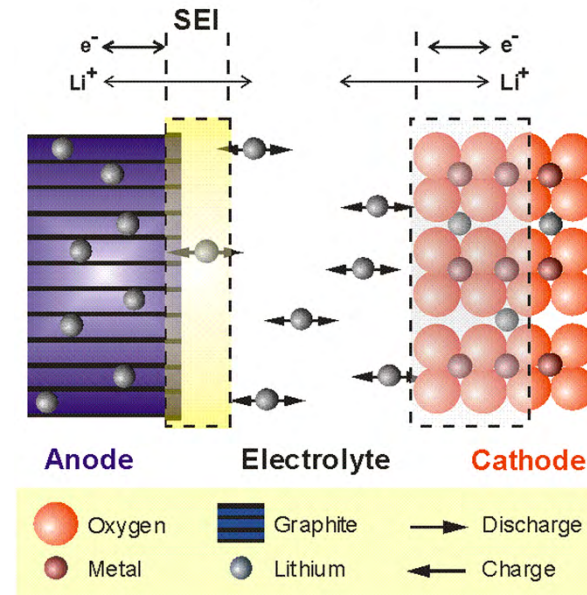
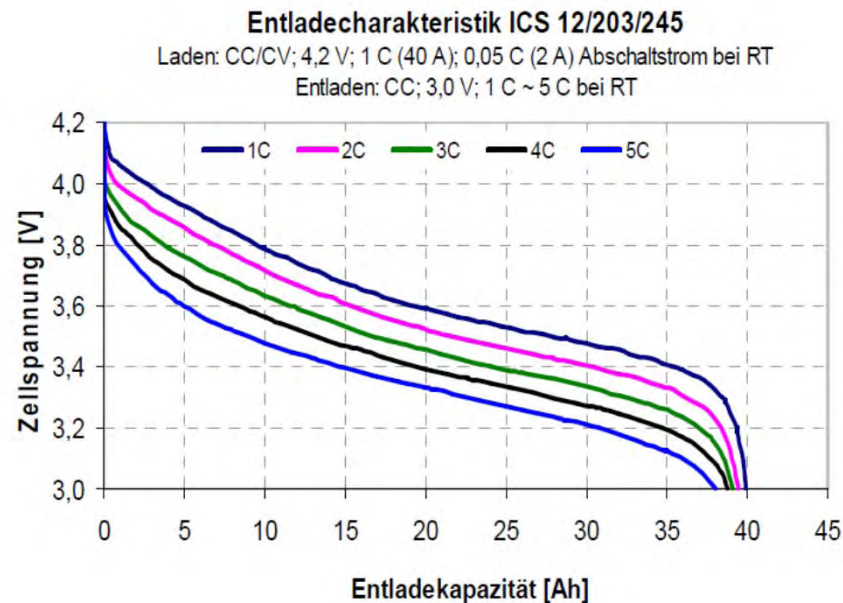
Thermal management of batteries (Heat dissipation and temperature distribution)

Battery safety (thermal runaway)

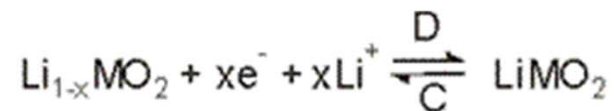
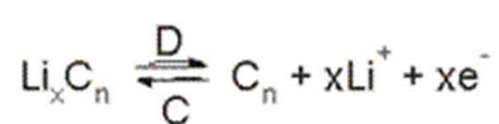
Structural changes in active materials

Surface energies (nano-micro)

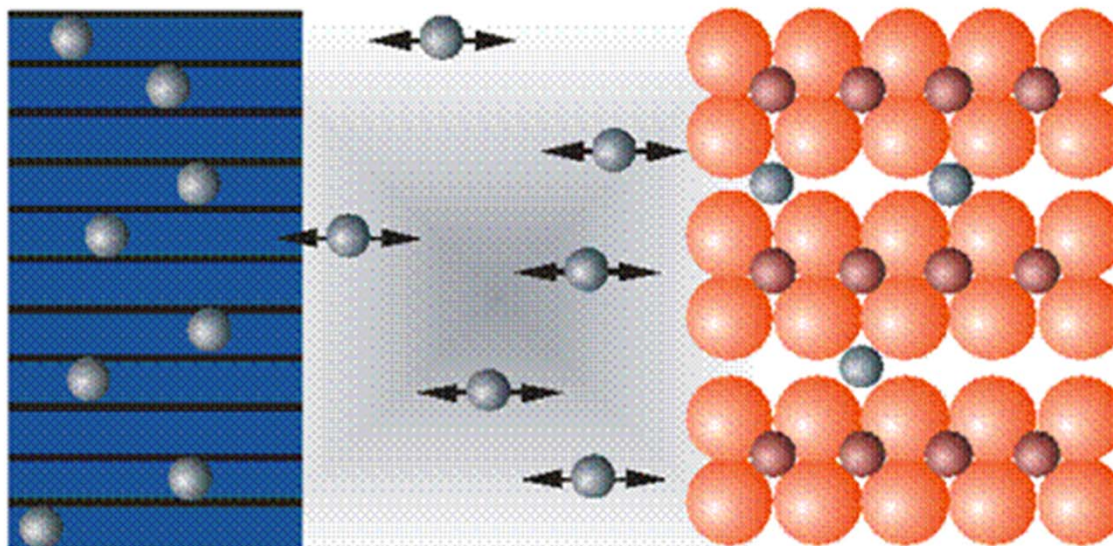
Synthesis of complex ceramic materials



Lithium Ion Batteries – Operation



Graphite

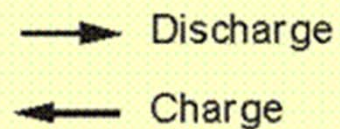
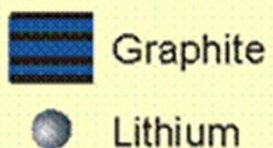
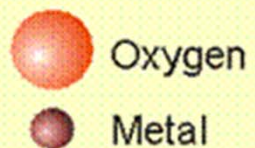


LiCoO₂

Negative Electrode
"Anode"

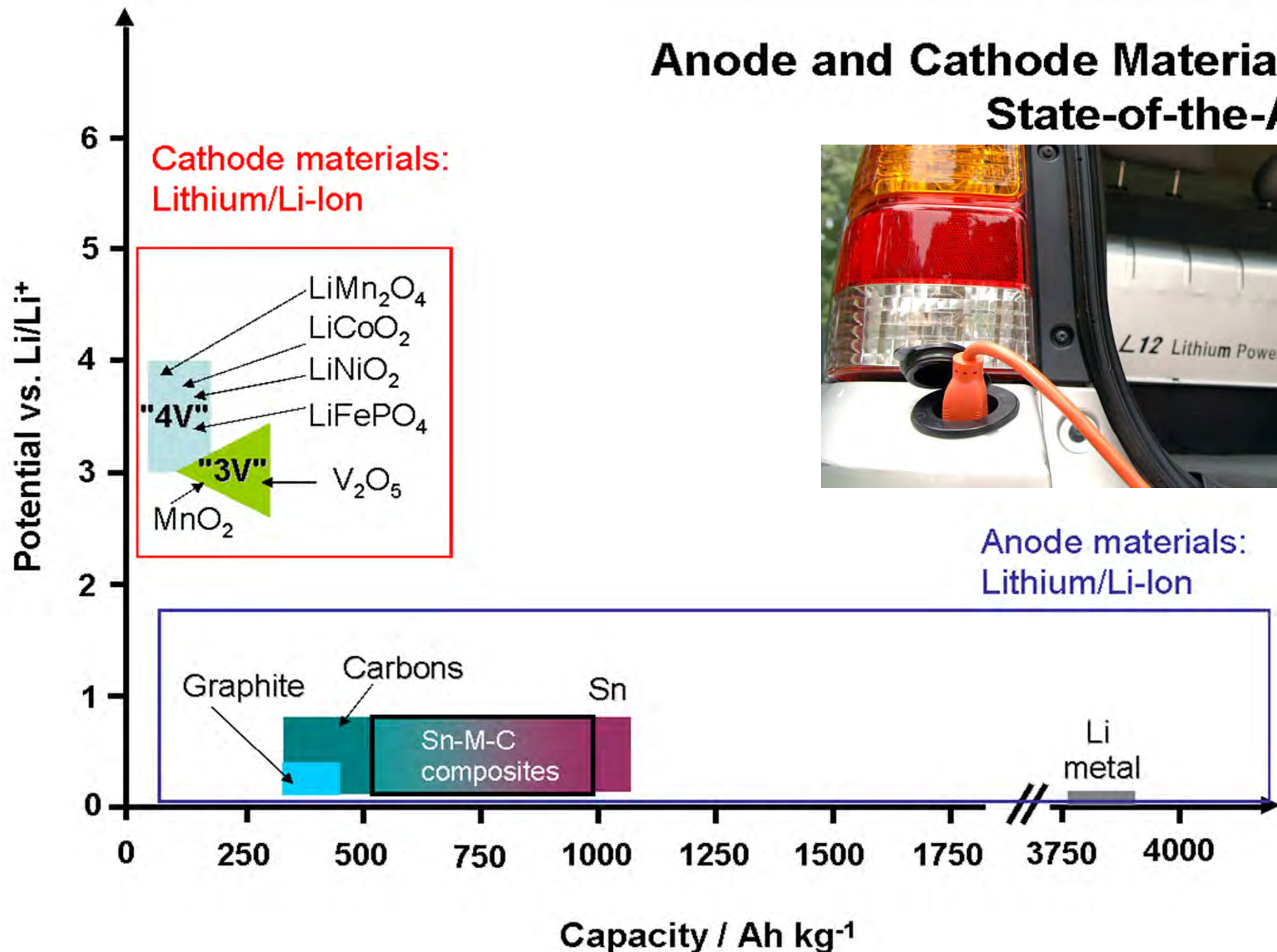
Electrolyte

Positive Electrode
"Cathode"



Presently: Anode: graphitic C; Electrolyte: LiPF₆ in organic carbonate solvents; Cathode: Co-based LiMO₂

Anode and Cathode Materials: State-of-the-Art



Source: M. Winter, Univ. Münster

**German Research Foundation, Priority Programme 1473
Materials with New Design for Improved Lithium Ion Batteries -
WeNDeLIB**

**DFG Schwerpunktprogramm 1473, Kick-Off-Treffen,
Werkstoffe mit neuem Design für verbesserte Lithium-Ionen-Batterien - WeNDeLIB**

Started in October 2010

Program Commission:

Hans Jürgen Seifert	Karlsruher Institut für Technologie (Chair)
Rainer Schmid-Fetzer	Technische Universität Clausthal (Co-Chair)
Martin Winter	Universität Münster (Co-Chair)
Nicola Hüsing	Universität Salzburg
Andreas Gutsch	Li-Tec, Kamenz, now with KIT
Bengt Hallstedt	RWTH Aachen
Ingo Steinbach	ICAMS, Bochum



International Member:

Alexandra Navrotsky University of California, Davis

13 joint projects (36 projects in total) + coordinator project

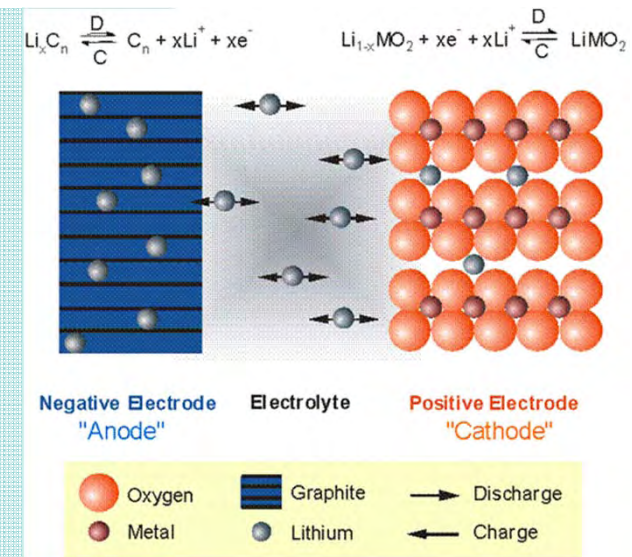
**German Research Foundation, Priority Programme 1473
Materials with New Design for Improved Lithium Ion Batteries -
WeNDeLIB**

Vision of this priority program:

Coupling of materials thermodynamics and kinetics and modelling of materials design for innovative lithium ion batteries

Ideal case:

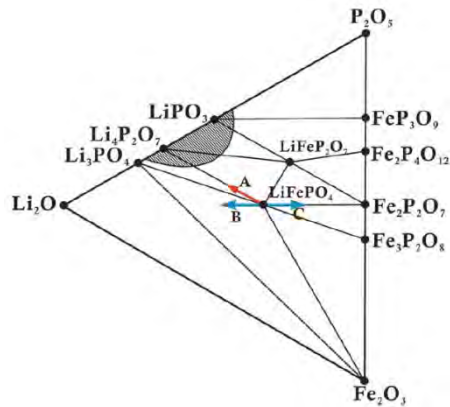
Complete design of battery before the experimental work or processing starts in the lab or in industrial operation



Still a long way to go - We introduce a new *interdisciplinary* concept for LiB (no international program to be compared with this approach)

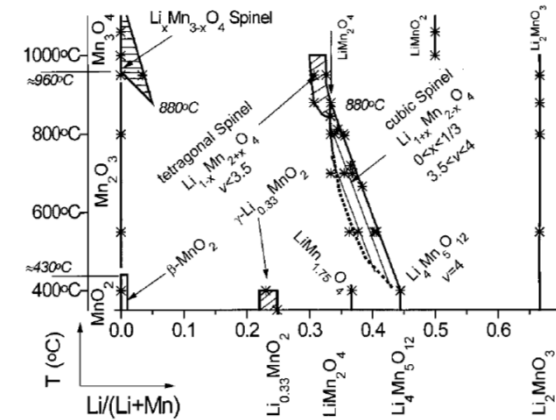
- Scientific Focus -

Interdisciplinary Work – Correlation of:



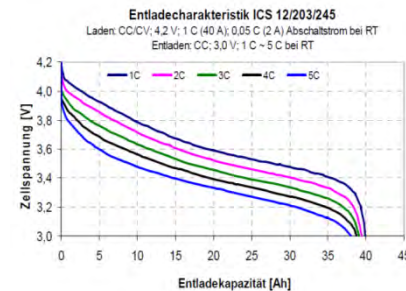
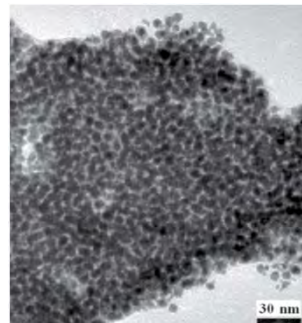
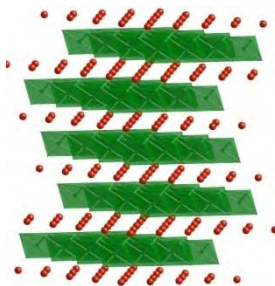
Materials

- Thermodynamics,
- Constitution,
- Kinetics



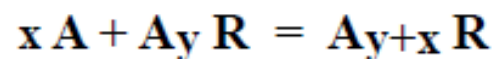
**Crystal chemistry,
Microstructure,
Innovative Materials
Synthesis**

**Electrochemical
performance
and safety of
cells / batteries**



Approach by electrochemical cell reaction equations

Write reaction as



ΔG_r° = Gibbs free energy change due to the reaction

$$= \sum \Delta G_f^\circ(\text{products}) - \sum \Delta G_f^\circ(\text{reactants})$$

This can be related to the cell voltage

$$\Delta G_r^\circ = - z q E$$

z = charge number carried by ions in electrolyte

q = elementary charge per particle

E = externally measurable cell voltage

Approach by electrochemical cell reaction equations

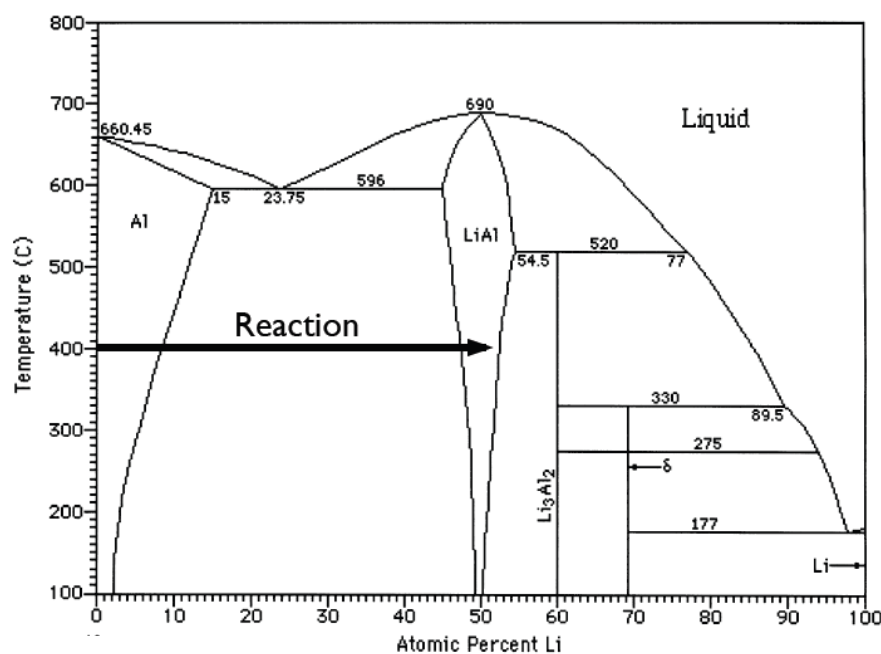
If $\Delta G_{\text{r}}^{\circ}$ has units of energy/mol, then

$$\Delta G_{\text{r}}^{\circ} = - z F E$$

$F = \text{charge per mol} = 96,500 \text{ Coulombs/mol}$

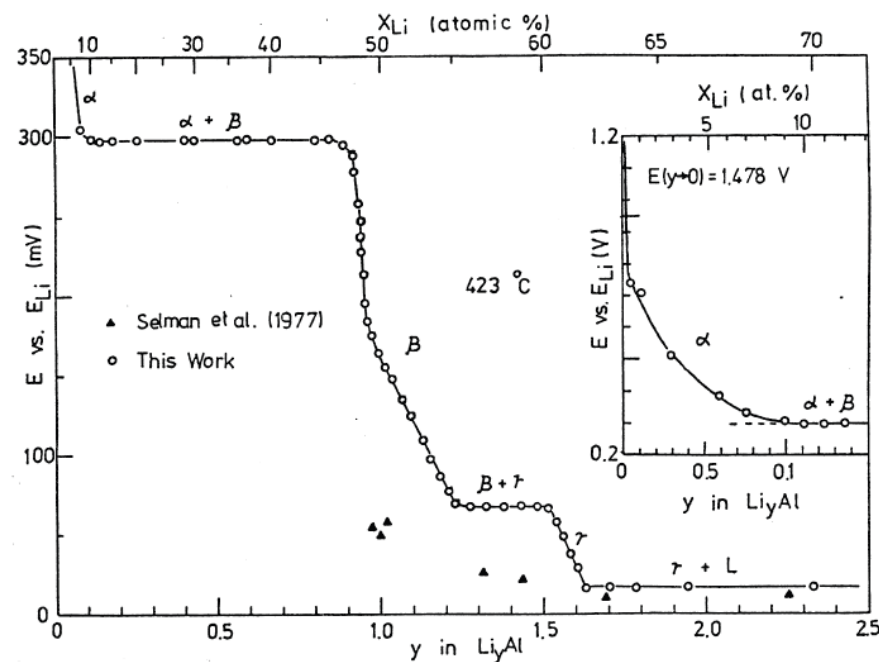
Approach by phase diagrams

Coulometric Titration of Li Into Al at 400°C



Al

Li

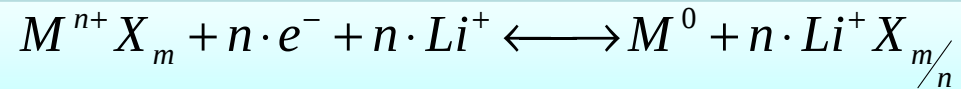


y in Li_yAl

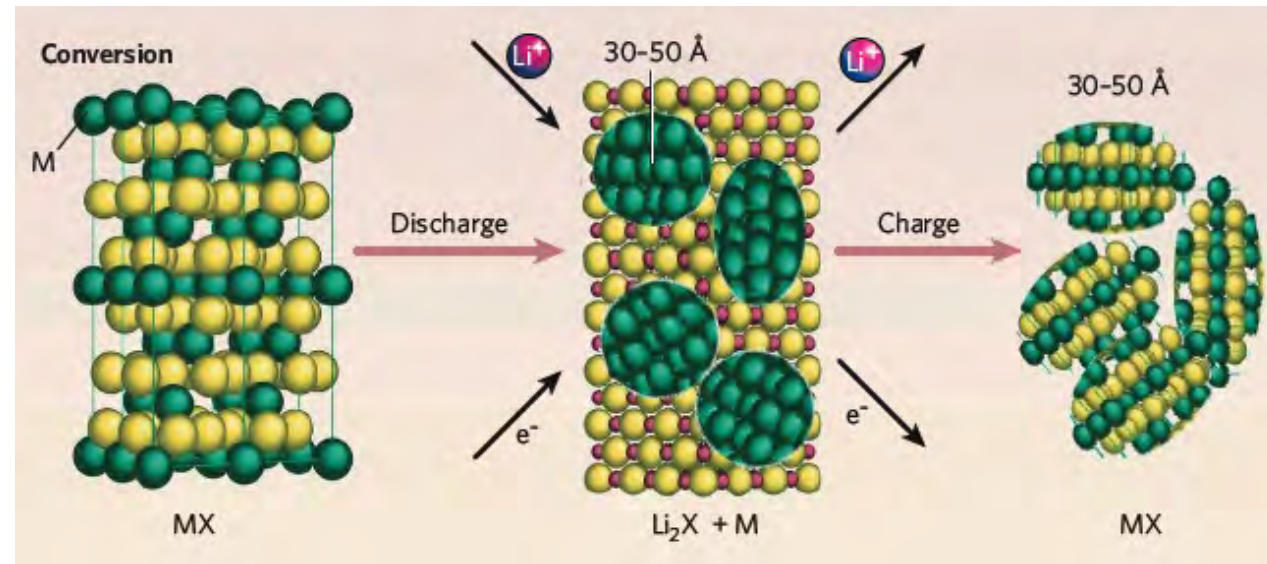
Measured Using LiCl-KCl
as a Molten Salt Electrolyte

C.J. Wen, B.A. Boukamp, R.A. Huggins, W. Weppner,
J. Electrochem. Soc. 126, 2258 (1979)

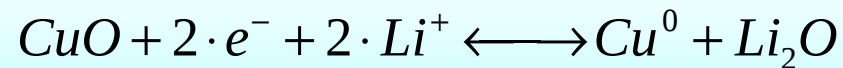
■ Electrochemical conversion mechanism



X = O, N, F, S, P

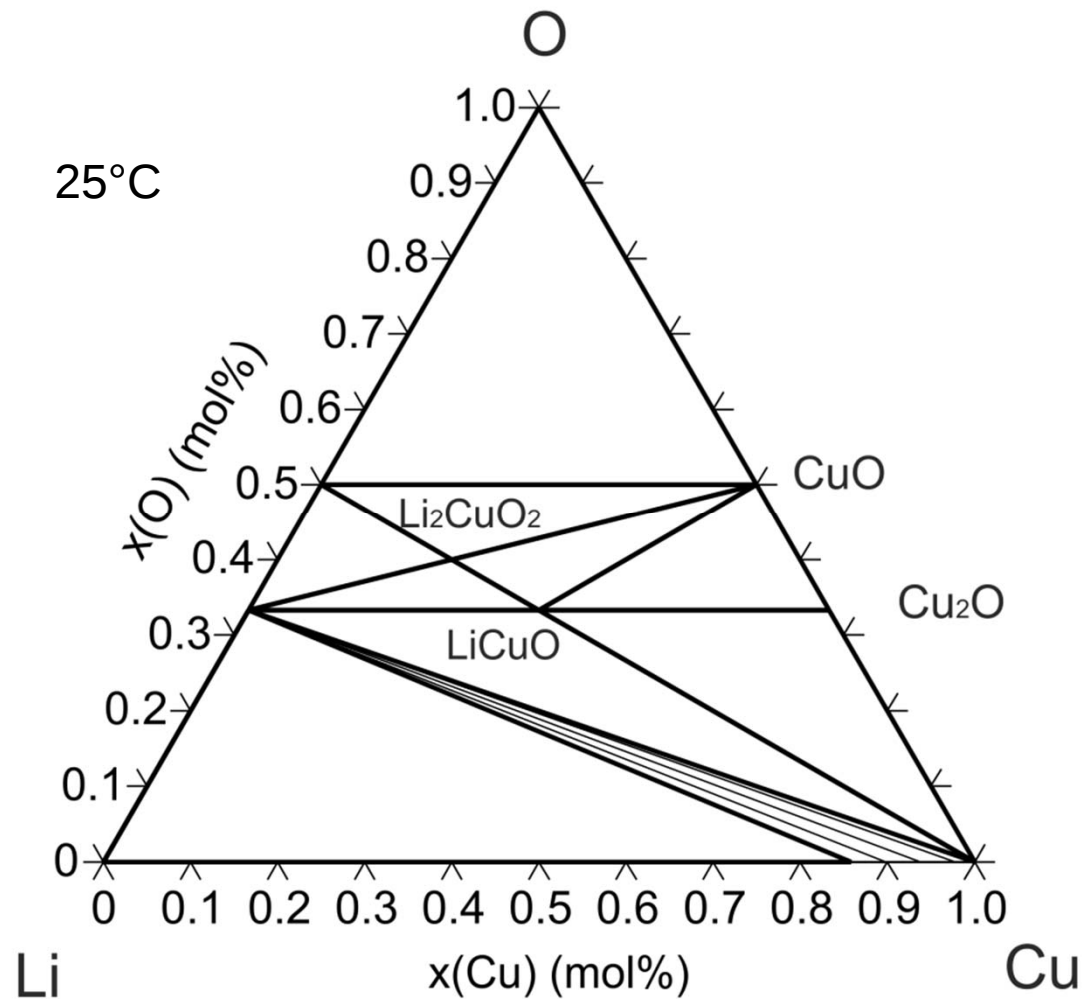


M. Armand et al., Nature, 2008, 451:652-657

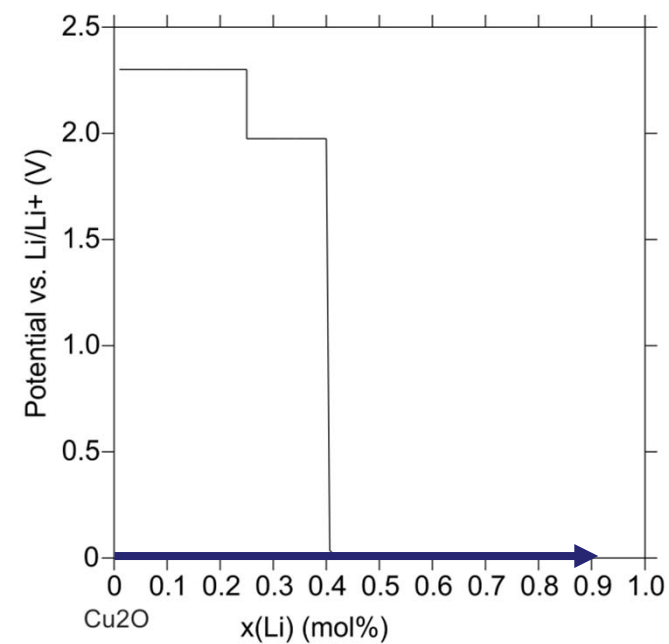
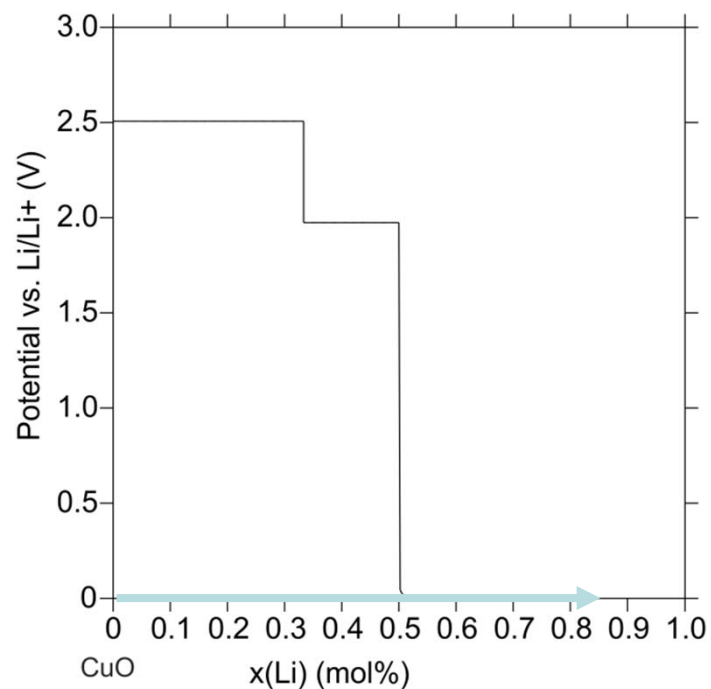
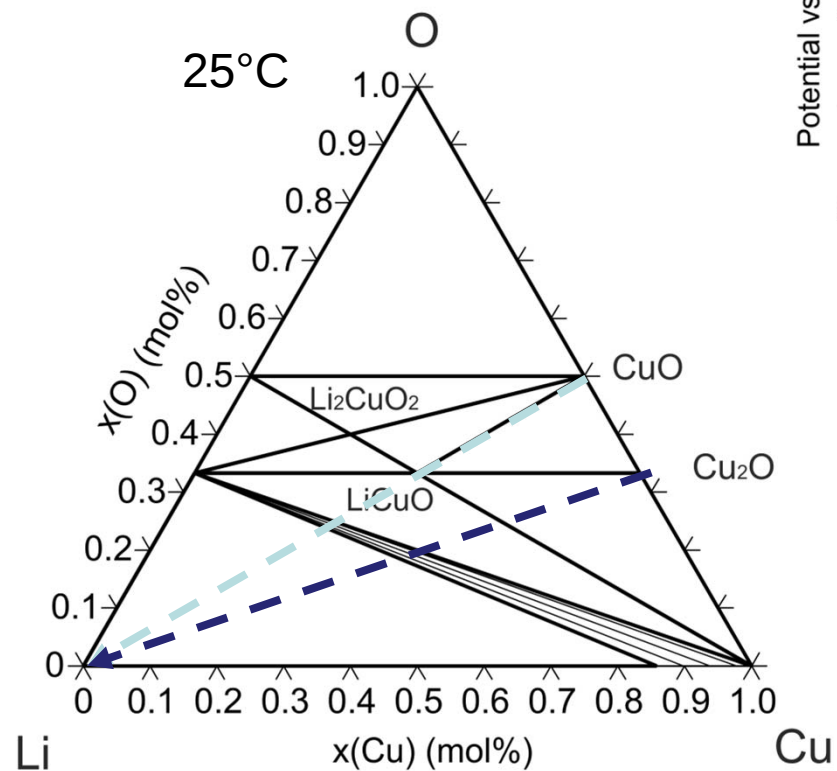


- Cu-Fe-O electrodes for LIB exhibit
 - Fe-oxides: high theoretical capacity
 - Cu-oxides: cycling stability

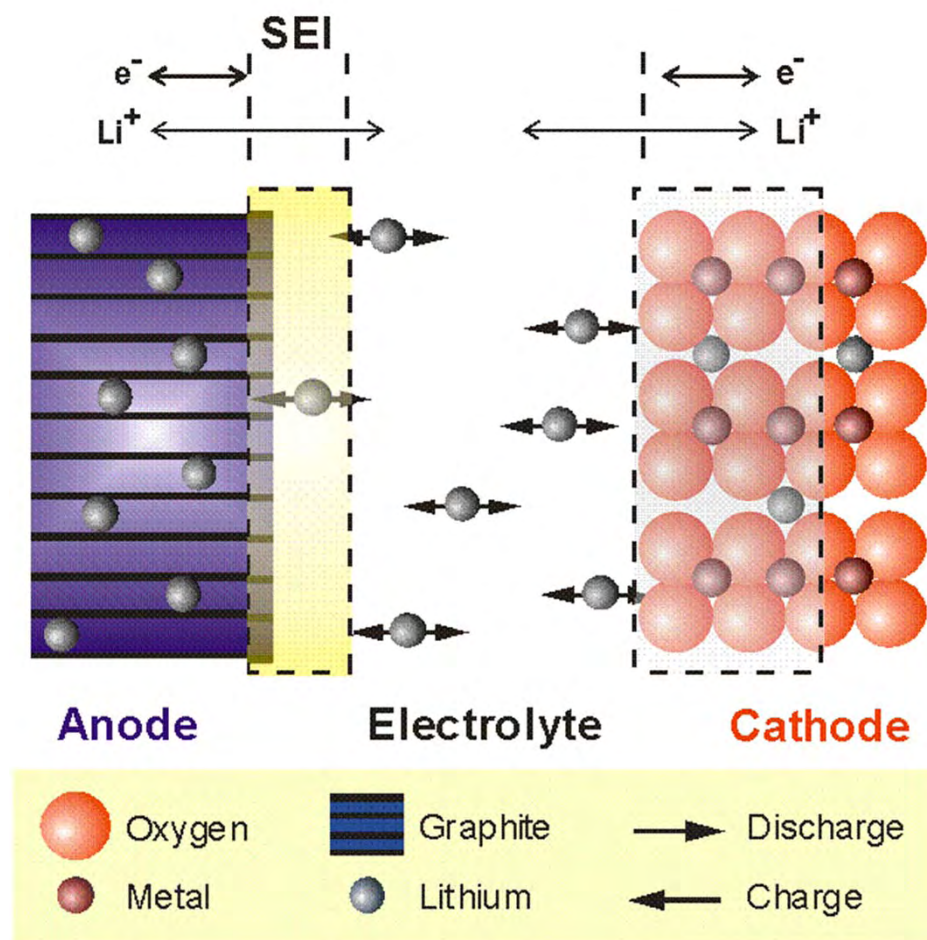
Calculated Li-Cu-O system (CALPHAD result); isothermal section



Calculated Li-Cu-O System, equilibrium voltages

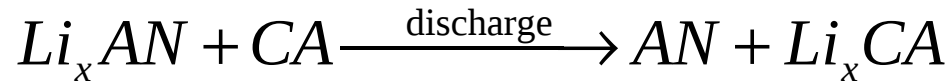


More relationships Thermodynamics - Phase Diagrams - Electrochemistry



More relationships Thermodynamics - Phase Diagrams - Electrochemistry

Full lithium ion cell discharge reaction



Free energy of the full reaction is:

$$\Delta G(x, T) = -n \cdot F \cdot E_0(x, T)$$

Free energy of the full reaction can be written:

$$\Delta G(x, T) = -\Delta H(x, T) - T\Delta S(x, T)$$

Neglecting T-dependence:

$$\Delta G_0(x, T) = -\Delta H(x) - T\Delta S(x)$$

Combining equations:

$$\Delta S(x) = F \left(\frac{\partial E_0(x, T)}{\partial T} \right) \bigg|_x \quad \Delta H(x) = F \left(-E_0(x, T) + T \frac{\partial E_0(x, T)}{\partial T} \right) \bigg|_x$$

$E_0(x, T)$ Open circuit voltage

n Charge number
($n=1$ for Li^+)

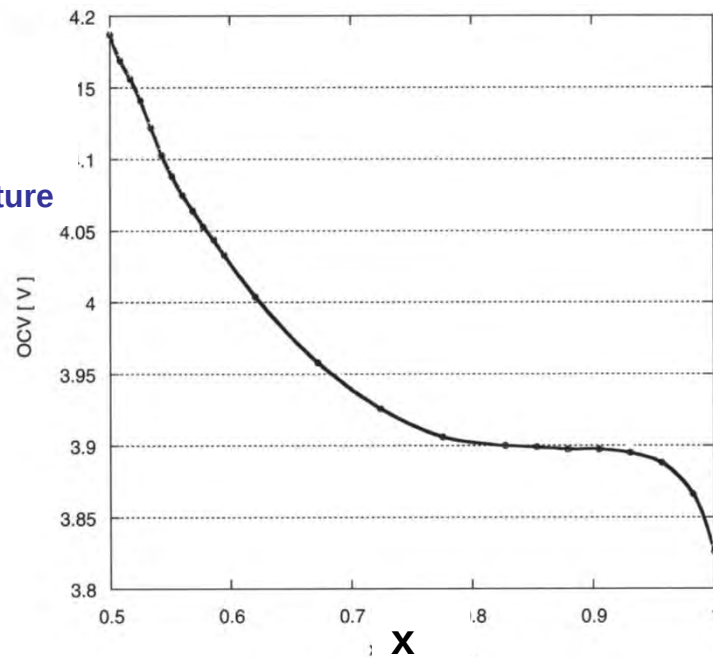
F Faraday constant

ΔH
 ΔS Heat and entropy
of reaction

$\frac{\partial E_0(x, T)}{\partial T} \bigg|_x$ Temperature
slope of $E_0(x, T)$

In-situ technique “entropymetry” and phase diagrams

OCV
for one
specific
temperature



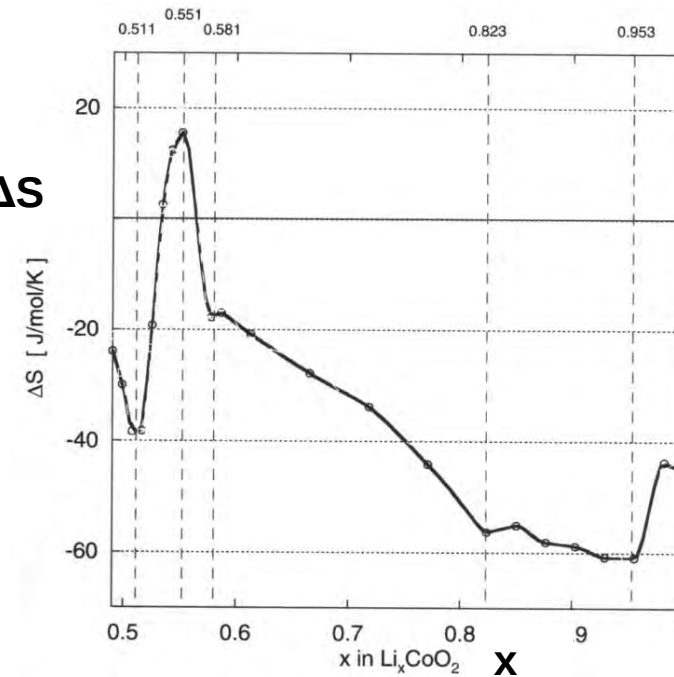
Open circuit voltage of Li_xCoO_2

Note: Half cells measured

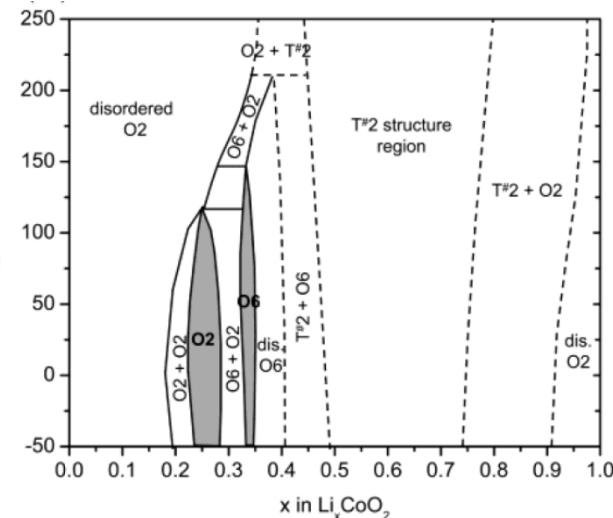
$$\overline{\Delta S} \Big|_0^1 = F \left(\int_0^1 \frac{\partial E_0(y, T)}{\partial T} \Big|_y dy \right)$$

Li_xCoO_2
Phase diagram

ΔS



Entropy of Li intercalation in Li_xCoO_2



Yazami et al. in Lithium Ion Rechargeable
Batteries, WILEY-VCH (2010)

Reversible and irreversible heat during cell reaction

$$Q_r = T\Delta S \frac{I}{nF} \quad \text{Reversible heat generation}$$

with

$$\Delta S(x) = F \left(\frac{\partial E_0(x, T)}{\partial T} \bigg|_x \right)$$

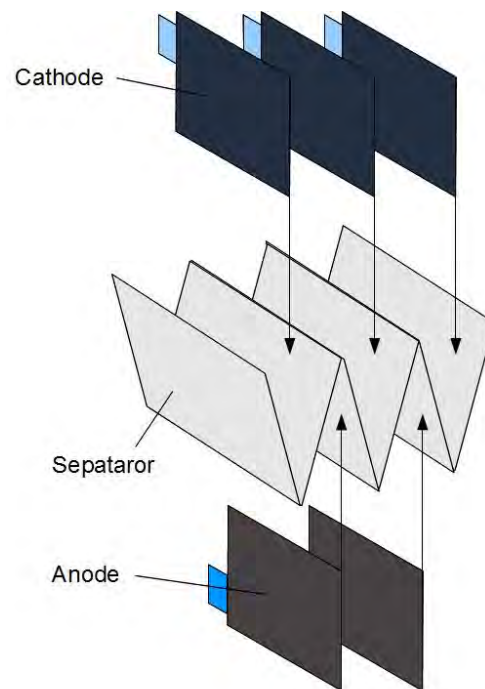
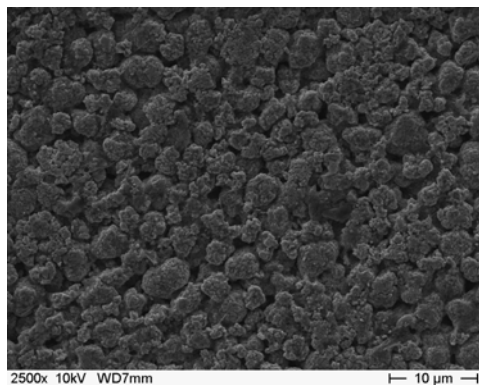
$$Q_{irr} = -I^2 R_i \quad \text{Irreversible heat generation}$$

$$Q = Q_r + Q_{irr} \quad \text{Total heat generation}$$

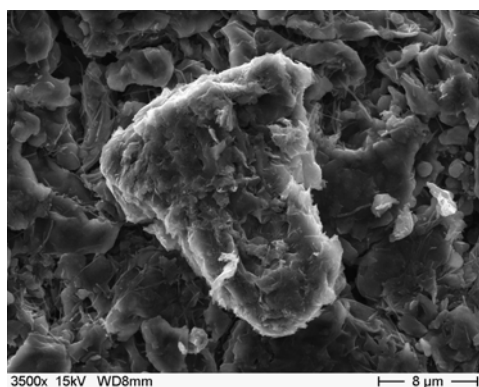
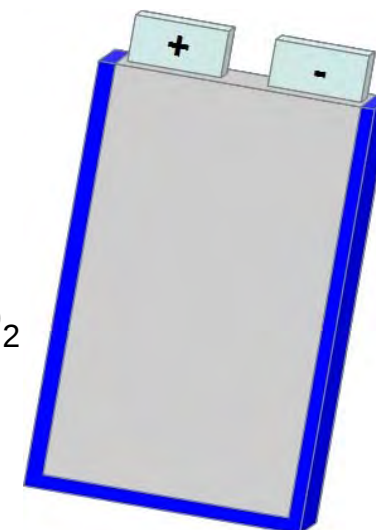
+ side reactions



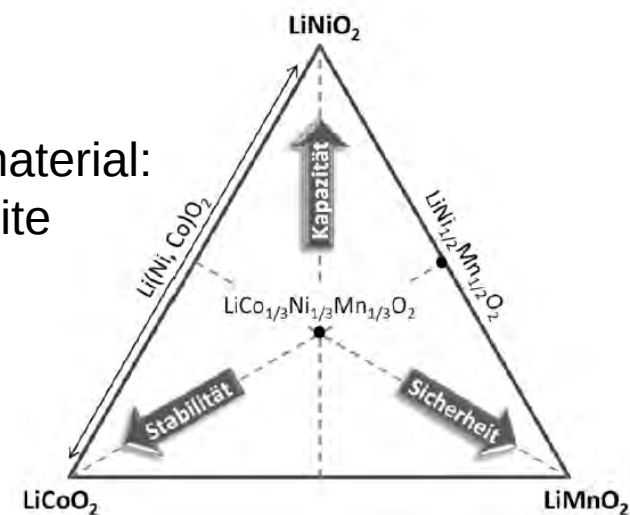
40Ah pouch cell



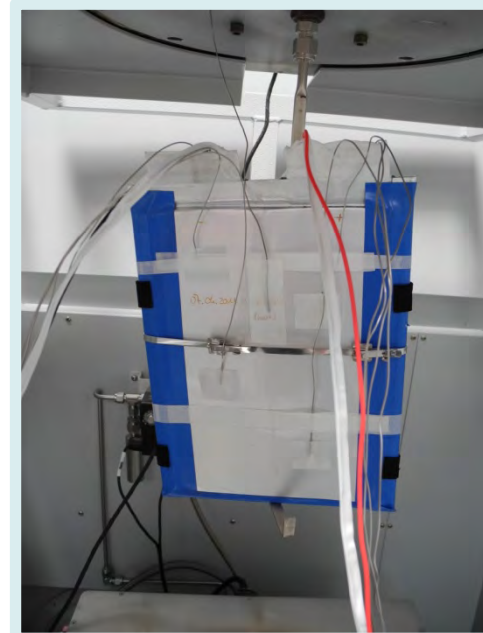
Cathode material:
 $\text{Li}(\text{Ni}_{1/3}\text{Mn}_{1/3}\text{Co}_{1/3})\text{O}_2$
 $\rightarrow$ NMC



Anode material:
 $\rightarrow$ graphite



40Ah cell with eight thermocouples measured in Accelerating Rate Calorimeter (ARC)



Isothermal cycling of a 40Ah pouch cell

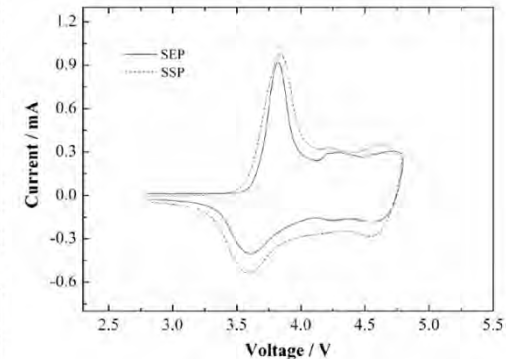
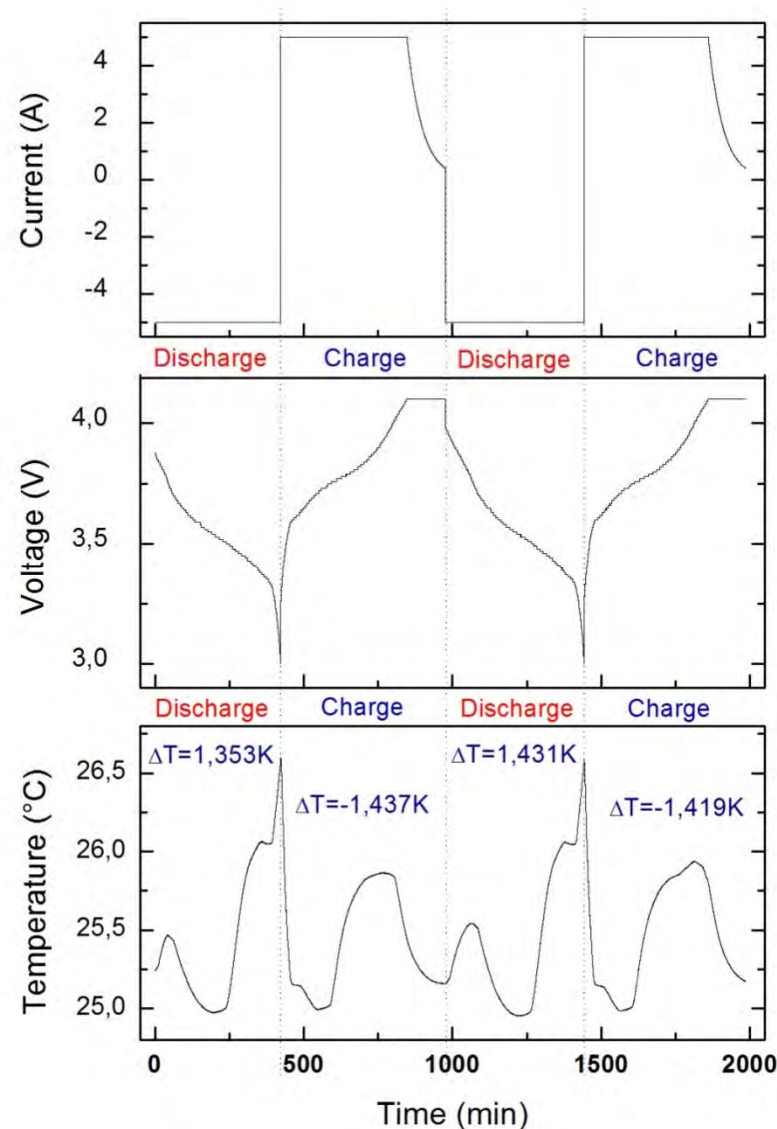
Discharge parameter:

- method: constant current (CC)
- $U_{\min} = 3,0V$
- $I = 5A \rightarrow C/8\text{-rate}$

Charge parameter:

- method: constant current, constant voltage (CCCV)
- $U_{\max} = 4,1V$
- $I = 5A \rightarrow C/8\text{-rate}$
- $I_{\min} = 0.5A$

at room temperature



temperature coefficient

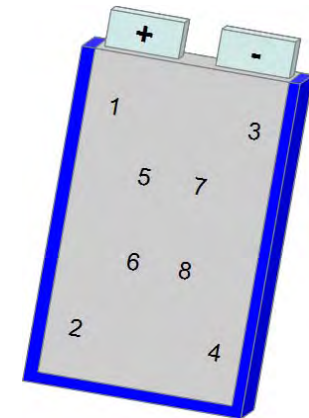
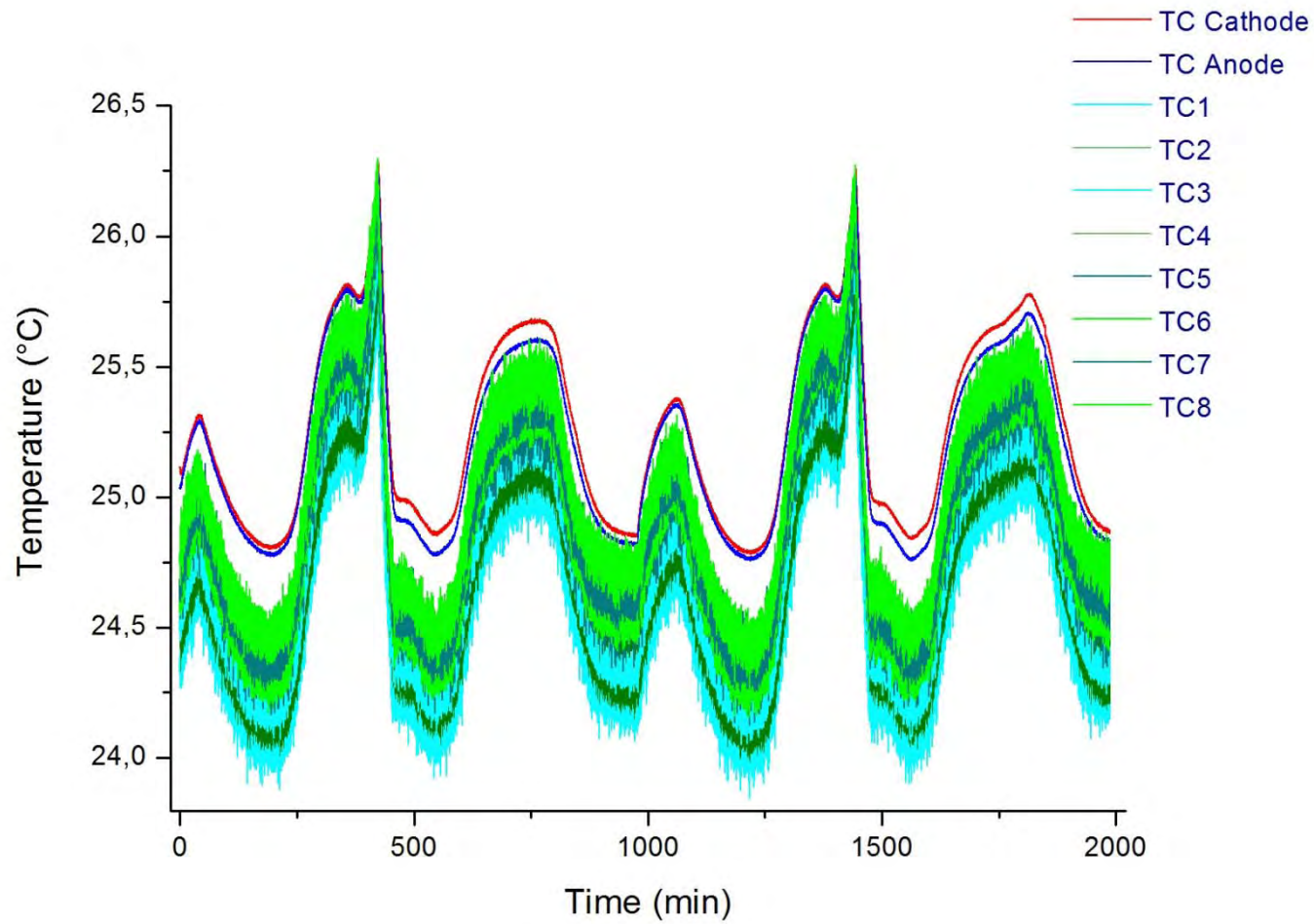
$$\left(\frac{\delta E}{\delta T}\right) < 0$$

Procedure like in:

H.-B. Ren, et. al., Int. J. Electrochem. Sci. 6, p. 727 – 738 (2011)

A.K. Shukla, T.P. Kumar, Current Sci. 94, p. 314-331 (2008)

Temperature measurements on a 40Ah pouch cell



Adiabatic cycling of a 40Ah pouch cell

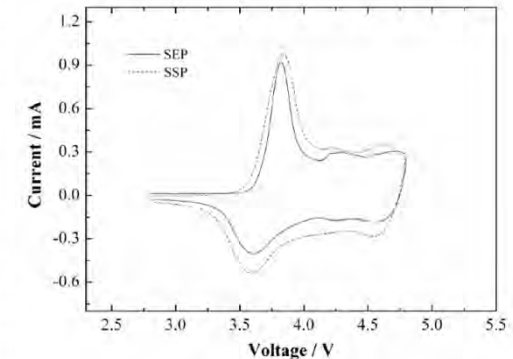
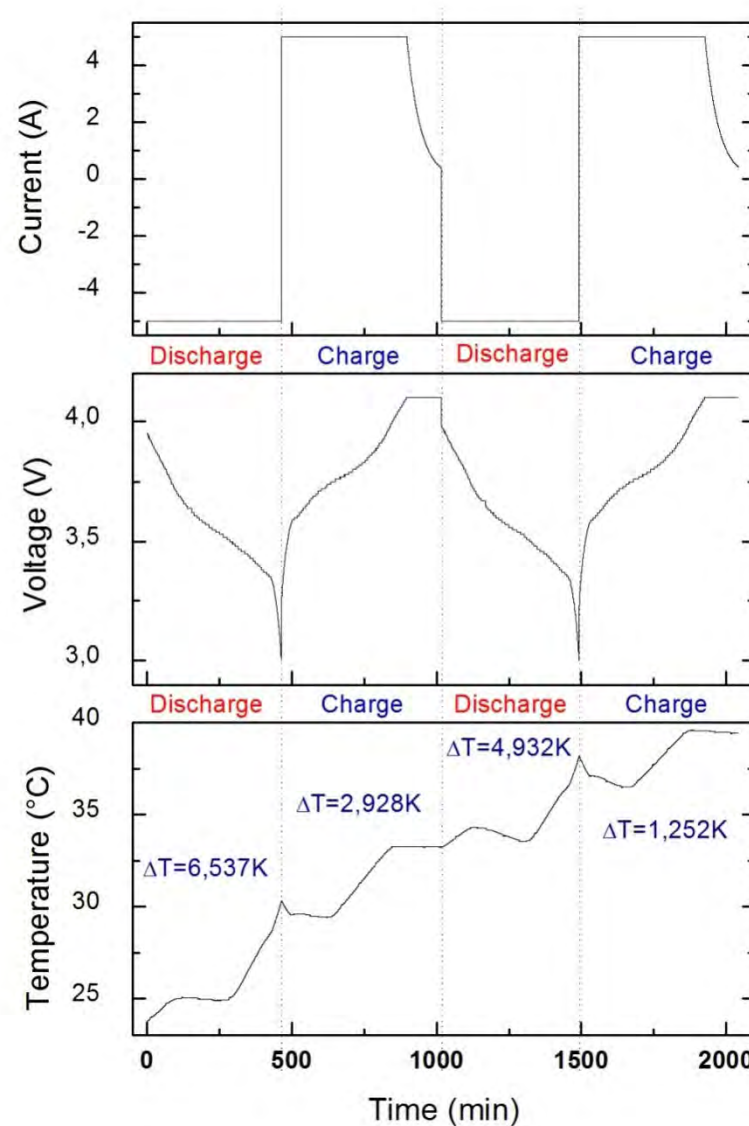
Discharge parameter:

- method: constant current (CC)
- $U_{\min} = 3,0V$
- $I = 5A \rightarrow C/8\text{-rate}$

Charge parameter:

- method: constant current, constant voltage (CCCV)
- $U_{\max} = 4,1V$
- $I = 5A \rightarrow C/8\text{-rate}$
- $I_{\min} = 0.5A$

at room temperature



temperature coefficient

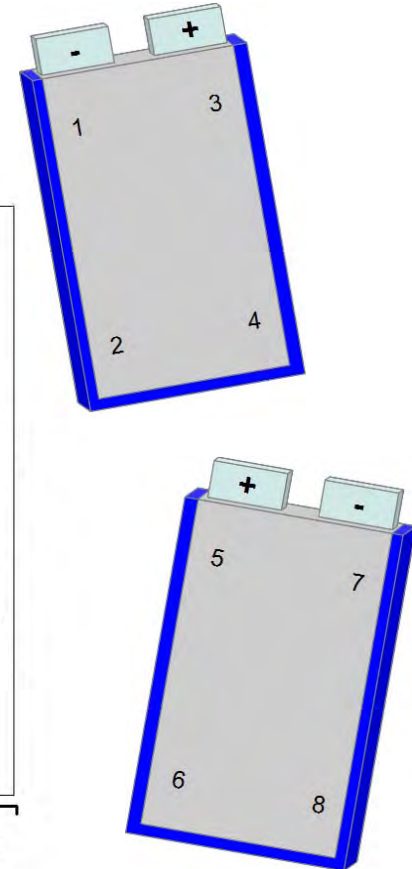
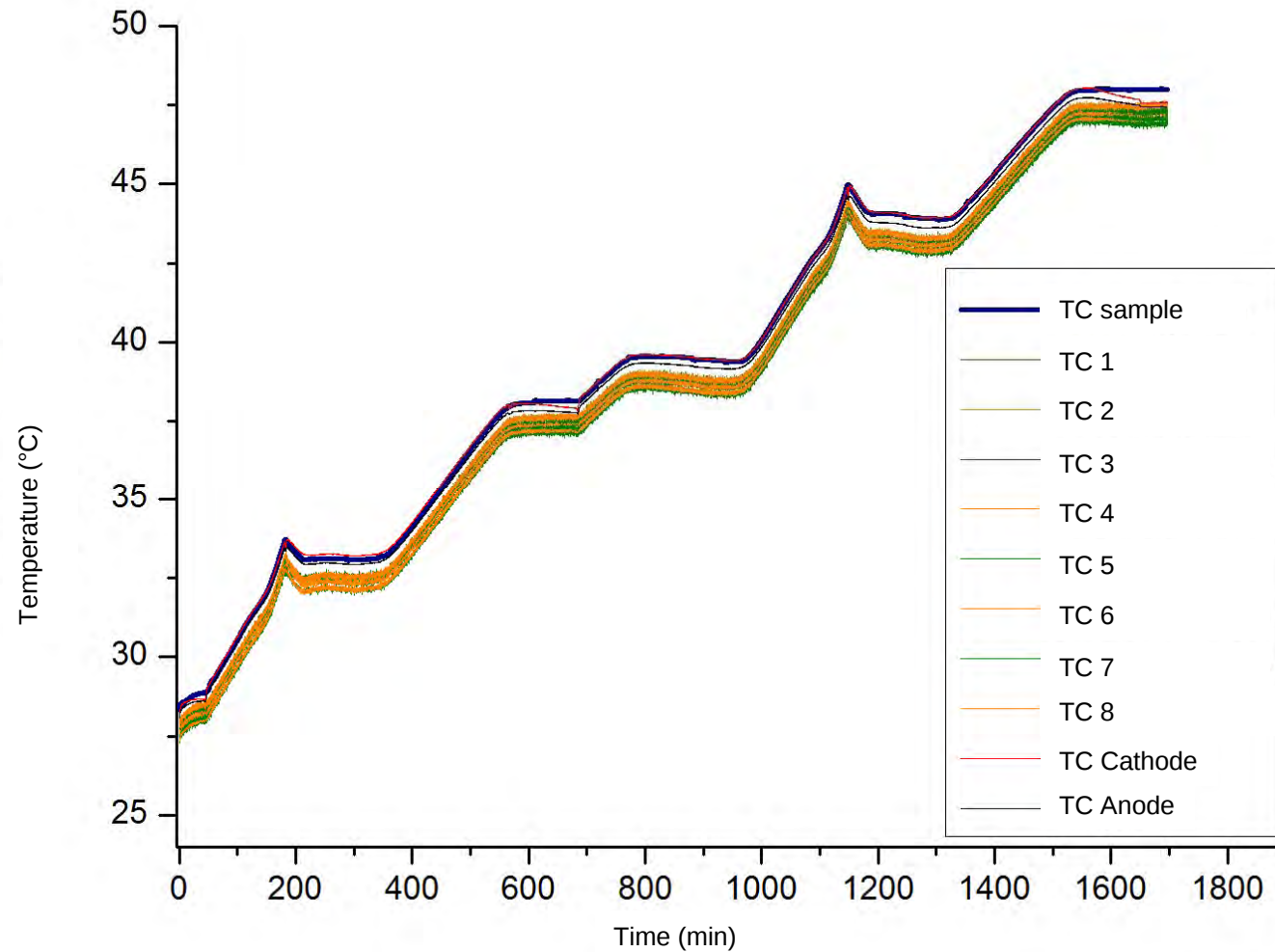
$$\left(\frac{\delta E}{\delta T}\right) < 0$$

Procedure like in:

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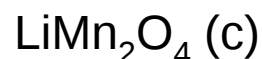
Temperature measurements on a 40Ah pouch cell



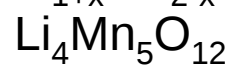
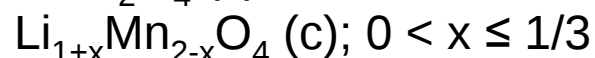
Li-Mn-O System

Thermodynamically stable phases in the Li-Mn-O system.

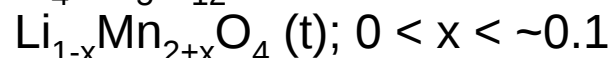
Stoichiometric



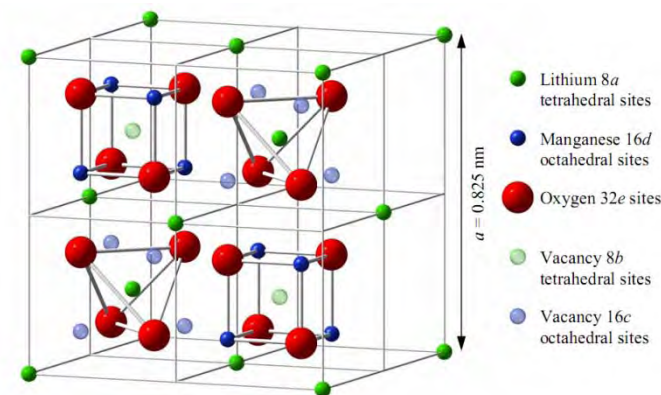
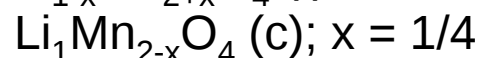
Cation-mixed



Mn-rich



Mn-deficient

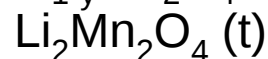


Thermodynamically unstable phases in the Li-Mn-O system.

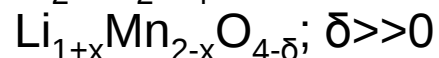
De-lithiated



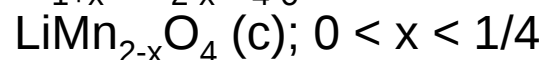
Lithiated



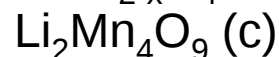
Oxygen-deficient



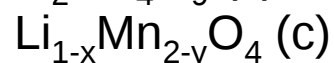
Mn-deficient



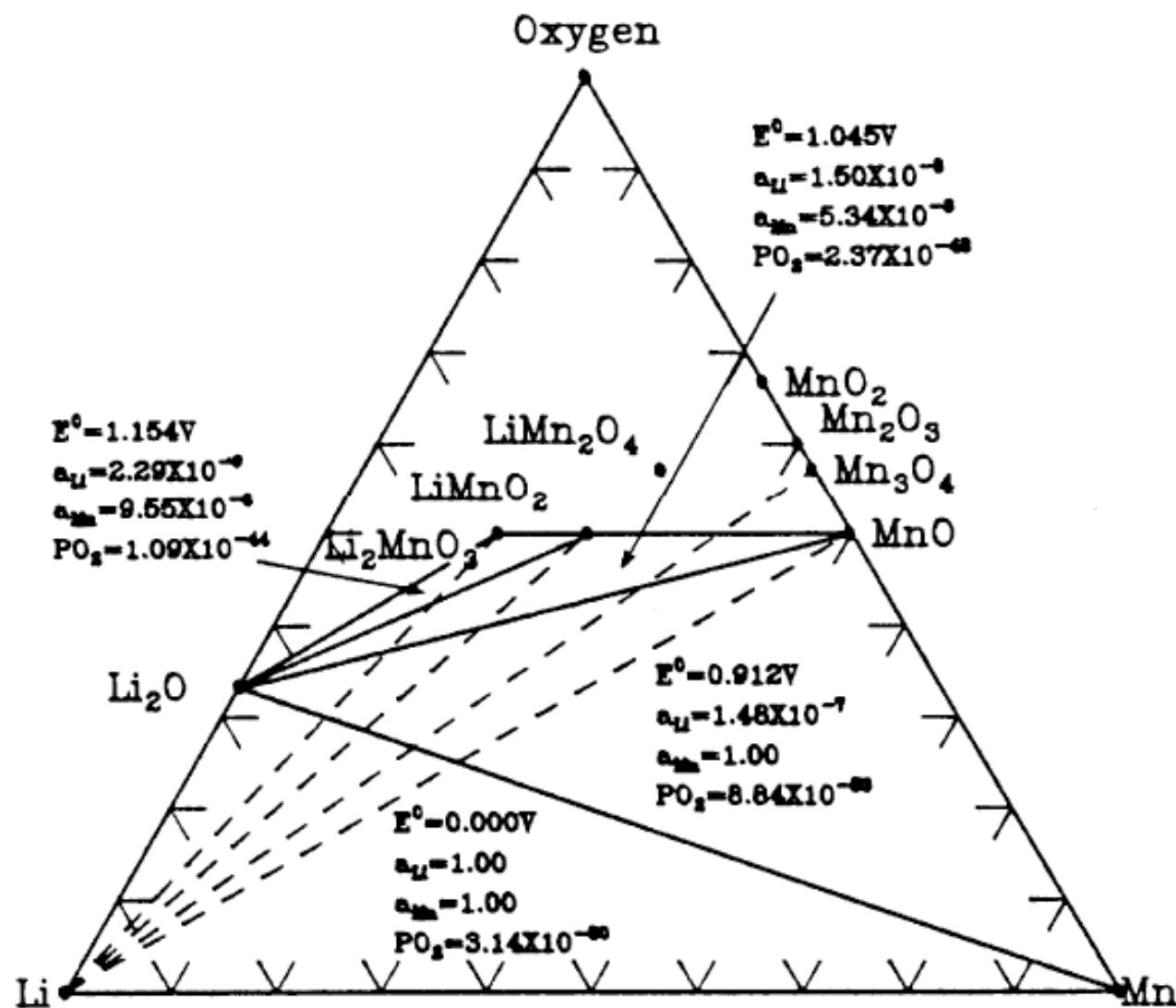
Oxygen-rich



Cation-deficient

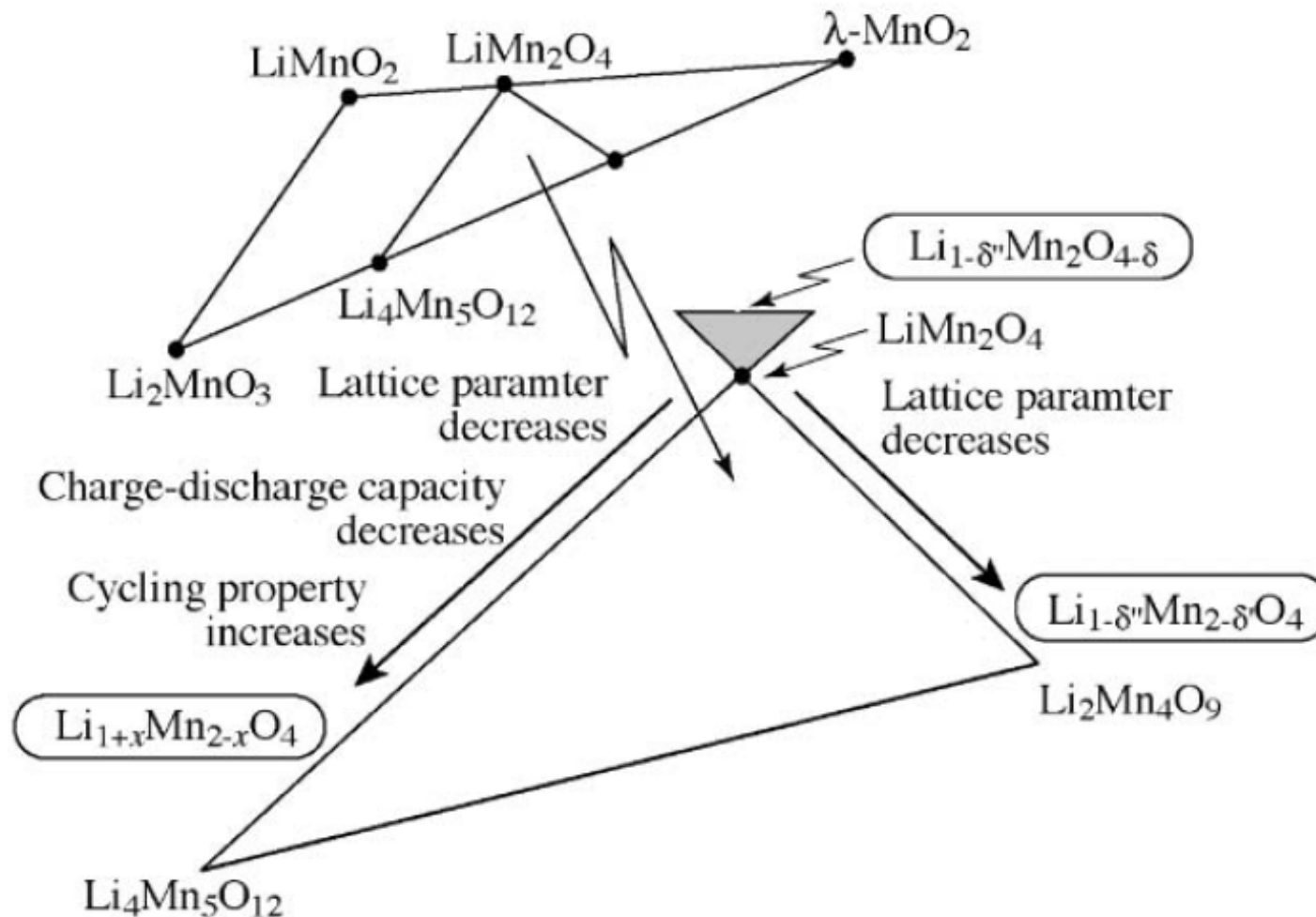


Li-Mn-O System



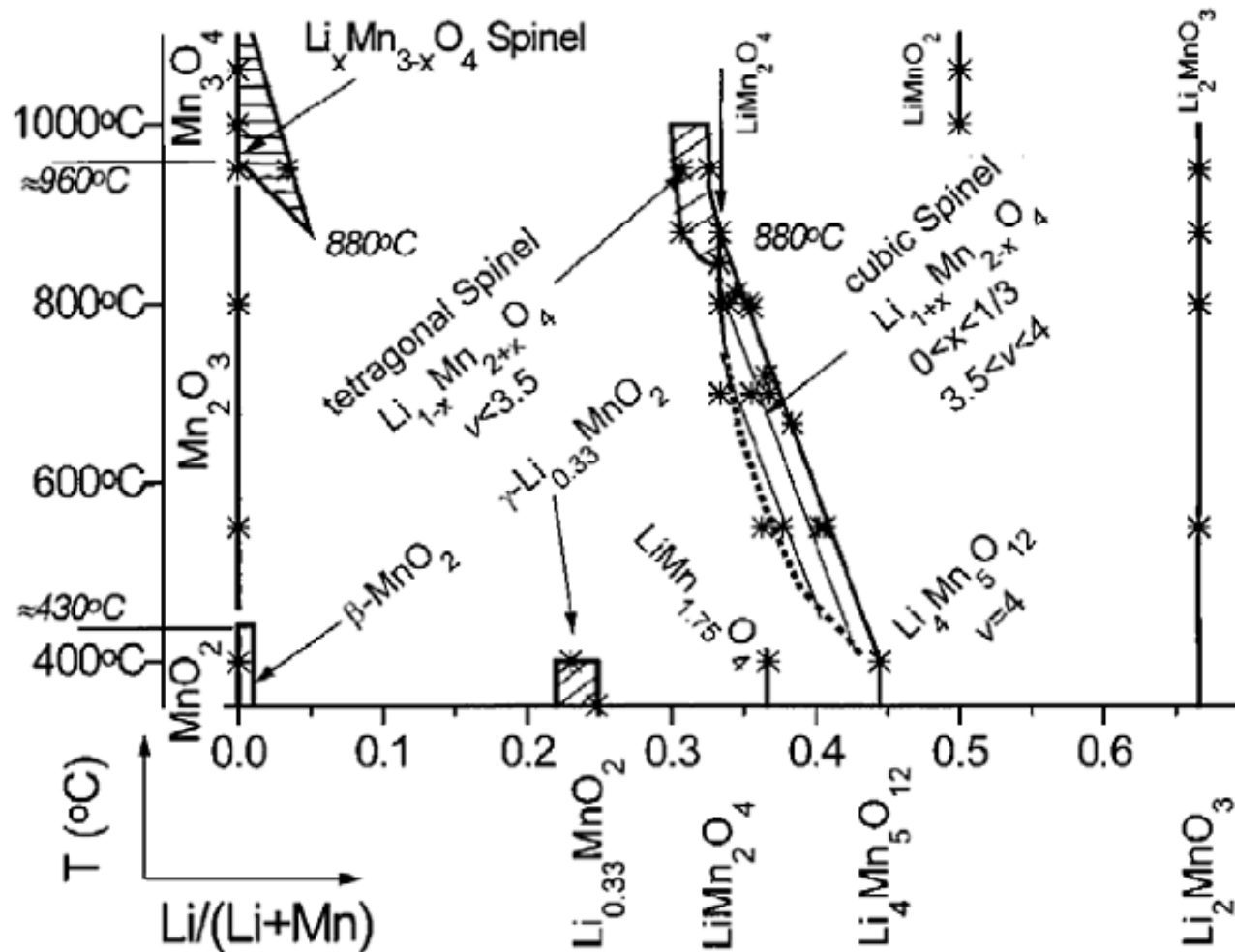
R. Huggins, Advanced Batteries, Springer 2011

Li-Mn-O System



Phase relationships in the system $\text{LiMnO}_2 - \text{Li}_2\text{MnO}_3 - \lambda\text{-MnO}_2$ and subsystem $\text{LiMn}_2\text{O}_4 - \text{Li}_4\text{Mn}_5\text{O}_{12} - \text{Li}_2\text{Mn}_4\text{O}_9$ (Yonemura et al. 2004).

Li-Mn-O System



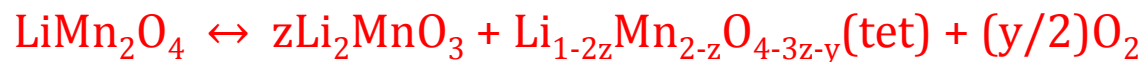
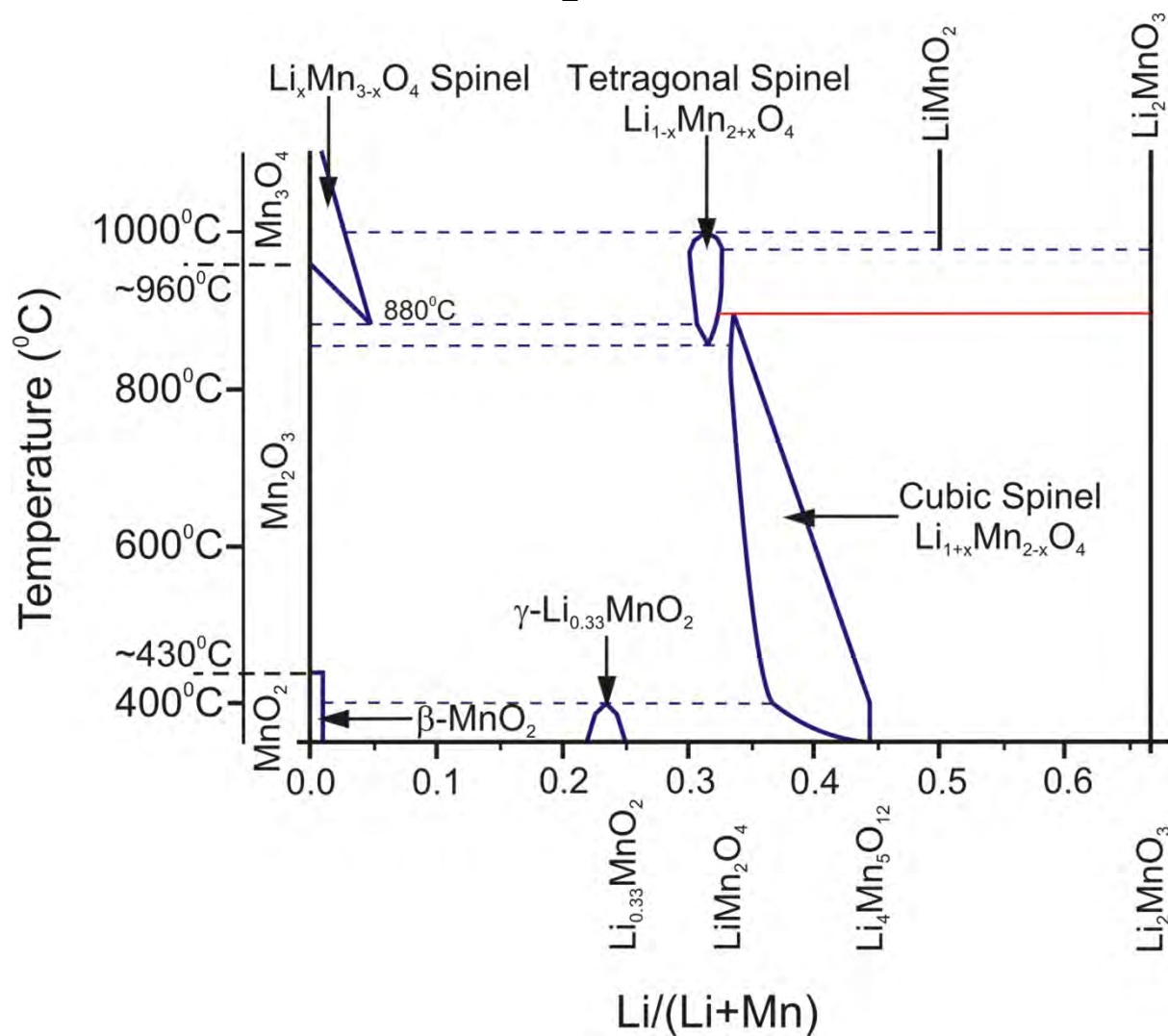
[1999 Pau]

- Samples prepared using the solid state method
- Phase diagram investigated at $p\text{O}_2=0.21$ atm

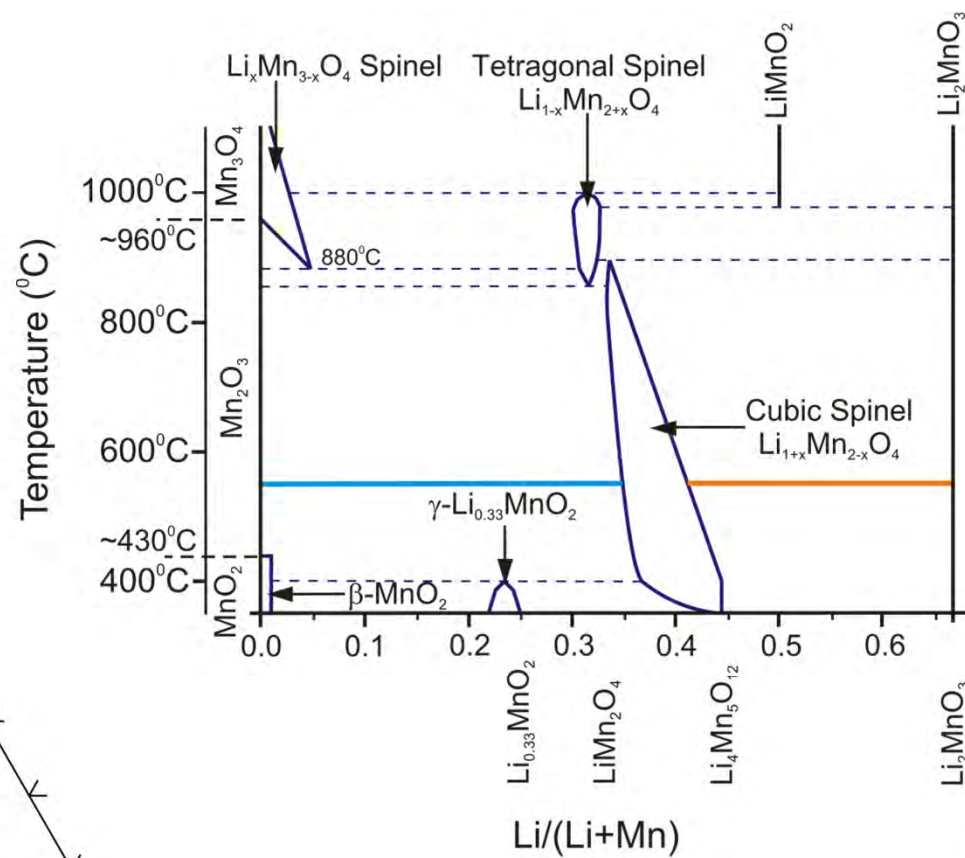
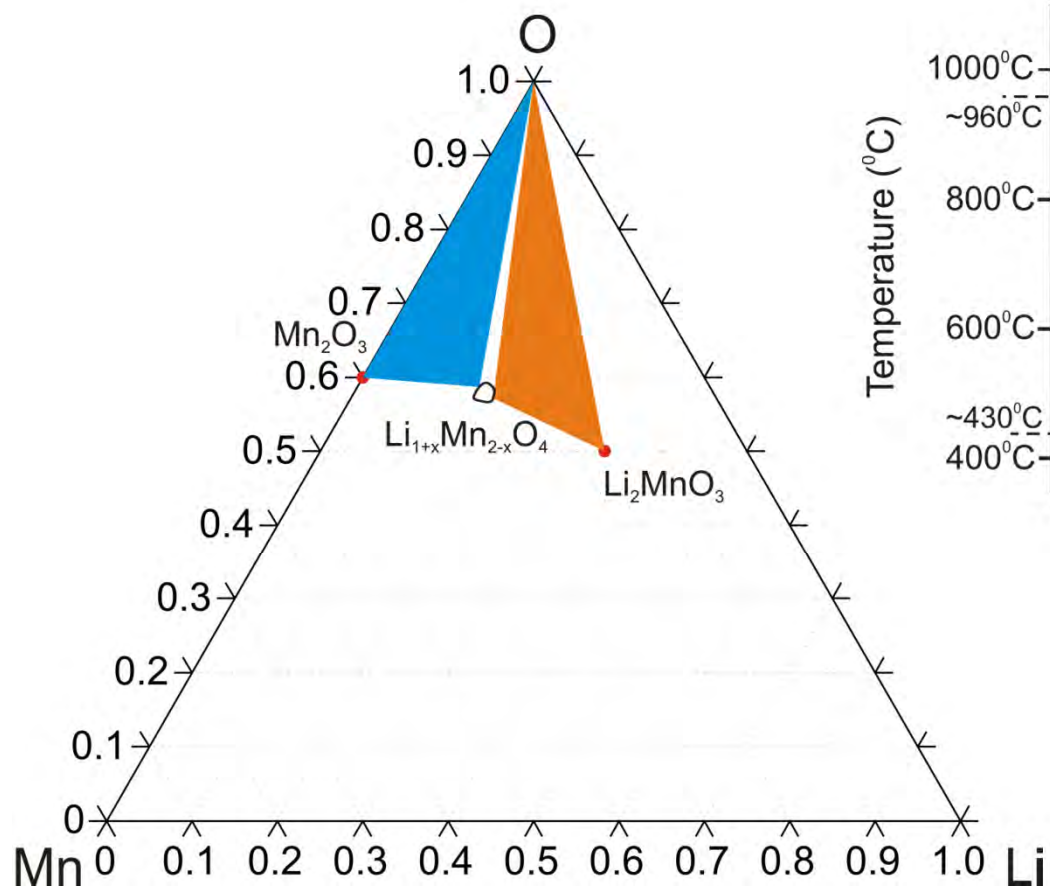
[1999 Pau] *Chem. Mater.*, 11 (1999), 3065-3079.

Li-Mn-O System

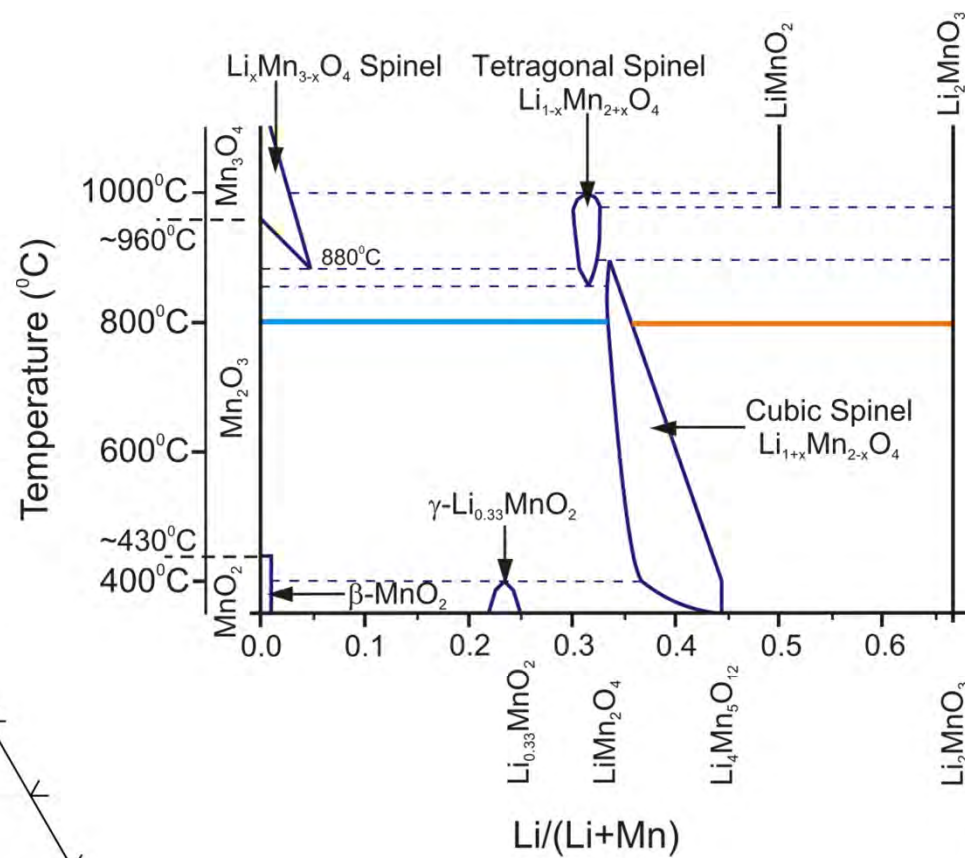
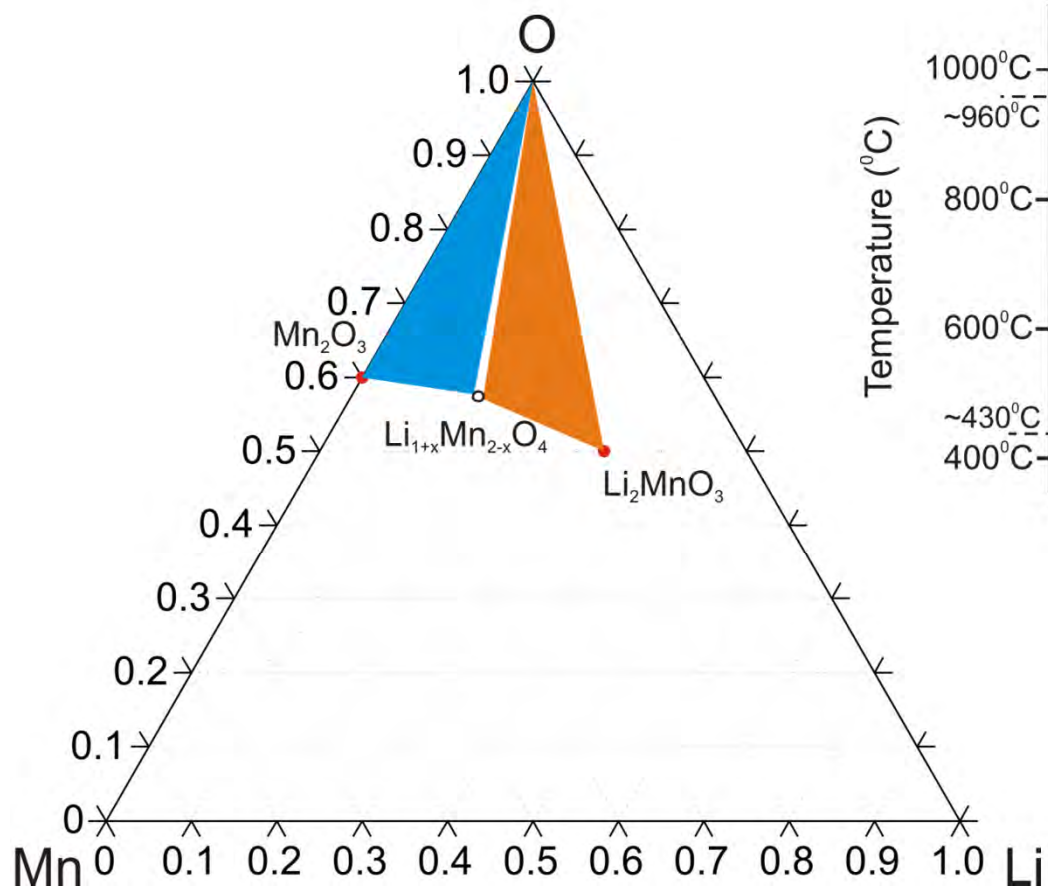
$p(\text{O}_2)=0.21 \text{ atm}$



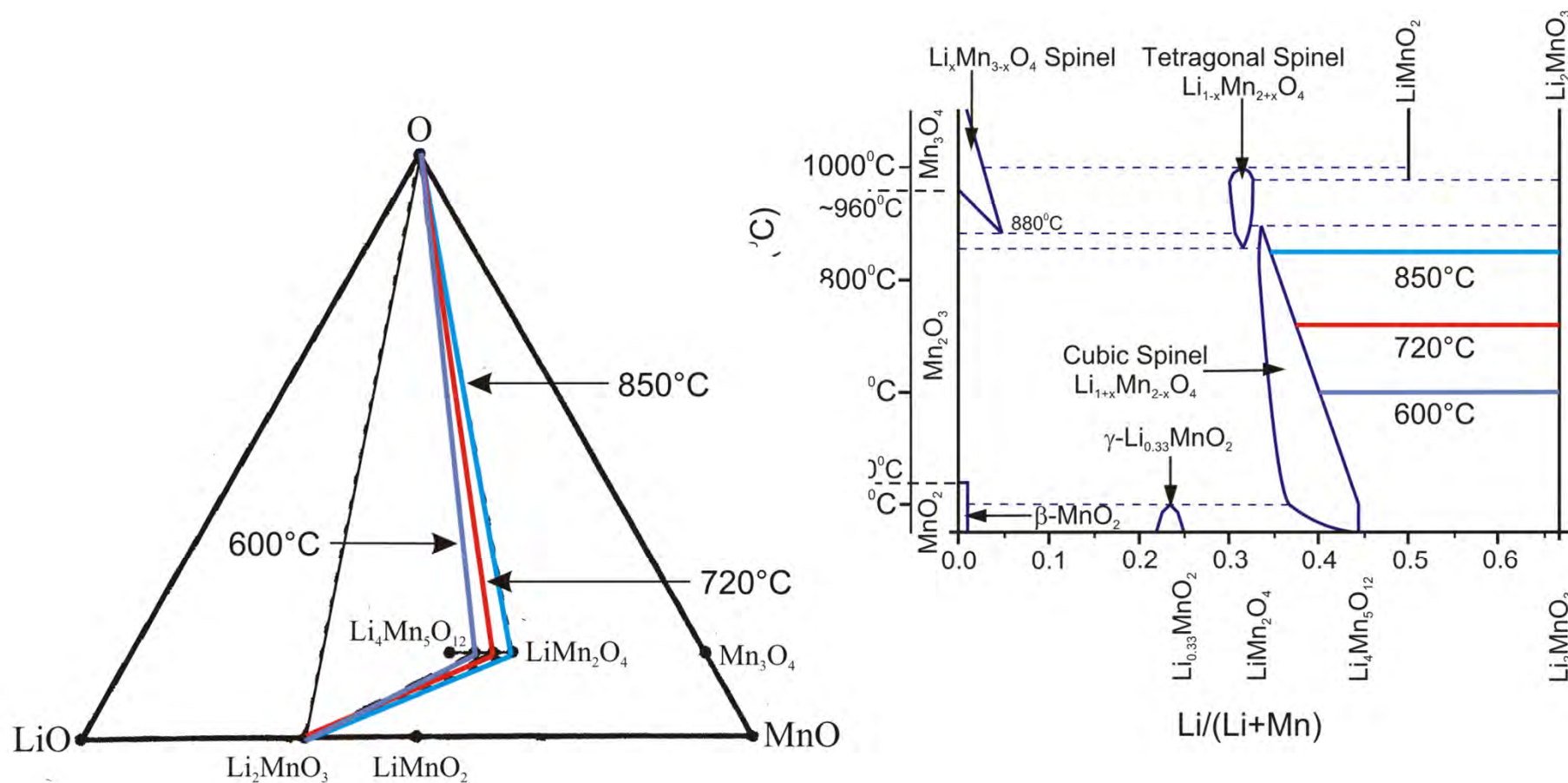
Li-Mn-O System



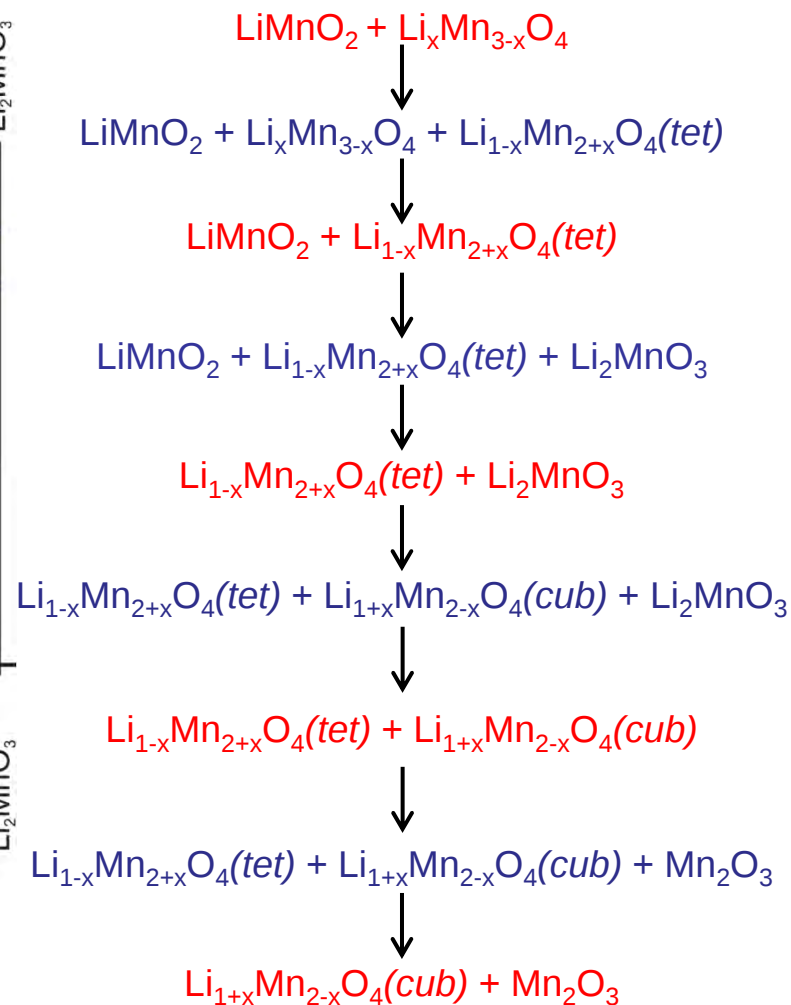
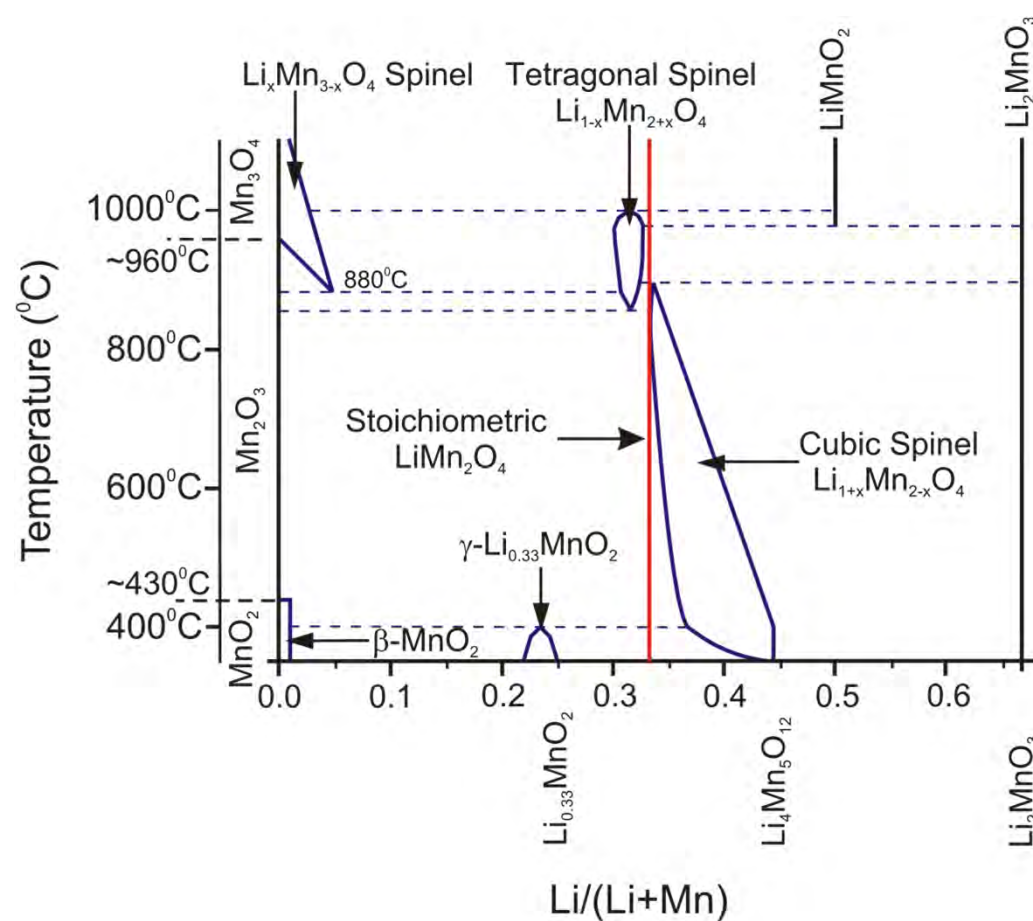
Li-Mn-O System



Li-Mn-O System



Li-Mn-O System



Enthalpy of Drop Solution of $\text{Li}_{1+x}\text{Mn}_{2-x}\text{O}_{4-\delta}$



Al_2O_3 plug

SiO_2 glass dropping tube for sample introduction

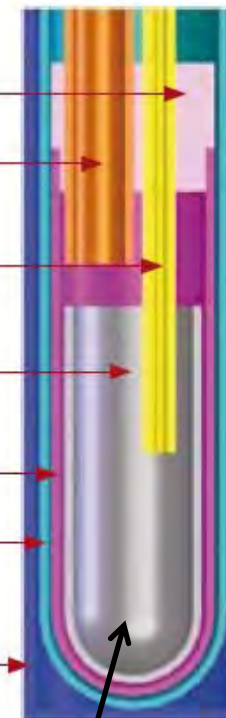
Platinum tube for bubbling gas introduction

Platinum crucible where solvent is introduced

SiO_2 glass crucible

SiO_2 glass liner

Inconel protection tube

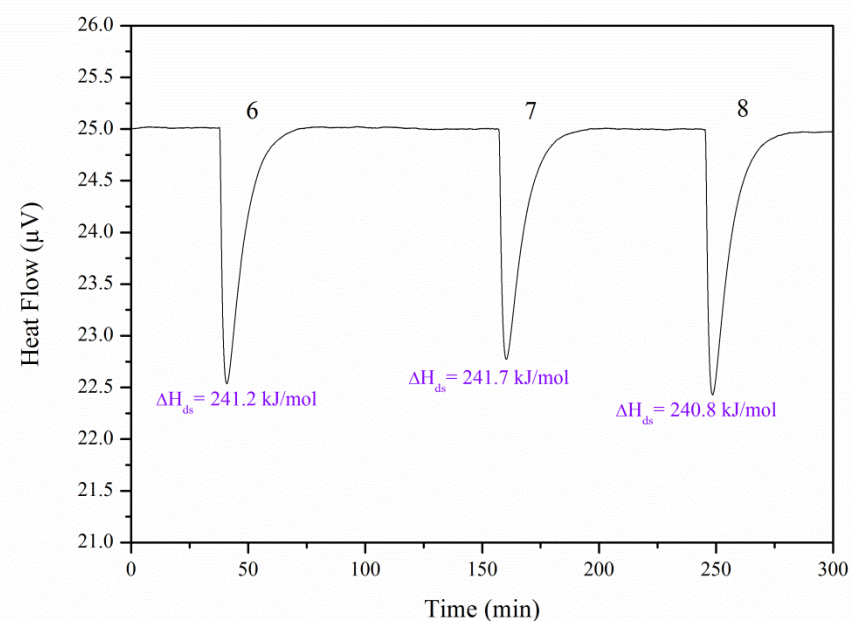
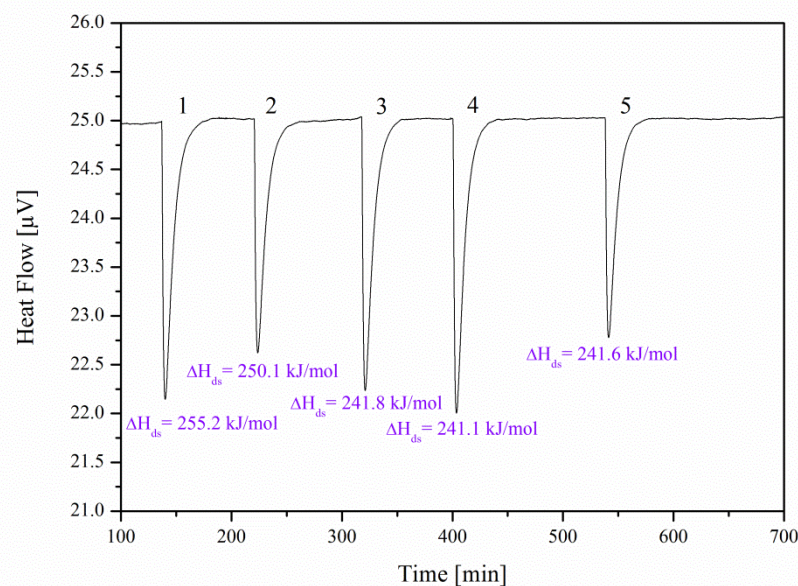


Sodium Molybdate, 700°C

AlexSys, SETARAM

High Temperature Calvet Calorimeter

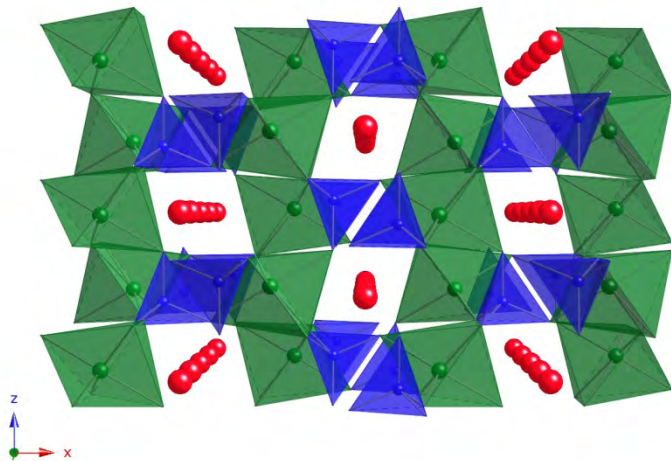
Enthalpy of Drop Solution of $\text{Li}_{1+x}\text{Mn}_{2-x}\text{O}_{4-\delta}$



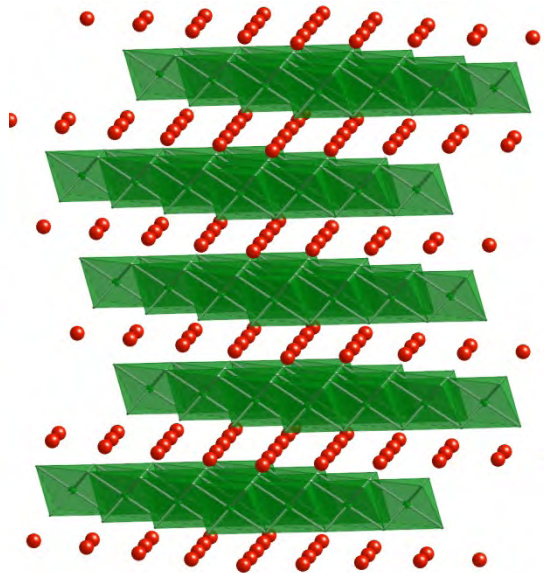
Sample Number	DROP 1	DROP 2	DROP 3	DROP 4	DROP 5	DROP 6	DROP 7	DROP 8
Date	08. Mai	08. Mai	08. Mai	08. Mai	08. Mai	09. Mai	09. Mai	09. Mai
Mass pellet (mg)	6,00	5,14	6,10	6,62	4,85	5,35	4,83	5,59
T(room) (°C)	23,90	24,10	24,20	24,10	24,20	24,50	24,30	24,20
T(cal.) (°C)	700,40	700,40	700,40	700,40	700,40	700,40	700,40	700,40
Formula weight (g/mol)	180,815	180,815	180,815	180,815	180,815	180,815	180,815	180,815
Moles of LiMn_2O_4 (mol)	0,0000332	0,0000284	0,0000337	0,0000366	0,0000268	0,0000296	0,0000267	0,0000309
Peak Area [μV.s]	1832,4170	1538,5640	1765,6030	1910,2030	1402,3320	1544,6110	1397,2290	1611,2630
Calibration factor from Al_2O_3 calibration[J/μV.s]	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077
Measured Heat Effect (kJ/mol)	255,1652	250,0926	241,8308	241,0849	241,5781	241,2203	241,6957	240,8258
Accepted Measurement	0	0	1	1	1	1	1	1

Commercial cathode materials

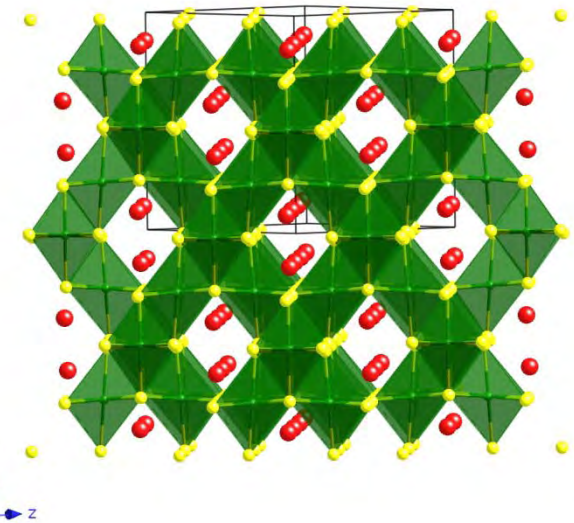
Olivine structure



Layered structure



Spinel structure



LiCoO₂: ≈ 160 mAh/g

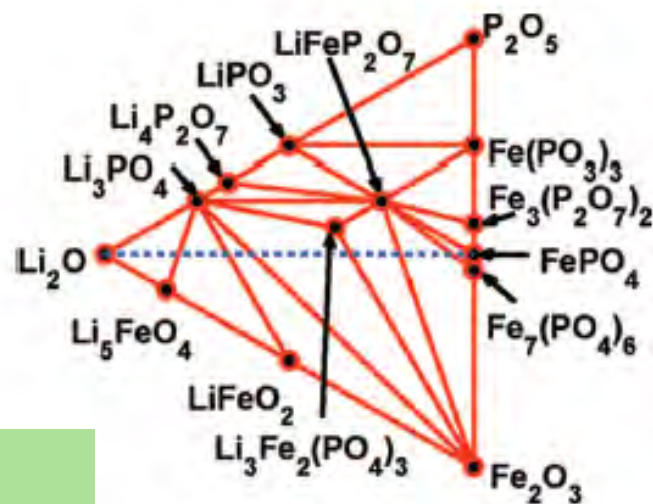
LiFePO₄: ≈ 160 mAh/g

LiMn₂O₄: ≈ 100 mAh/g

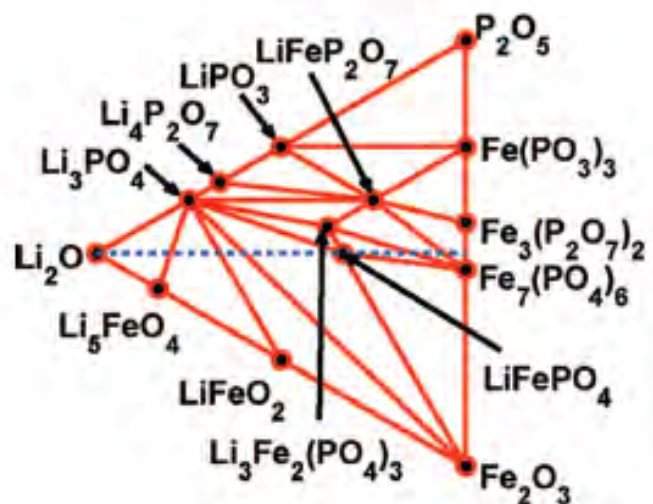
Gravimetric energy densities (capacities)

Li-Fe-P-O System

LiFePO₄ -
Stable phase?



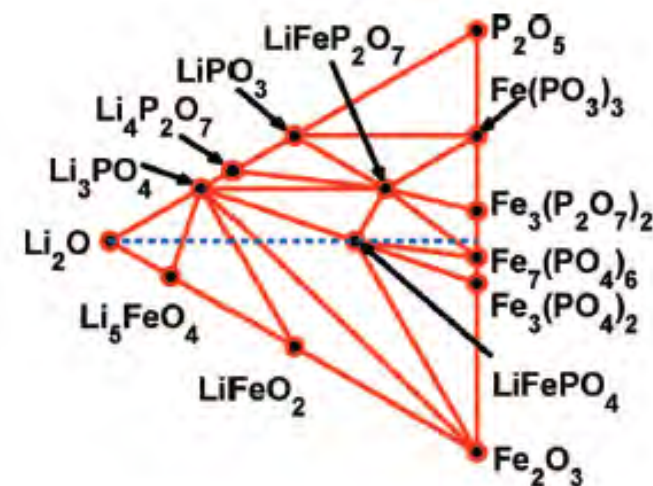
(a) $\mu_{O_2} = -10.50$ eV, $Fe_7(PO_4)_6$ appears



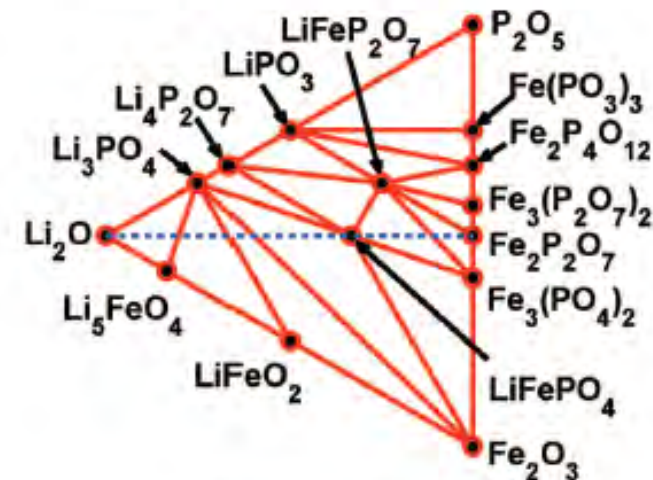
(b) $\mu_{O_2} = -11.52$ eV, $LiFePO_4$ appears

Figure 2. Phase diagrams at less reducing environments.

Ong et al. (2008)



(a) $\mu_{O_2} = -11.74$ eV, $Li_3Fe_2(PO_4)_3$ disappears

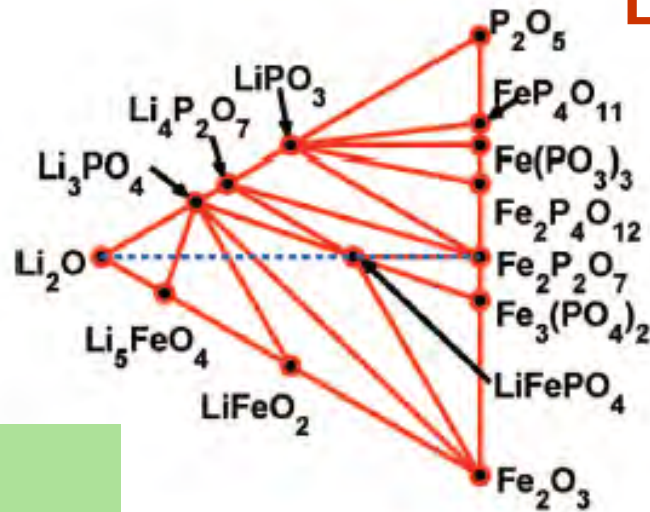


(b) $\mu_{O_2} = -12.38$ eV, $Fe_2P_2O_7$ appears

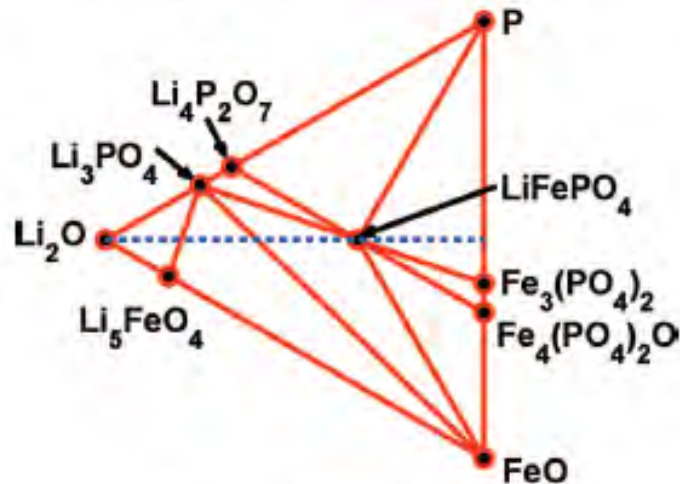
Figure 3. Phase diagrams at more reducing environments.

Li-Fe-P-O System

LiFePO₄ -
Stable phase?

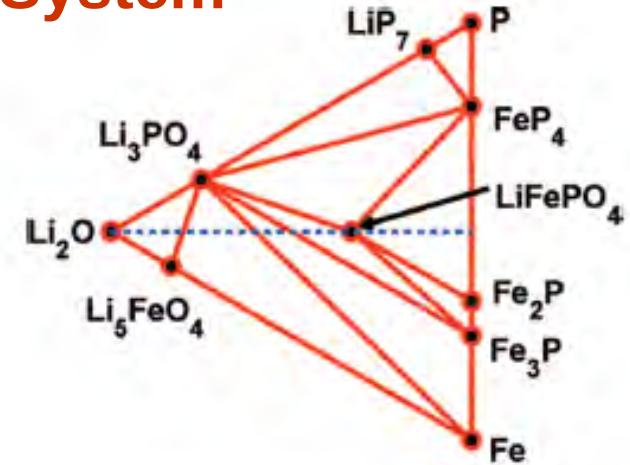


(a) $\mu_{O_2} = -13.08$ eV, LiFeP₂O₇ disappears

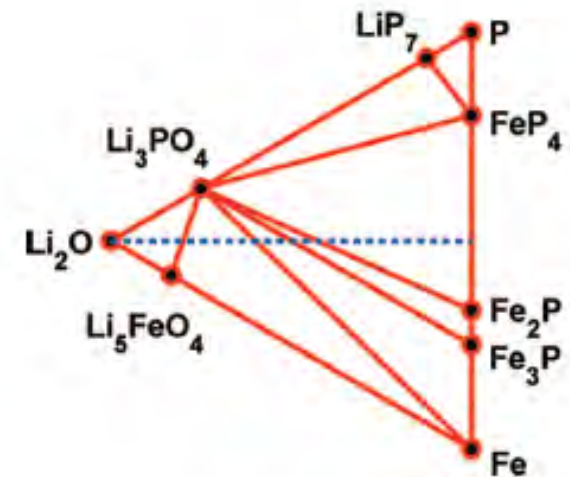


(b) $\mu_{O_2} = -16.08$ eV, Fe₂P₂O₇ disappears

Figure 4. Phase diagrams at highly reducing environments.



(a) $\mu_{O_2} = -16.70$ eV, Fe₃(PO₄)₂ disappears



(b) $\mu_{O_2} = -16.74$ eV, LiFePO₄ disappears

Figure 5. Phase diagrams at extremely reducing environments.

Li-Fe-P-O System

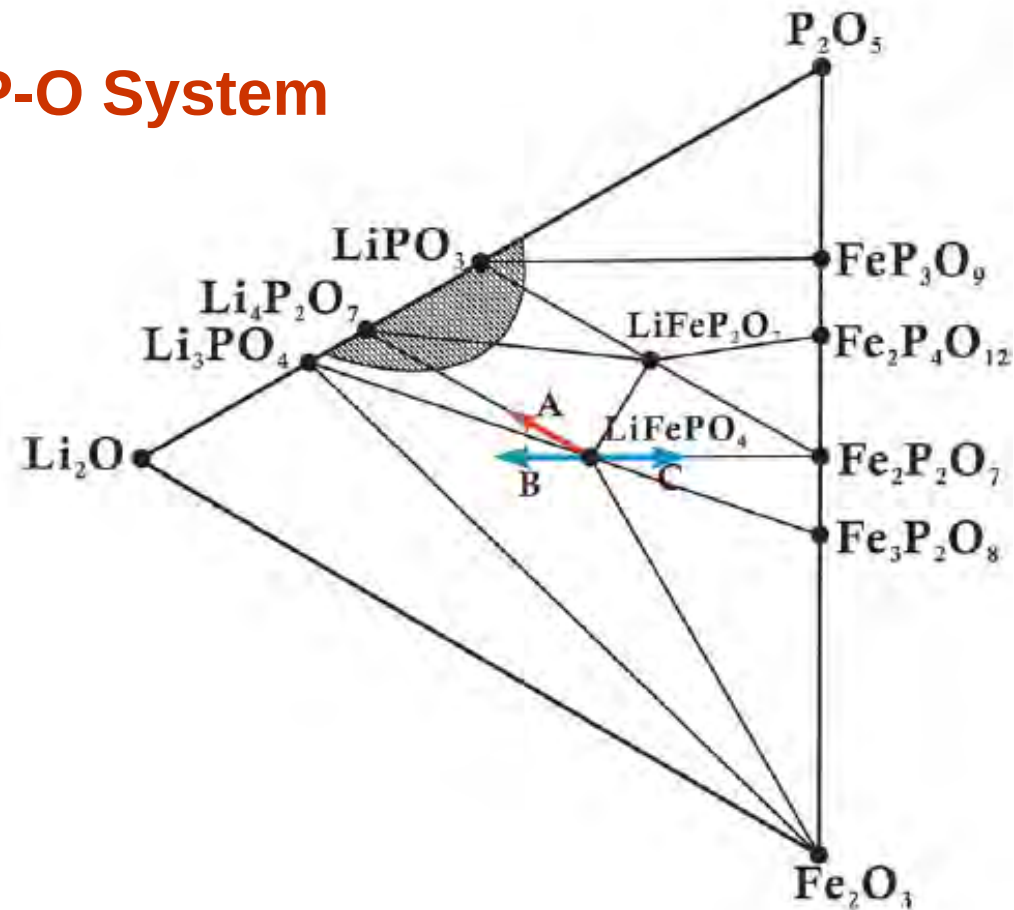


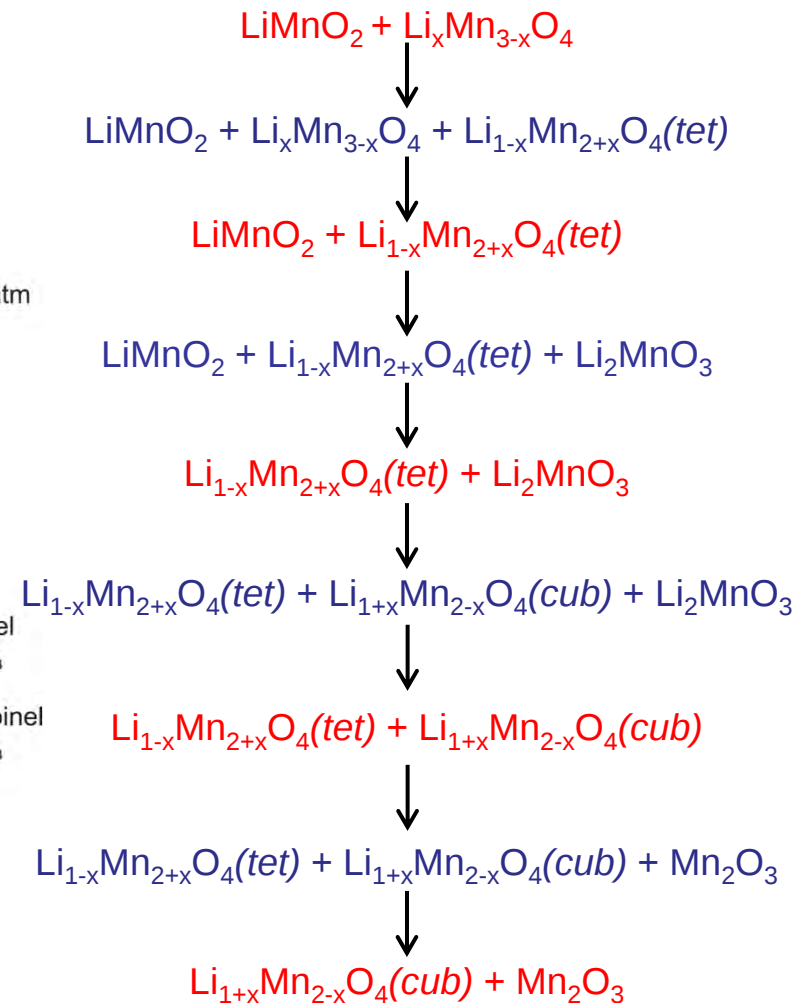
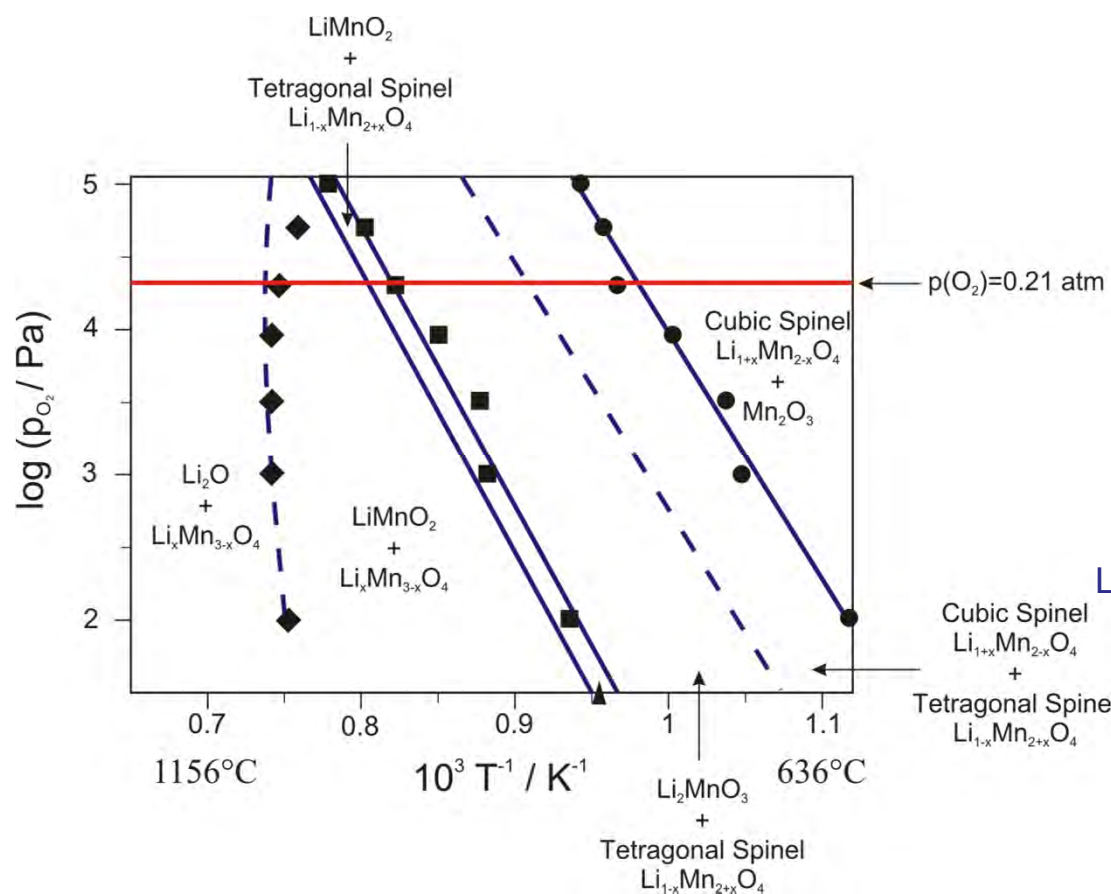
Figure S1. Calculated Li-Fe-P ternary phase diagram equilibrated with an oxygen potential under reducing conditions. The 'A' arrow indicates off-stoichiometry induced in the samples described in this Letter. The 'B' and 'C' arrow respectively indicate the more common one-to-one Fe/P deficiency and lithium deficiency. The shaded area in phase diagram indicates relevant coating compositions.

Kang and Ceder (2009)

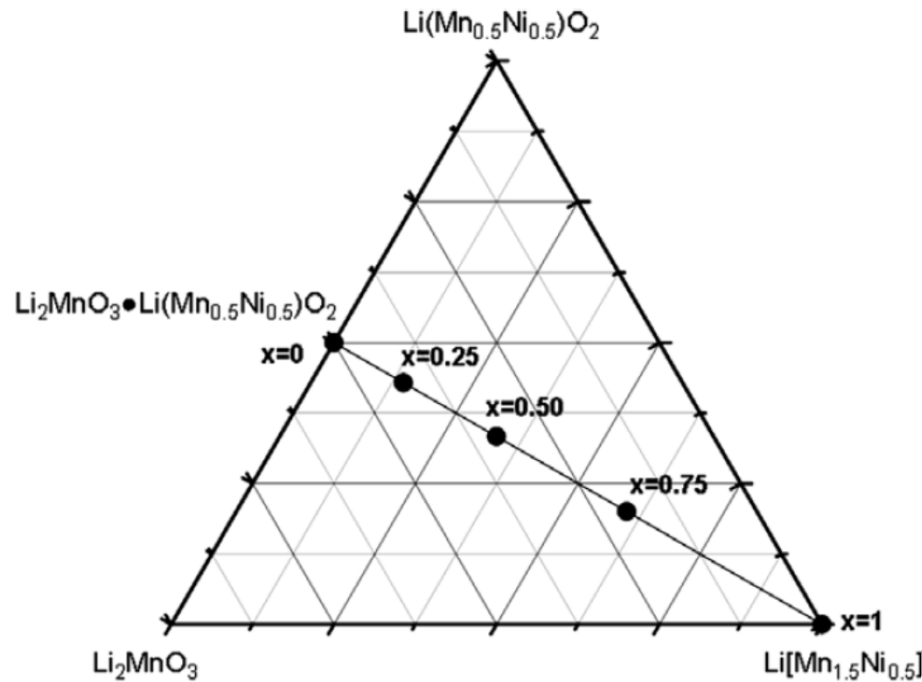
Thermodynamics of Lithium Battery Materials

- Materials Thermodynamics, Phase Diagrams and Electrochemistry to be simultaneously investigated
- Fundamental for electrochemical cell performance, understanding of thermal and safety behavior and for preparation of cathode materials
- Thermodynamics and phase diagrams even for the most important systems e.g. Li-Co-O, Li-Mn-O and Li-Fe-P-O to be investigated in more detail

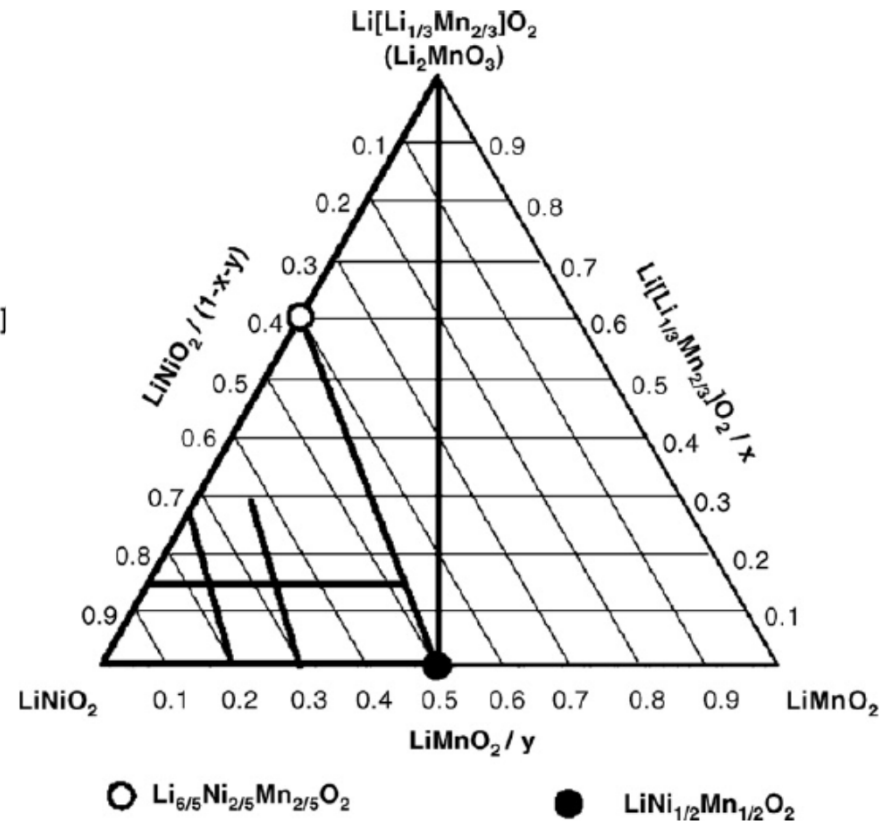
Li-Mn-O System



Li-Ni-Mn-Co-O System

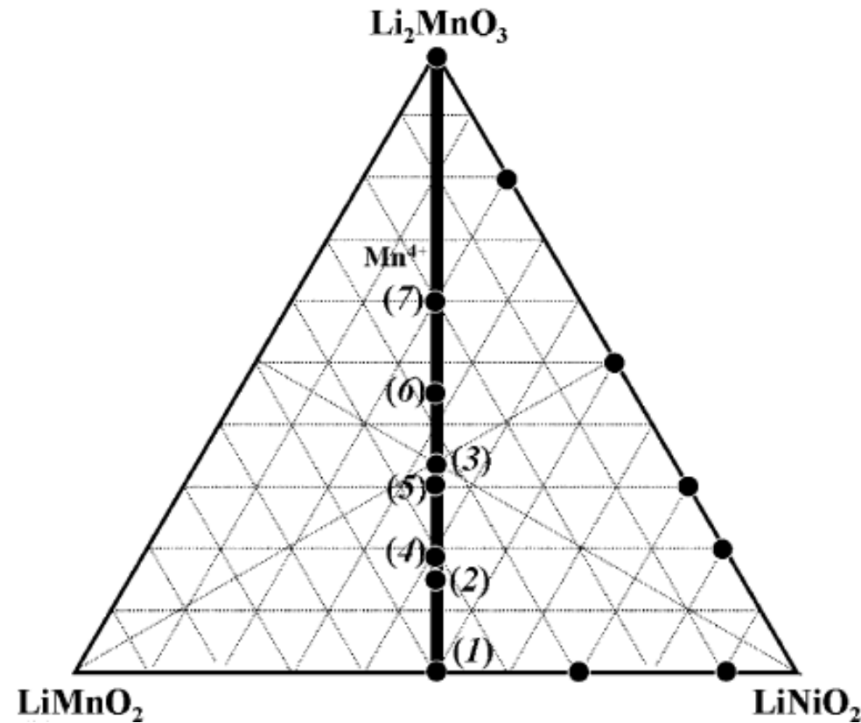


Phase compositions in the $\text{Li}[\text{Mn}_{1.5}\text{Ni}_{0.5}]\text{O}_4$ - Li_2MnO_3 - $\text{Li}[\text{Mn}_{0.5}\text{Ni}_{0.5}]\text{O}_4$ system (Park 2007).

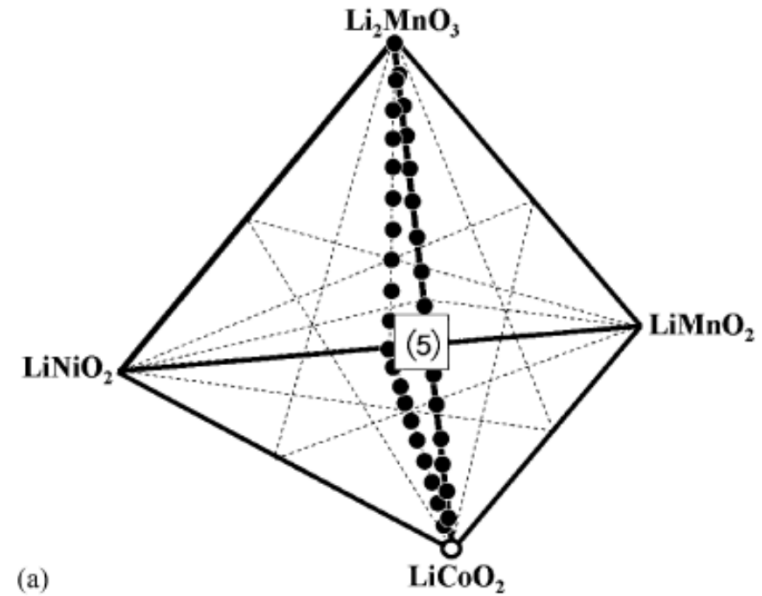


Composition triangle in the system LiNiO_2 - LiMnO_2 - $\text{Li}[\text{Li}_{1/3}\text{Mn}_{2/3}]\text{O}_2$. Bold lines represent the compositions which have been reported as single phase via a high temperature solid state reaction Zhang et al. (2008).

Li-Ni-Mn-Co-O System

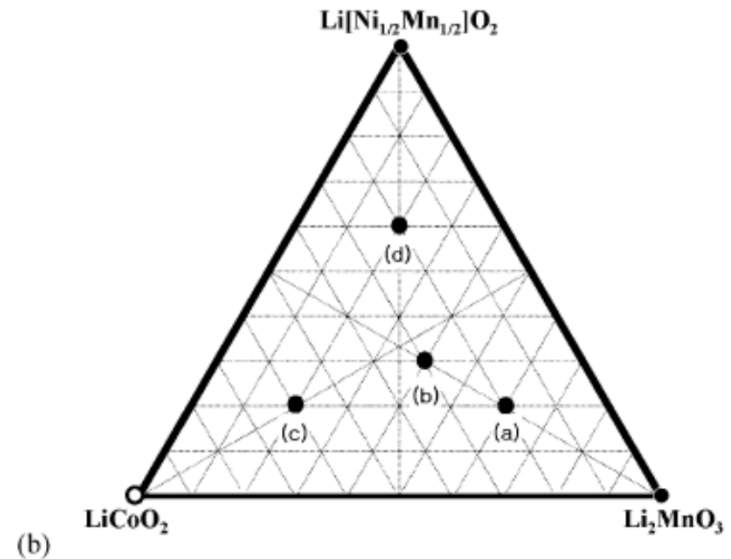


Triangle system Li_2MnO_3 - LiMnO_2 - LiNiO_2 (Park 2005).
Bold line indicates Mn oxidation state of +4.



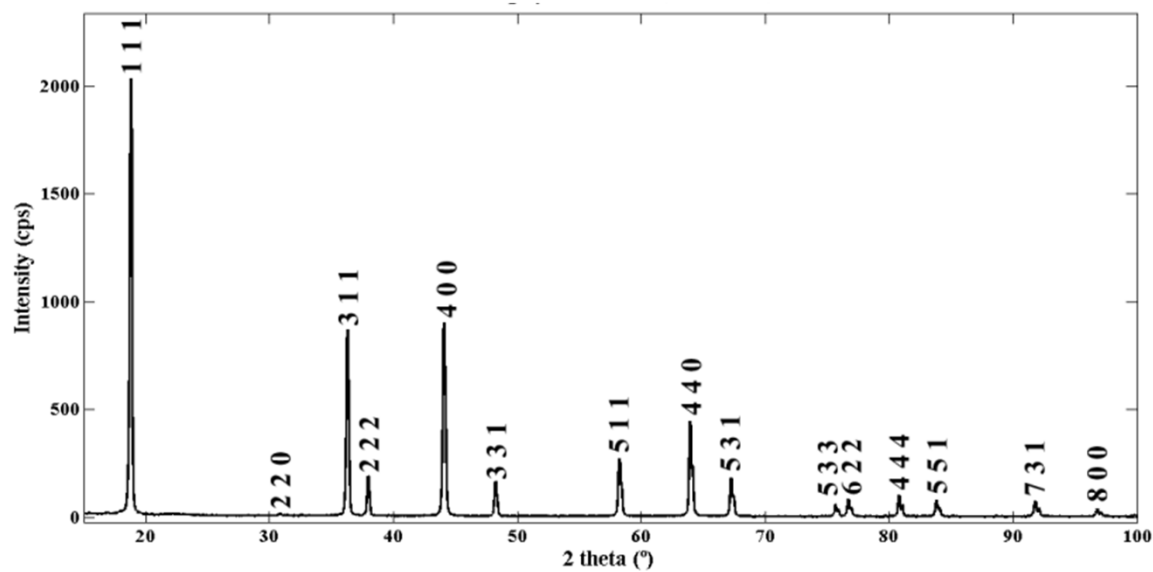
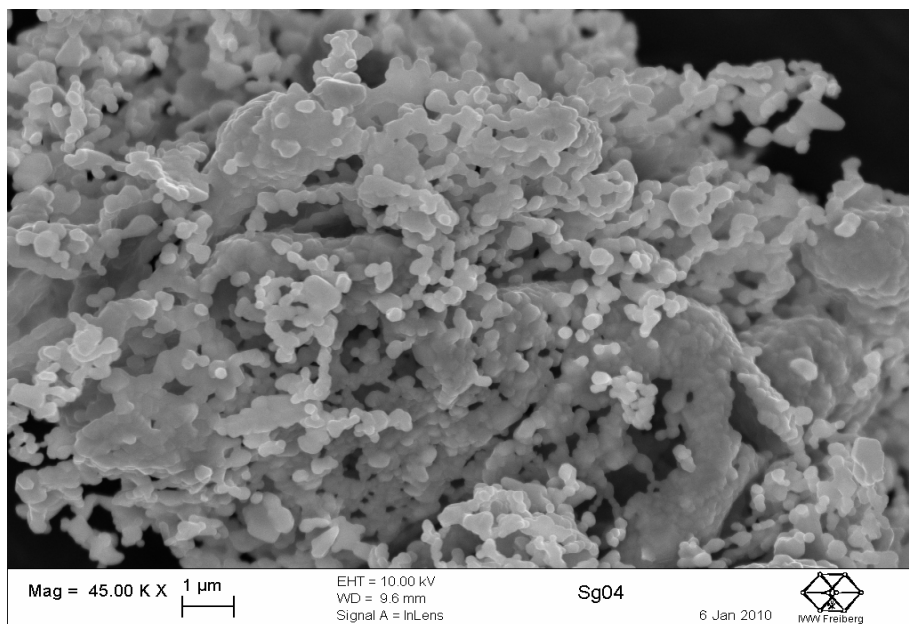
(a)

LiMnO_2 - LiCoO_2 - LiNiO_2 - Li_2MnO_3 phase diagram,
b) Section $\text{LiNi}_{1/2}\text{Mn}_{1/2}\text{O}_2$ - LiCoO_2 - Li_2MnO_3

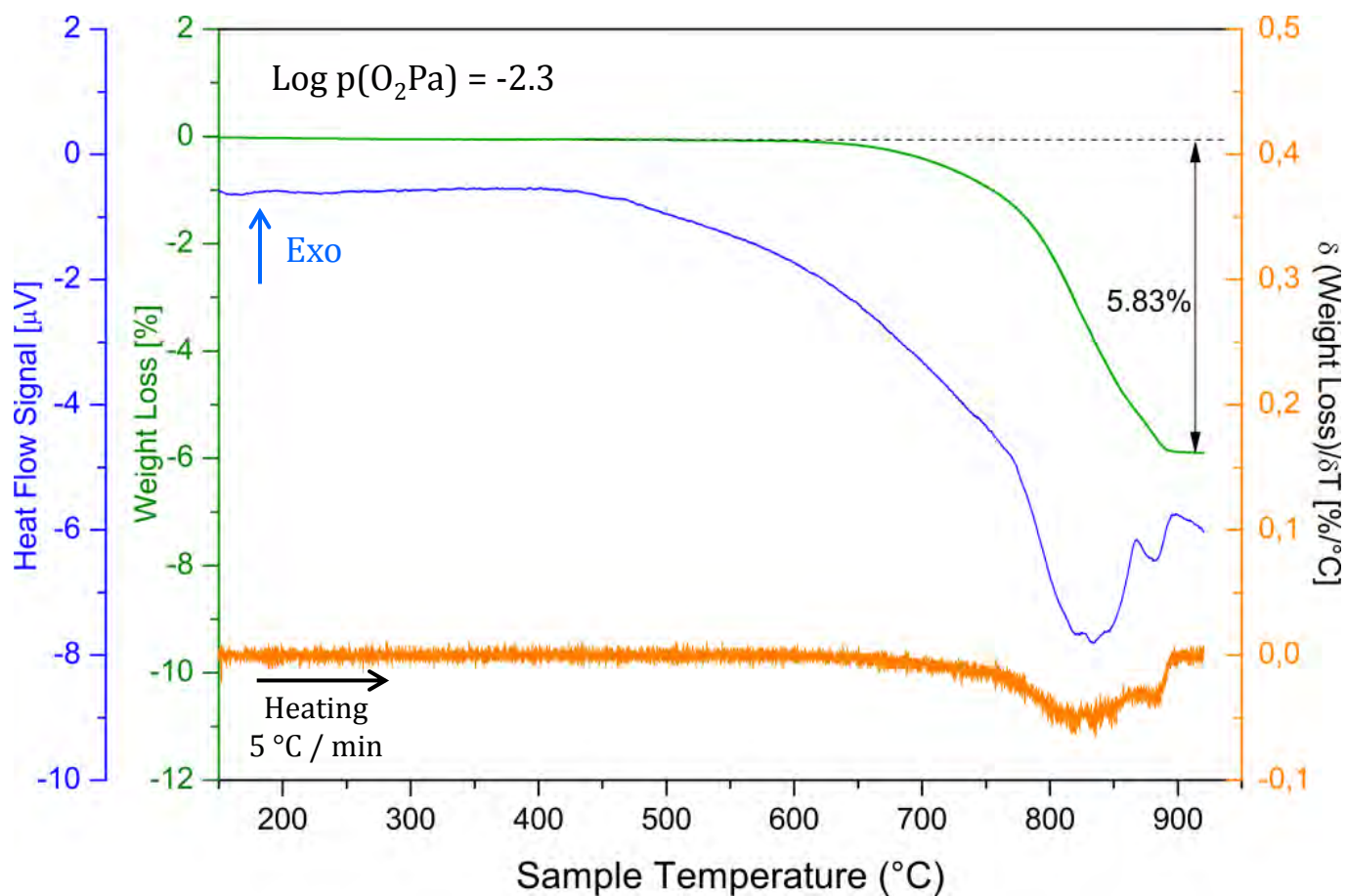


(b)

Li-Mn-O System



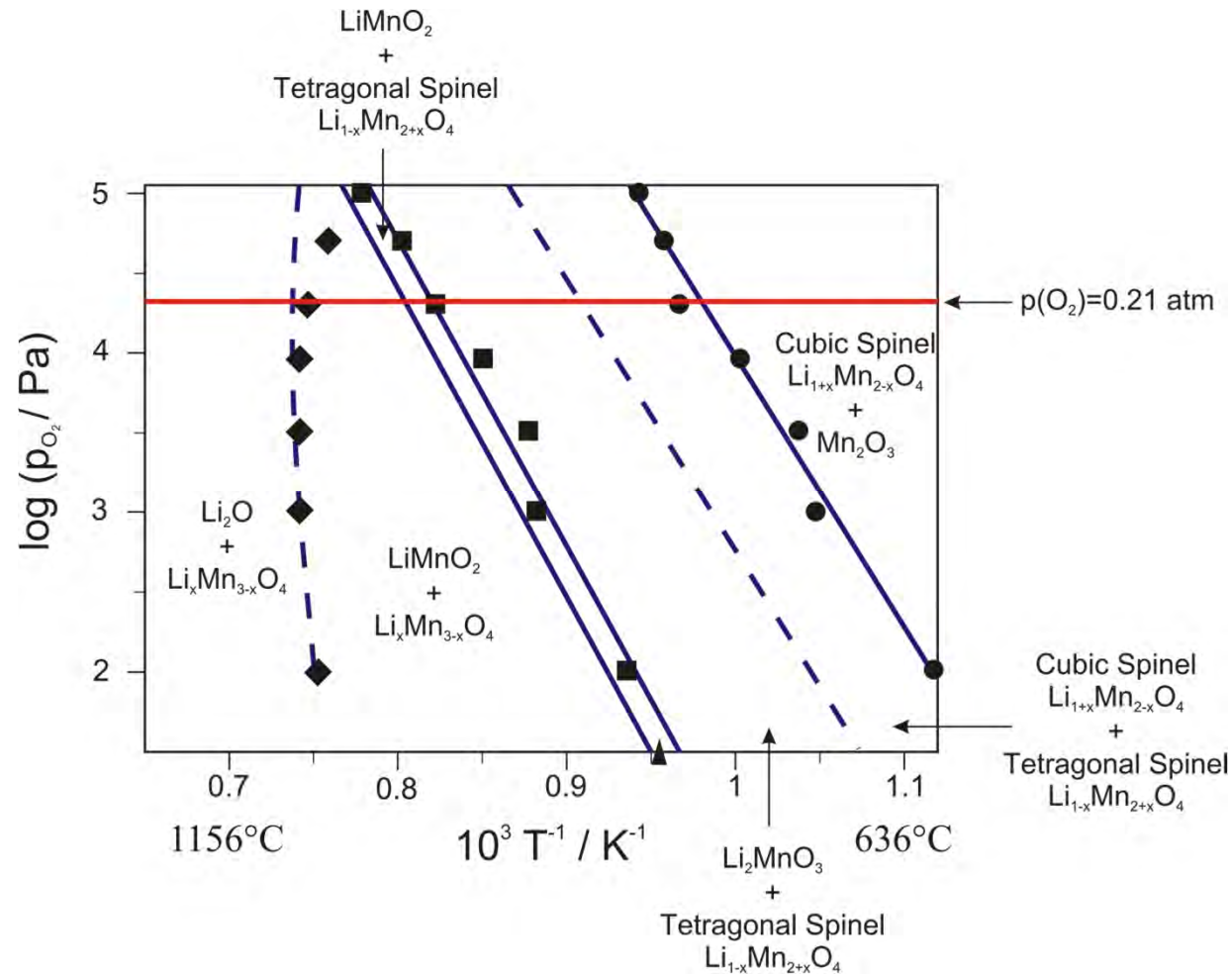
Li-Mn-O System



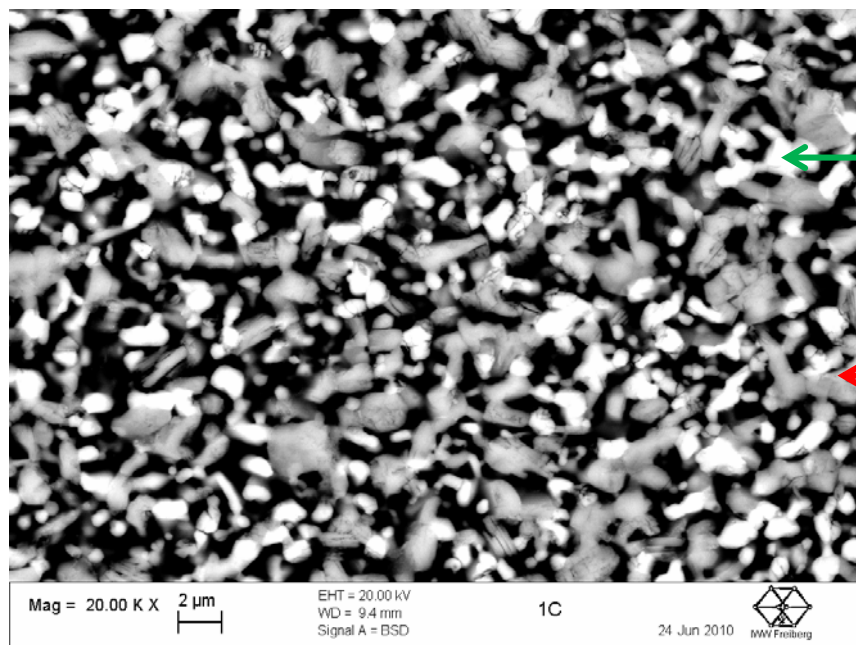
5.89% theoretical weight loss

Li-Mn-O System

- Reaction of stoichiometric LiMn_2O_4 at $\text{Log}(p_{\text{O}_2})=-2.3$ not indicated in the critically evaluated potential diagram for stoichiometric LiMn_2O_4

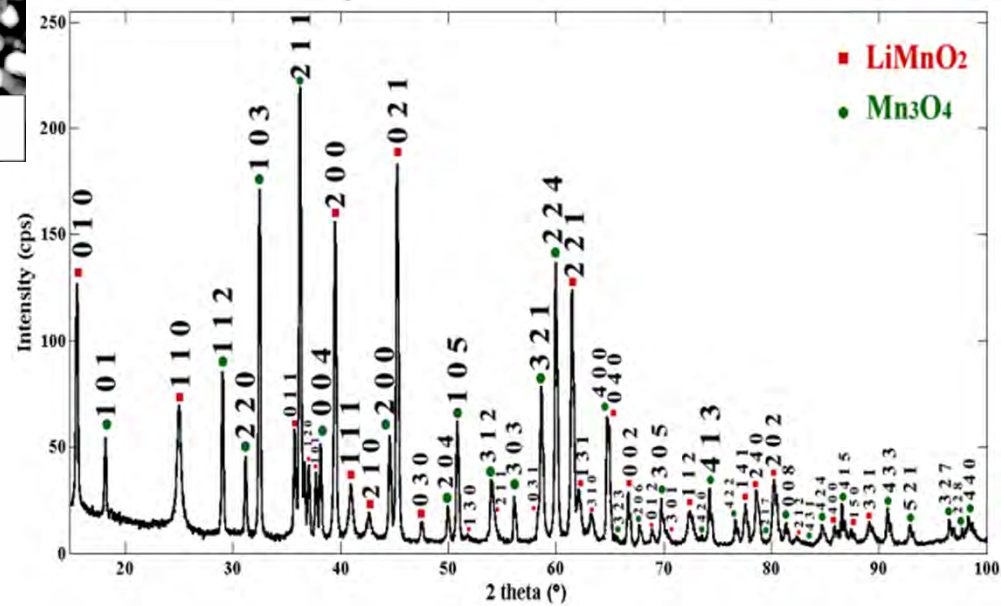


Li-Mn-O System

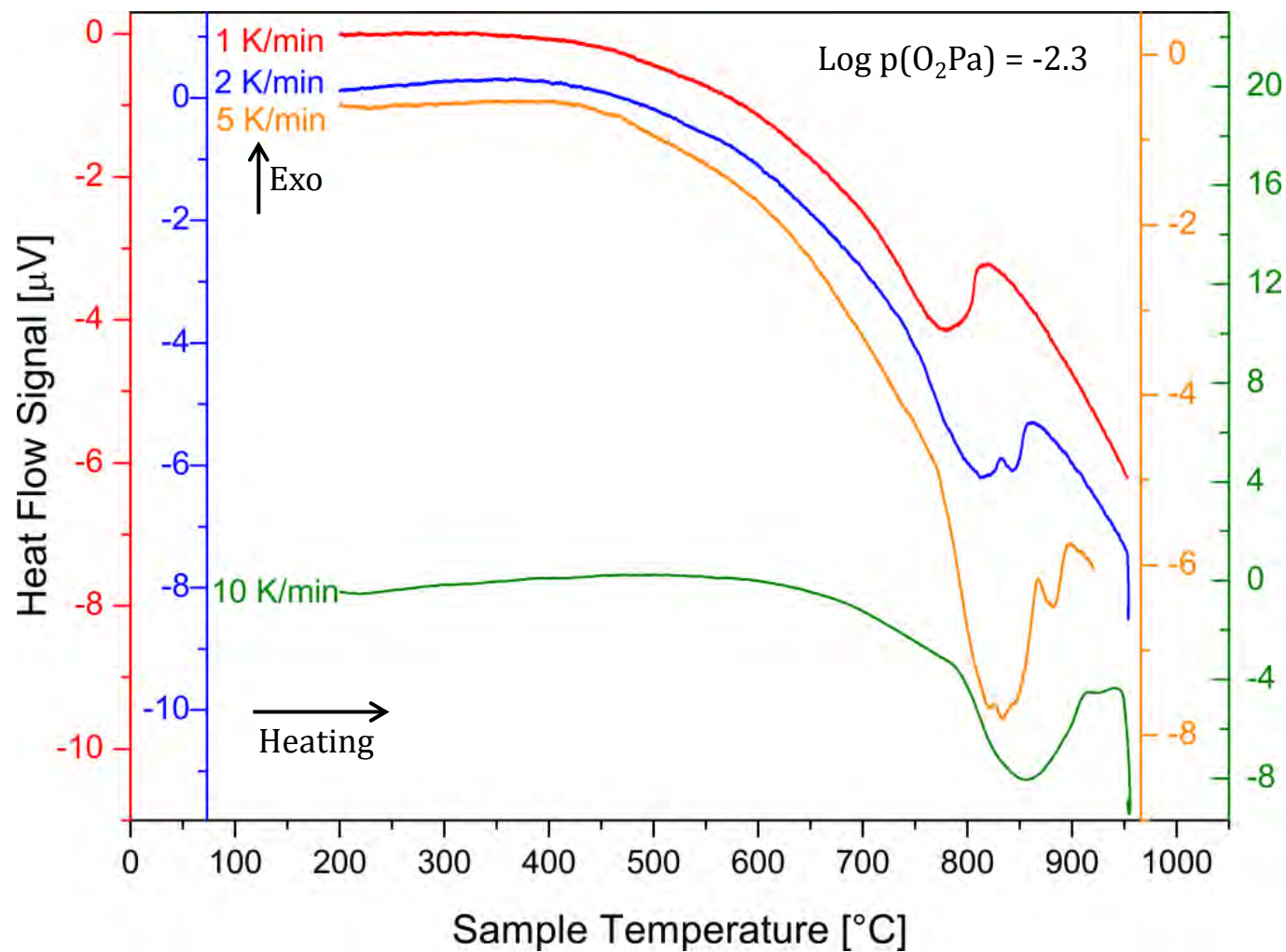


Mn_3O_4

LiMnO_2

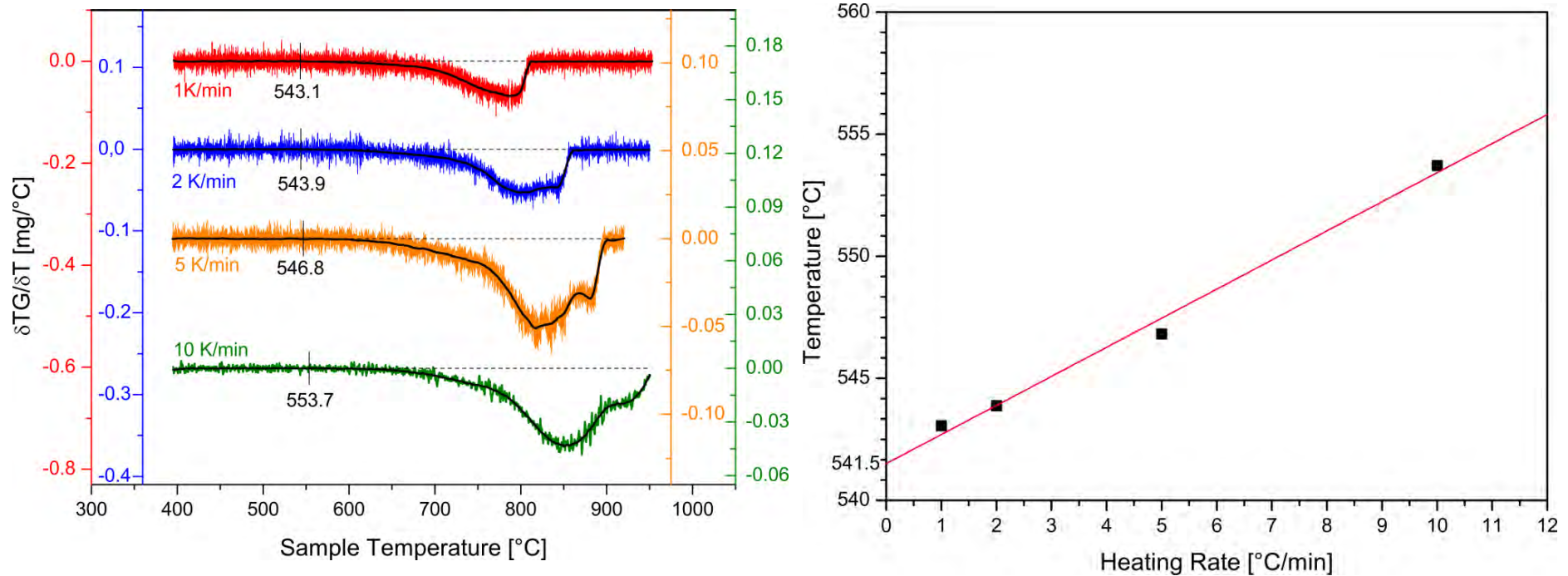


Li-Mn-O System



Li-Mn-O System

- Reaction temperature determined as first deviation of the 1st derivative of weight loss from baseline
- Reaction temperature at $\log(pO_2)=-2.3$ is 541.5°C



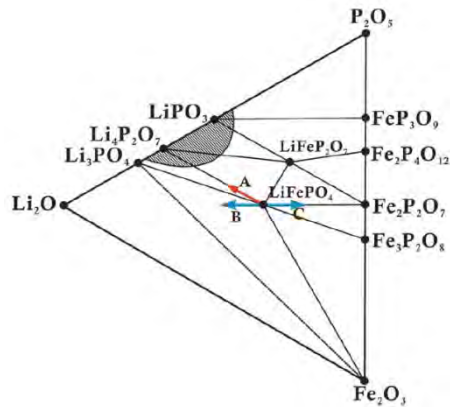
Thermodynamics of lithium ion batteries

Hans J. Seifert

Institute for Applied Materials – Applied Materials Physics (IAM-AWP)

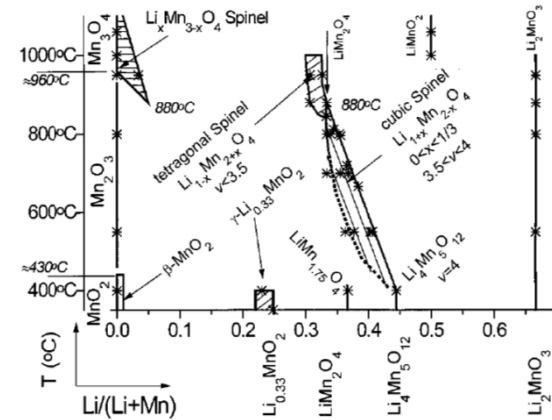


- SPP1473, Scientific Aims -



Materials

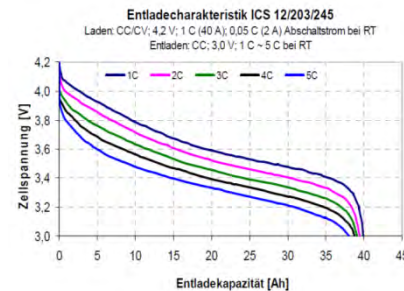
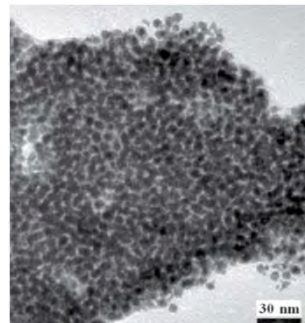
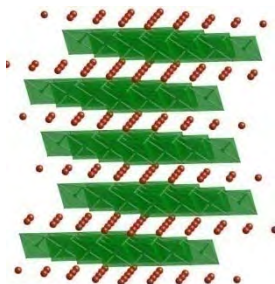
- Thermodynamics,
- Phase Diagrams,
- Kinetics



Micro- and Nanomaterials

**Crystal structures,
Crystal chemistry,
Microstructure,
Reactivity**

**Electrochemical
performance
and safety of
cells / batteries**



Li-Fe-P-O System

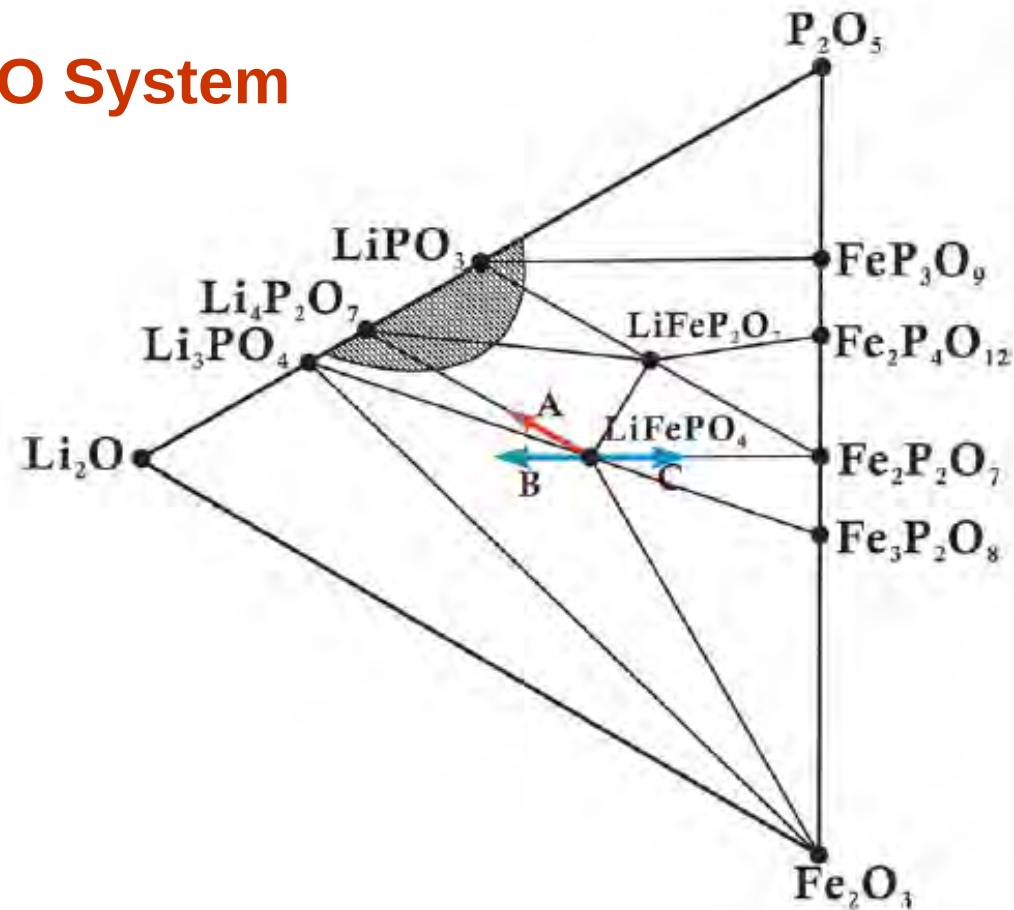
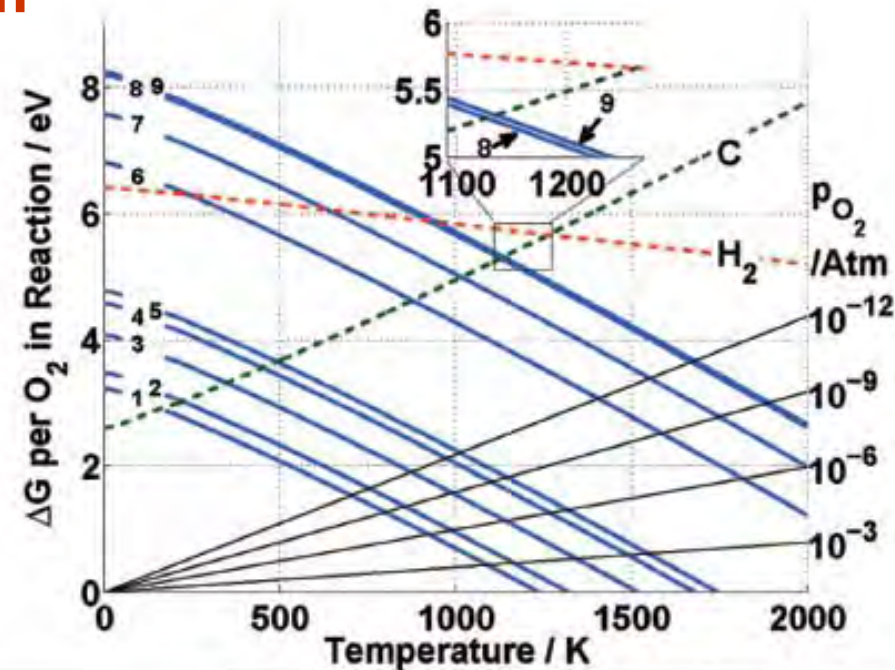


Figure S1. Calculated Li-Fe-P ternary phase diagram equilibrated with an oxygen potential under reducing conditions. The 'A' arrow indicates off-stoichiometry induced in the samples described in this Letter. The 'B' and 'C' arrow respectively indicate the more common one-to-one Fe/P deficiency and lithium deficiency. The shaded area in phase diagram indicates relevant coating compositions.

Kang and Ceder (2009)

Li-Fe-P-O System



Reaction	Line Label
$3 \text{Li}_3\text{Fe}_2(\text{PO}_4)_3 = 4 \text{LiFePO}_4 + 2 \text{LiFeP}_2\text{O}_7 + \text{Li}_3\text{PO}_4 + \text{O}_2$	1
$\frac{3}{2} \text{Fe}_7(\text{PO}_4)_6 = \text{Fe}_3(\text{P}_2\text{O}_7)_2 + \frac{5}{2} \text{Fe}_3(\text{PO}_4)_2 + \text{O}_2$	2
$2 \text{Fe}_3(\text{P}_2\text{O}_7)_2 = 2 \text{Fe}_2\text{P}_2\text{O}_7 + \text{Fe}_2\text{P}_4\text{O}_{12} + \text{O}_2$	3
$4 \text{LiFeP}_2\text{O}_7 = 4 \text{LiPO}_3 + 2 \text{Fe}_2\text{P}_2\text{O}_7 + \text{O}_2$	4
$6 \text{Fe}_2\text{O}_3 = 4 \text{Fe}_3\text{O}_4 + \text{O}_2$	5
$2 \text{Fe}_3\text{O}_4 = 6 \text{FeO} + \text{O}_2$	6
$\frac{6}{5} \text{Fe}_2\text{P}_2\text{O}_7 = \frac{4}{5} \text{Fe}_3(\text{PO}_4)_2 + \frac{4}{5} \text{P} + \text{O}_2$	7
$2 \text{FeO} = 2 \text{Fe} + \text{O}_2$	8
$\frac{1}{4} \text{Fe}_3(\text{PO}_4)_2 = \frac{1}{28} \text{FeP}_4 + \frac{5}{14} \text{Fe}_2\text{P} + \text{O}_2$	
$\frac{3}{4} \text{LiFePO}_4 = \frac{1}{4} \text{Li}_3\text{PO}_4 + \frac{5}{14} \text{Fe}_2\text{P} + \frac{1}{28} \text{FeP}_4 + \text{O}_2$	9
$2\text{CO} = 2\text{C} + \text{O}_2$	C
$2\text{H}_2\text{O} = 2\text{H}_2 + \text{O}_2$	H ₂

Figure 6. Modified Ellingham diagram for reduction reactions in the Li-Fe-P-O₂ system.

Ong et al. (2008)

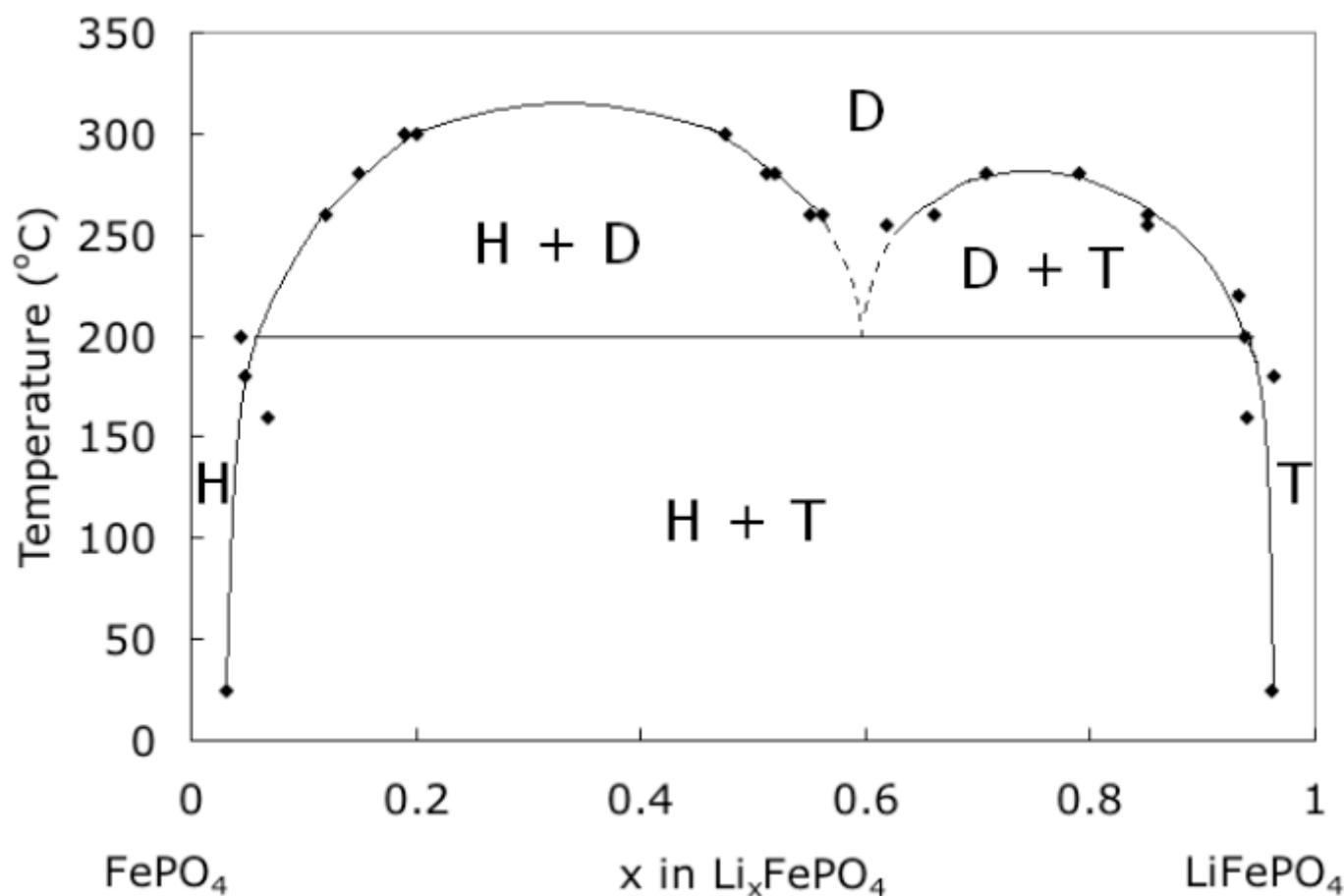
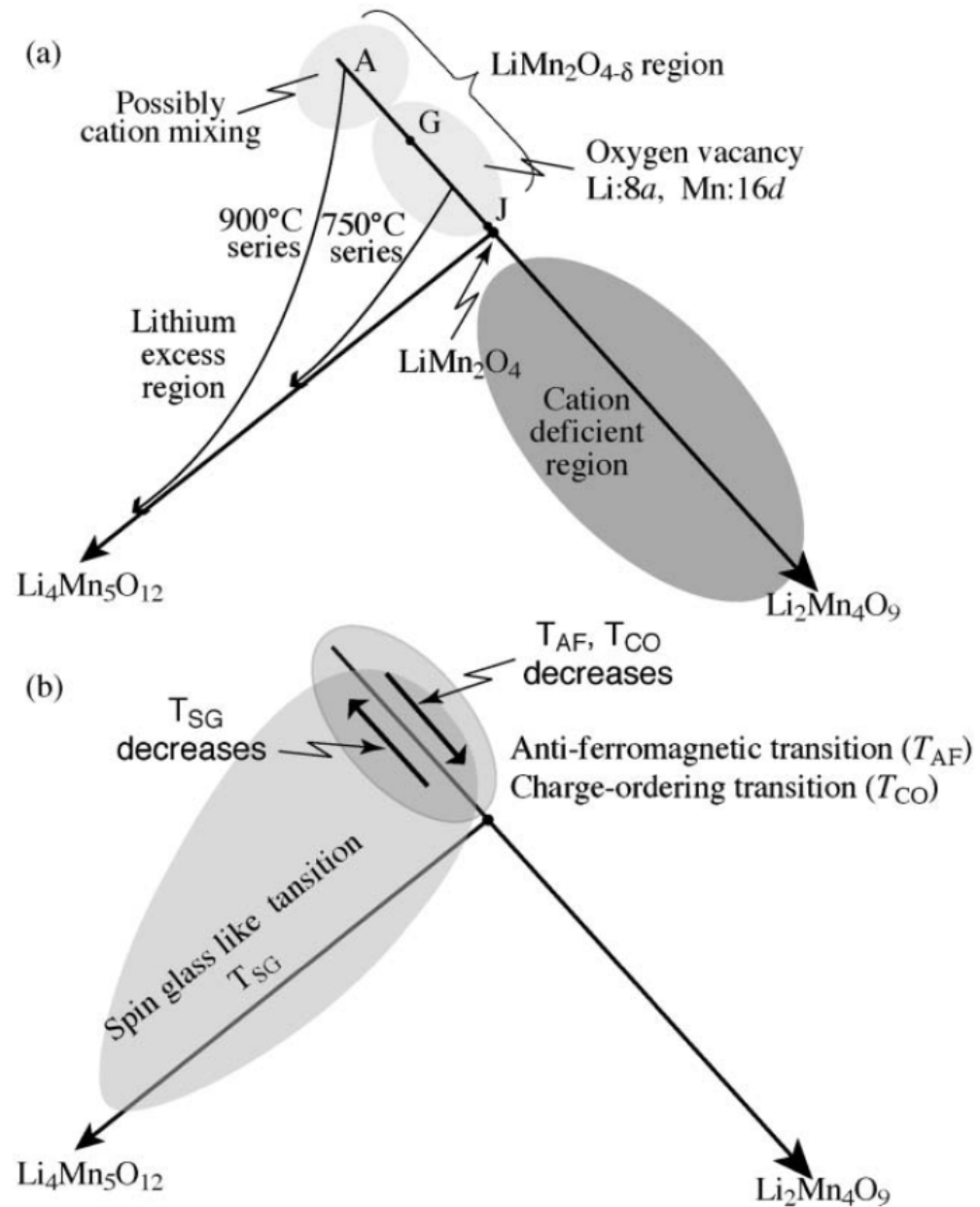


Figure 6. Phase diagram of LiFePO_4 (T, for triphylite) and FePO_4 (H, for heterosite) phases showing their merging to a solid solution (D, for disordered) in a eutectoid system. Data points at 25°C are based on published work by Yamada [10]. The eutectoid point is around the composition $x = 0.6$ and temperature 200°C . Above 200°C , mixtures of heterosite or triphylite and the disordered phase were seen up to around 300°C . Above 300°C , the disordered phase dominates.

Li-Fe-P-O System

Dodd et al. (2006)

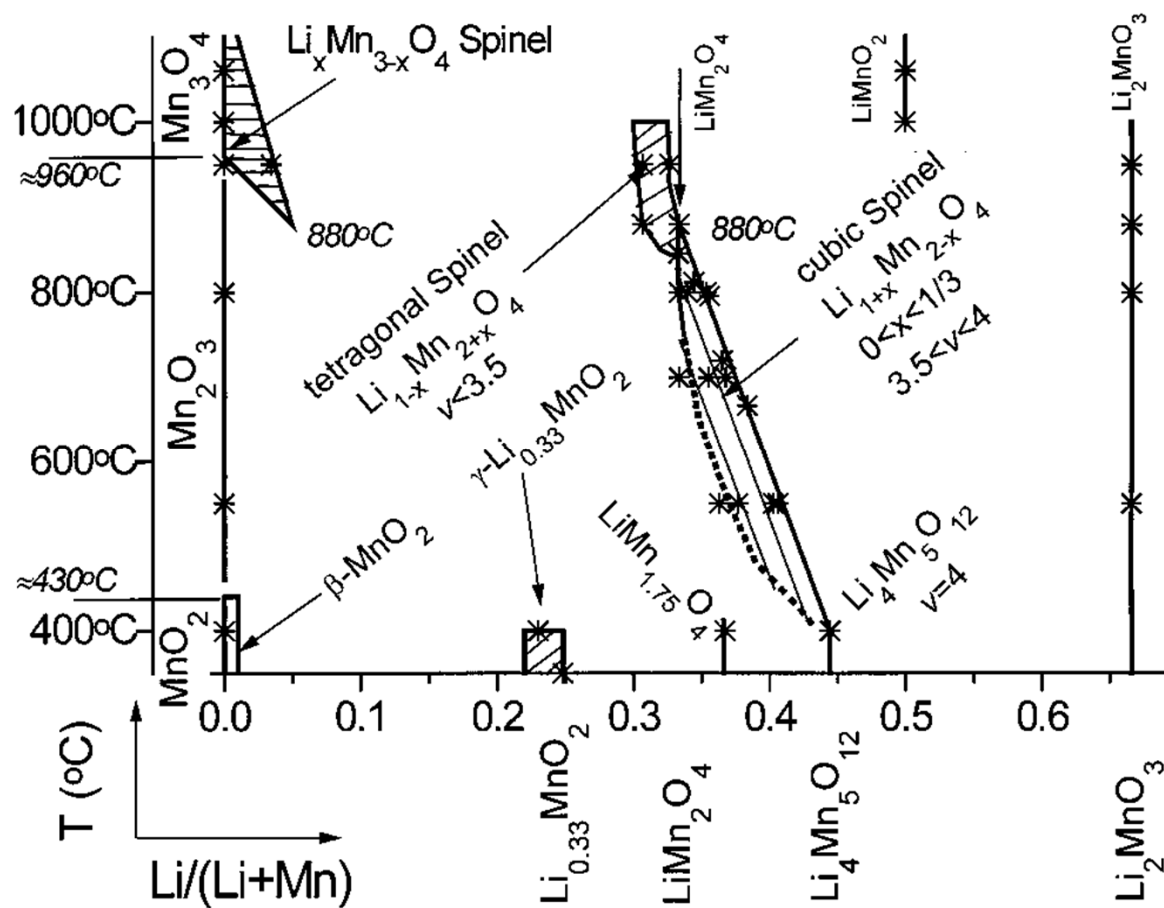
Li-Mn-O System



Detailed phase relationships in the subsystem
 LiMn_2O_4 - $\text{Li}_4\text{Mn}_5\text{O}_{12}$ - $\text{Li}_2\text{Mn}_4\text{O}_9$ (Yonemura et al. 2004).

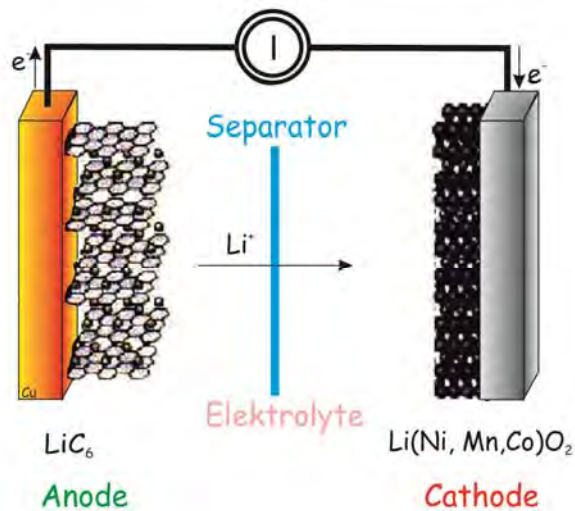
Li-Mn-O System

$p(\text{O}_2)=0.21 \text{ atm}$

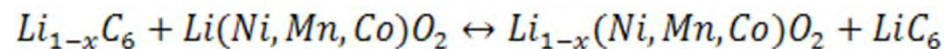
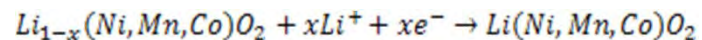
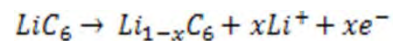


Lithium Ion Battery

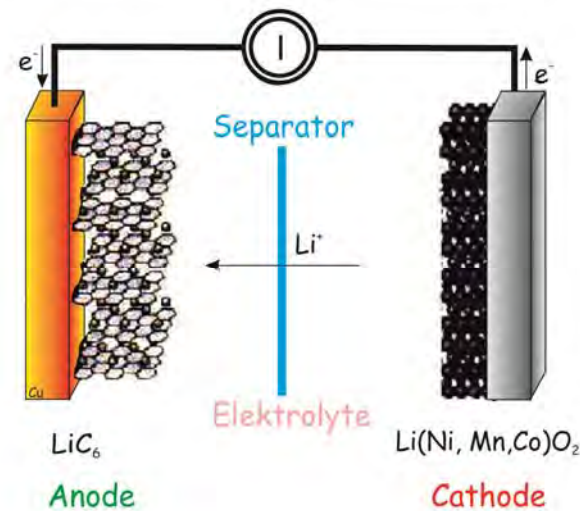
discharging



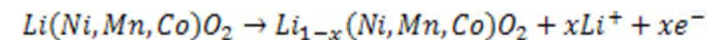
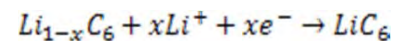
material of anode oxidized /
material of cathode reduced



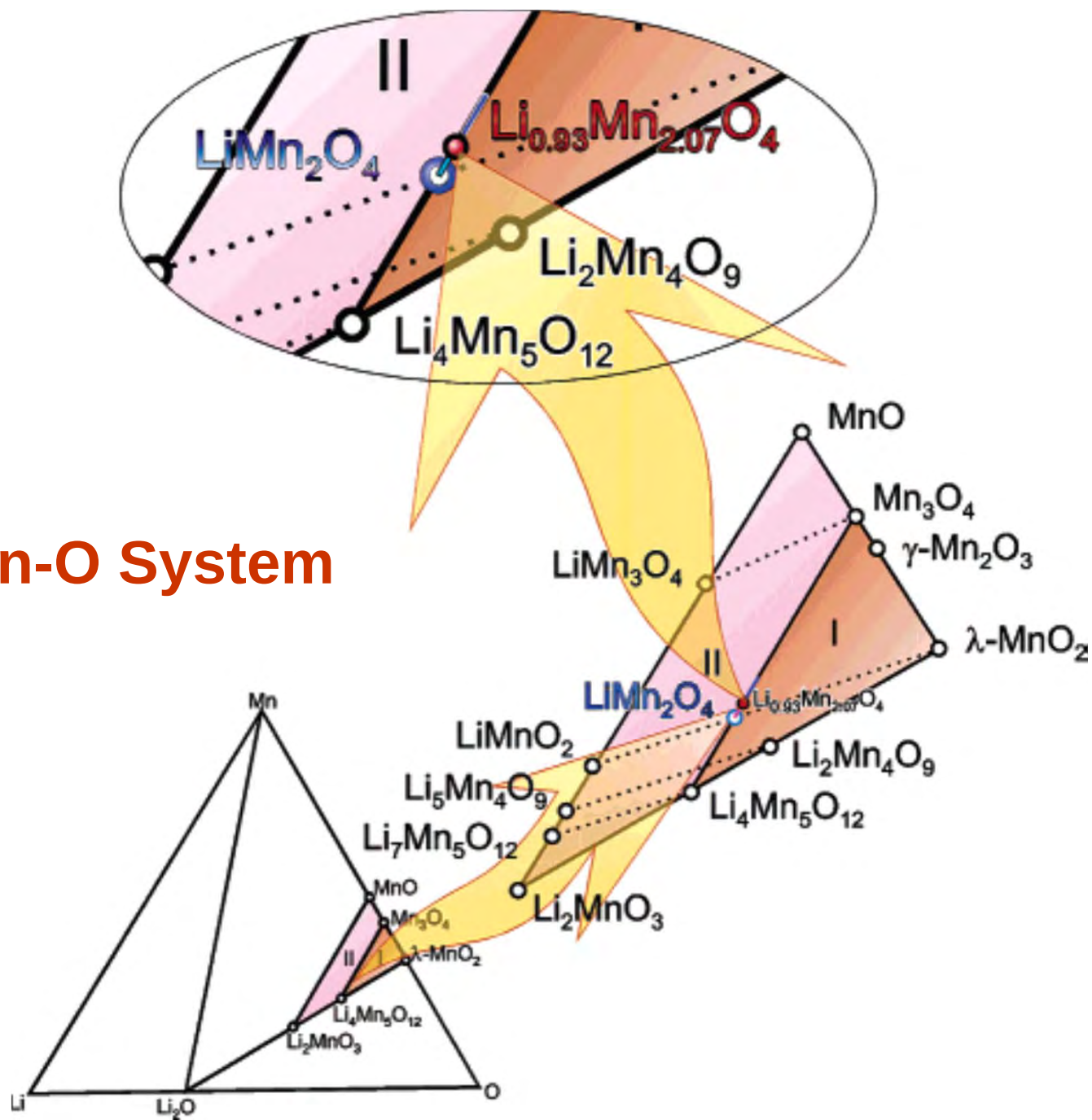
charging



material of anode reduced /
material of cathode oxidized

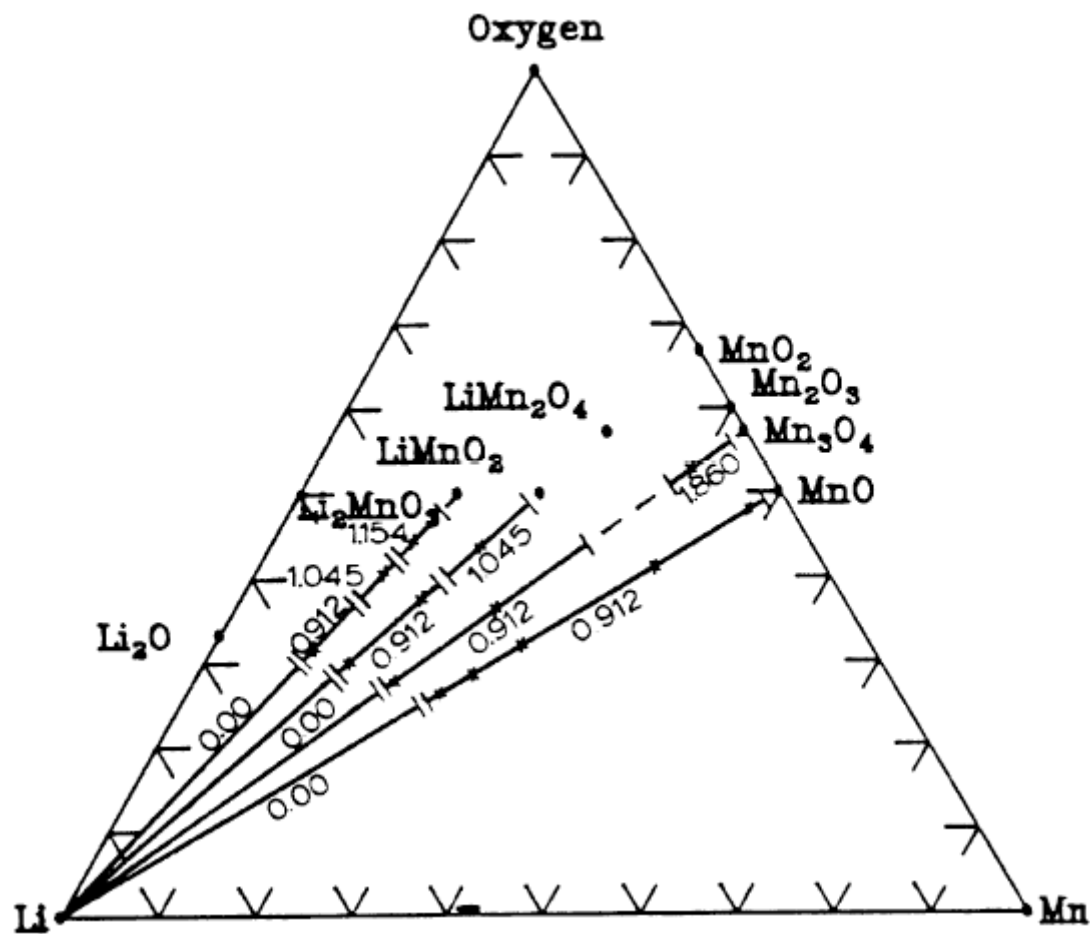


Li-Mn-O System



Li-Mn-O System

R. Huggins, Advanced Batteries



Heat generation rates

$$Q = \Delta G + T\Delta S + W_{el}$$

$\Delta G = -nFE_{eq}$

$\Delta S = nF \frac{dE_{eq}}{dT}$

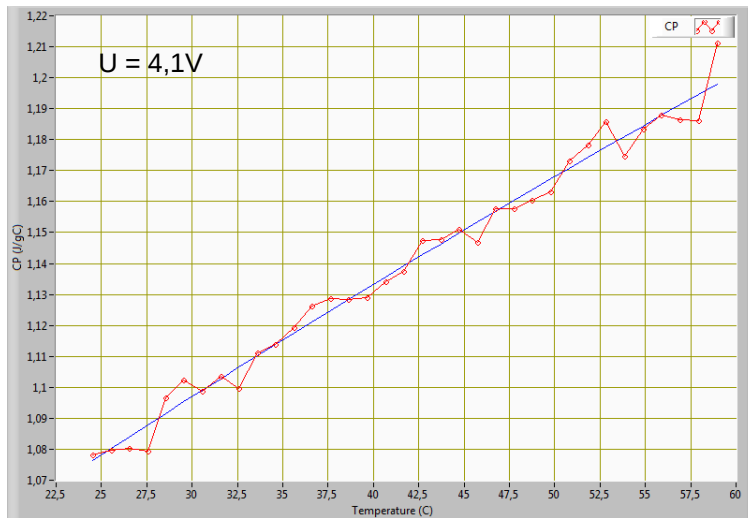
$W_{el} = -nFE$

$$q = I \left[(E_{eq} - E) + T \frac{dE_{eq}}{dT} \right] + q_p$$

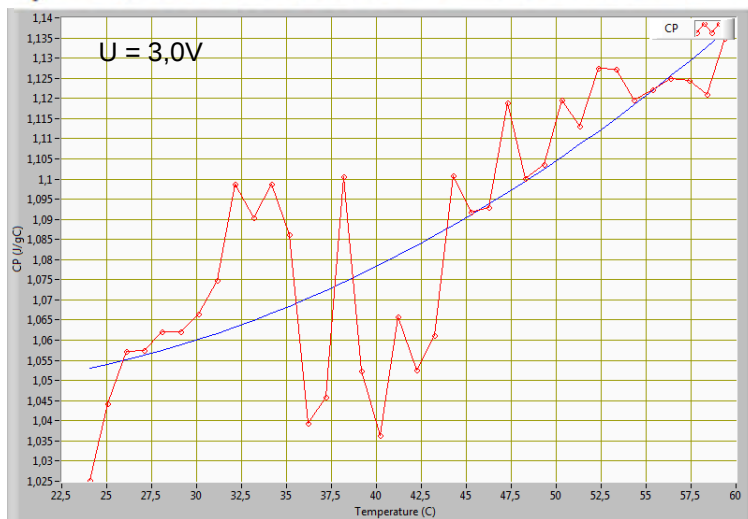
Sources of heat generation:

- | | |
|---|-----------------------------------|
| 1. The “reversible” heat released (or absorbed) by the chemical reaction of the cell | $q_{rev} = IT \frac{dE_{eq}}{dT}$ |
| 2. The “irreversible” heat generation by ohmic resistance and polarisation | $q_{irrev} = I(E_{eq} - E)$ |
| 3. The heat generation by “side reactions”,
i.e. parasitic/corrosion reactions and “chemical shorts” | q_p |

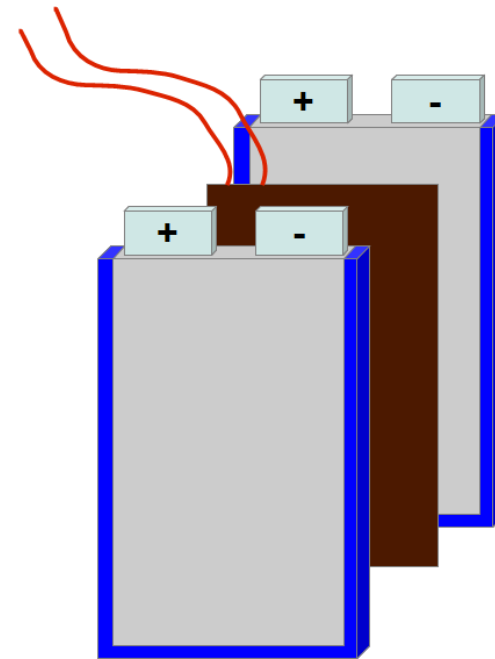
$C_{p, \text{eff}}$ measurement on a 40Ah pouch cell



$$c_p = 0,96511 + 0,00491 \cdot T - 1,76899 \cdot 10^{-5} \cdot T^2$$

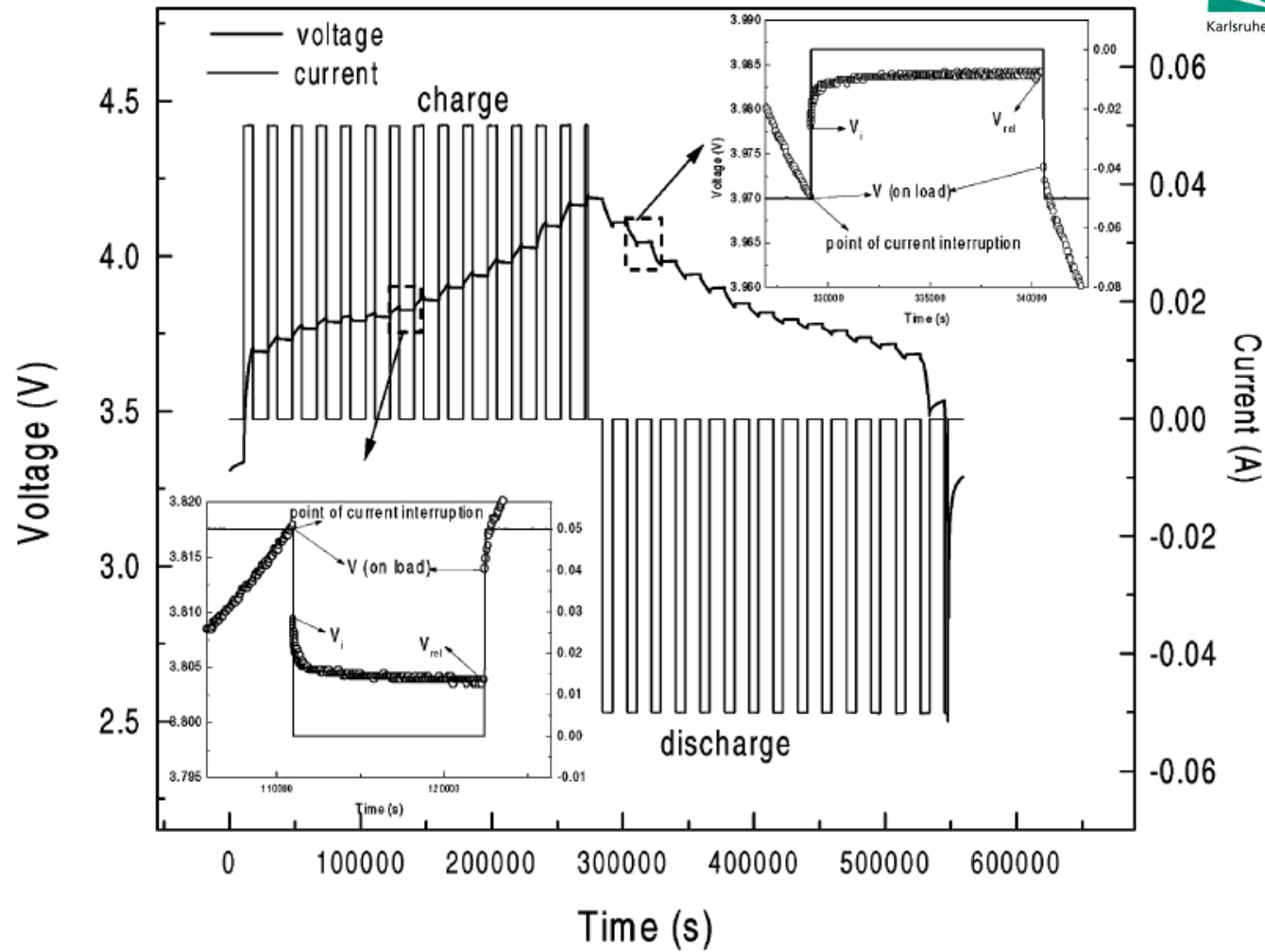


$$c_p = 1,05414 - 0,00102 \cdot T + 4,05094 \cdot 10^{-5} \cdot T^2$$



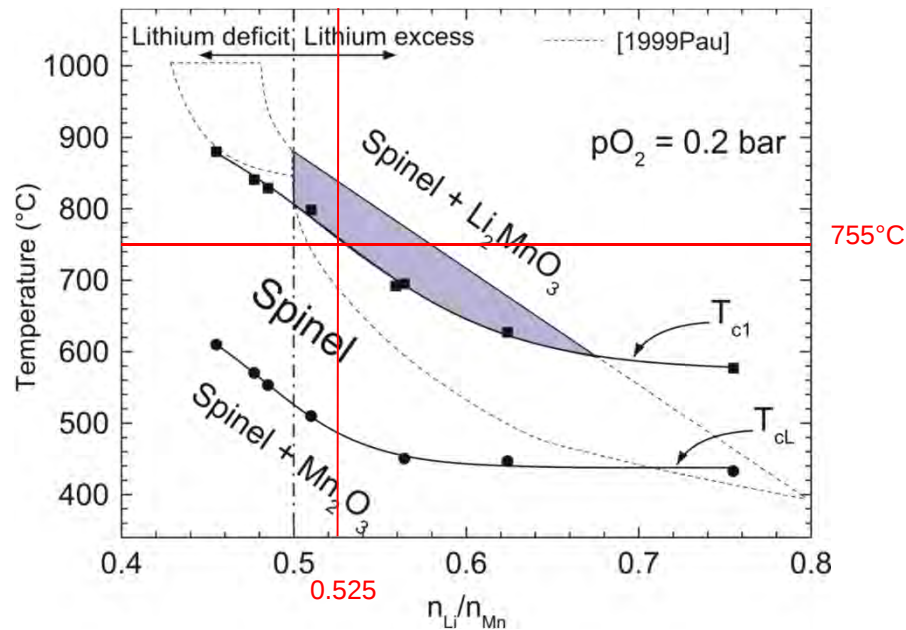
$$c_p = \frac{q}{m\Delta T} \quad q = \int U \cdot I dt$$

Separation of reversible and irreversible parts



$$Q_{rev} = n_{Li} T \Delta S = T \left(\frac{\partial E_{eq}}{\partial T} \right) (It)_{dc}$$

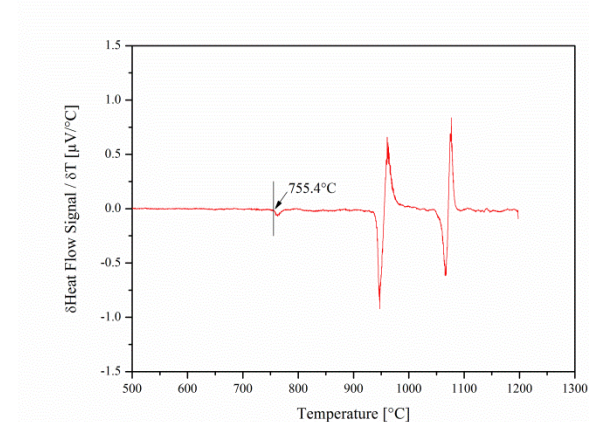
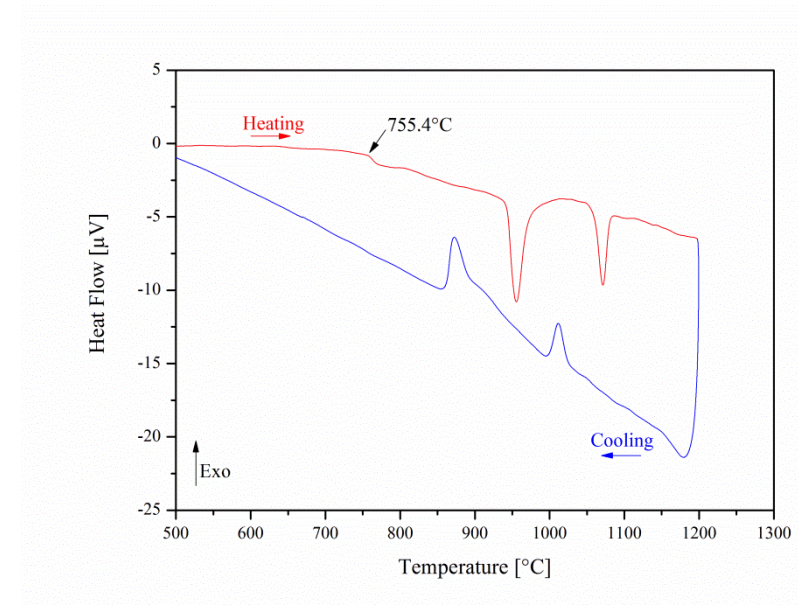
Enthalpy of Drop Solution of $\text{Li}_{1+x}\text{Mn}_{2-x}\text{O}_{4-\delta}$



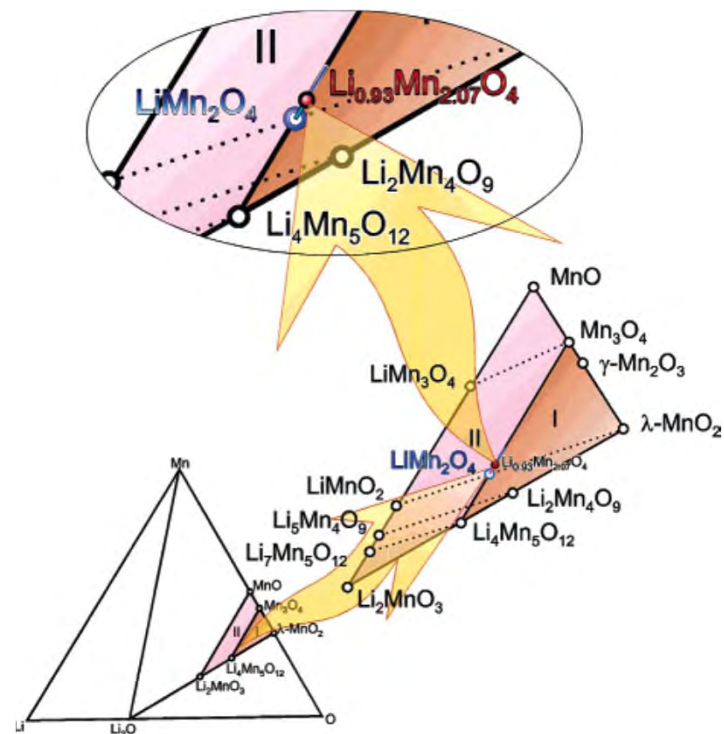
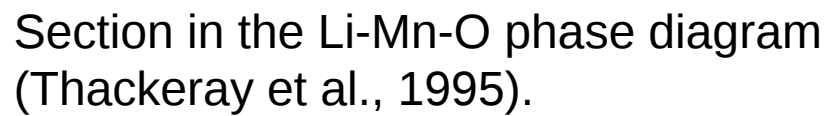
Li-Mn-O Temperature-Composition Ratio Section

- Samples prepared using a modified Pechini method
- The homogeneity range of the spinel phase determined using thermogravimetric analysis at $p\text{O}_2=0.2 \text{ atm}$

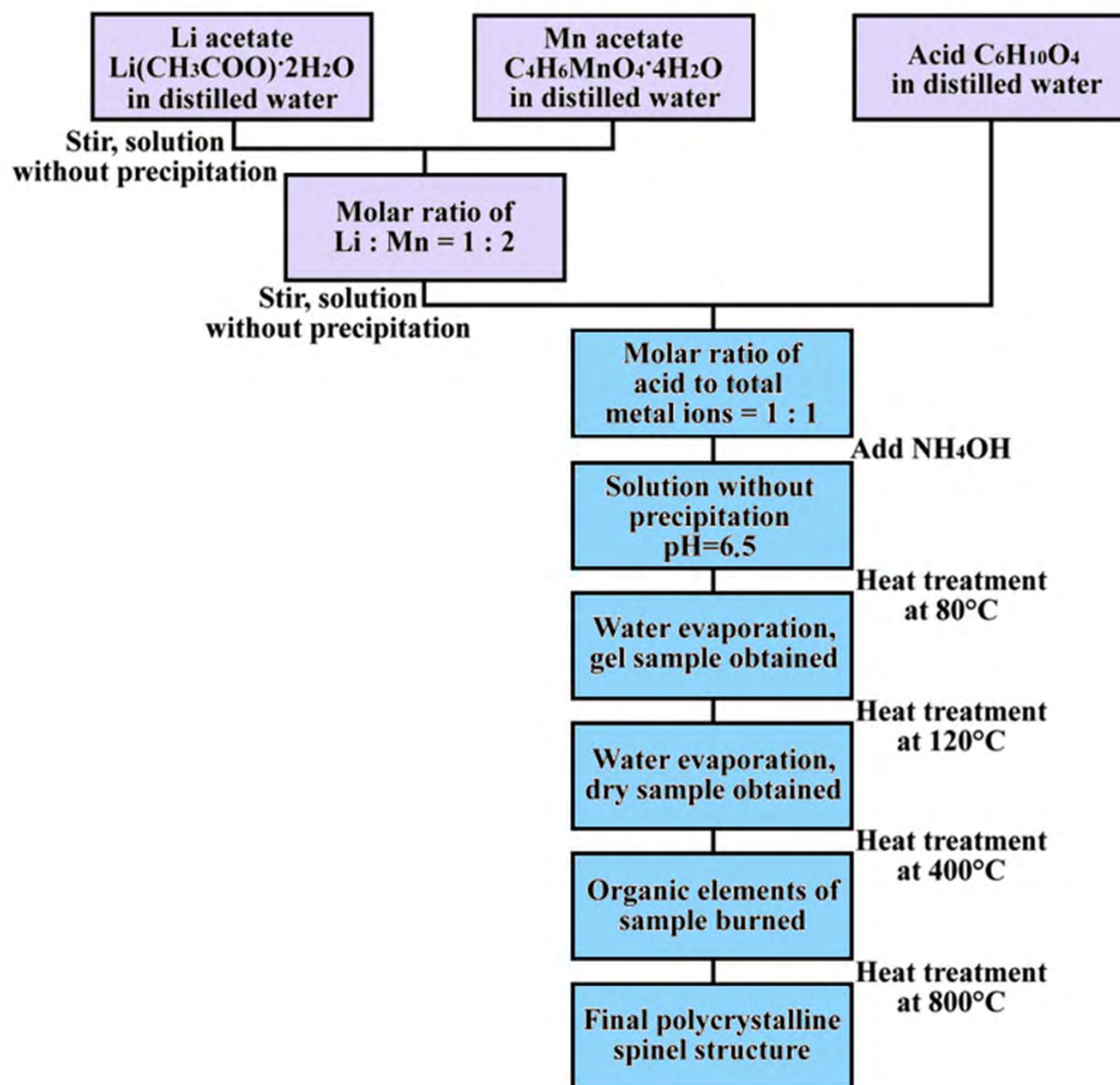
Li-rich boundary of the homogeneity range $\text{Li}_{1+x}\text{Mn}_{2-x}\text{O}_4$ should be refined



C = Cubic
T = Tetragonal

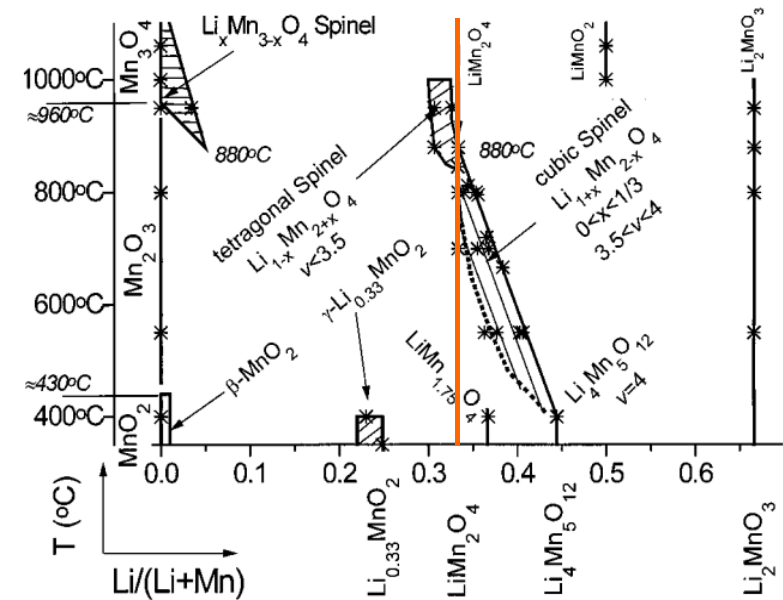
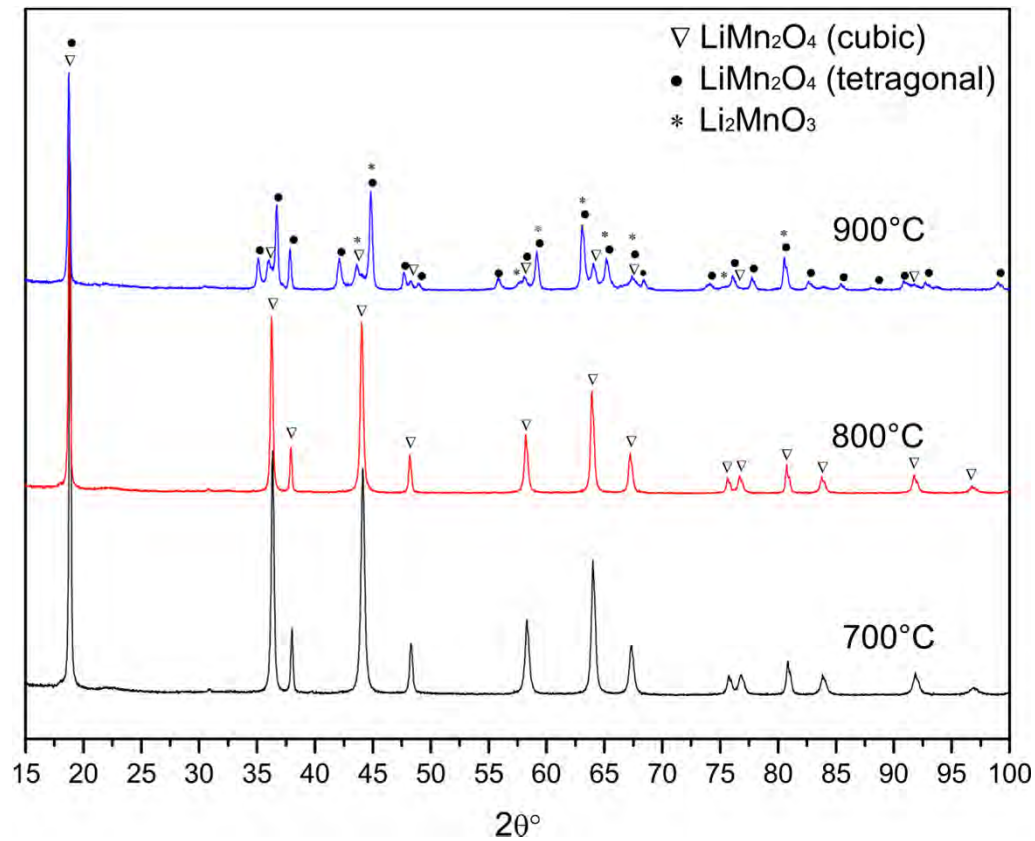


Li-Mn-O System, sample preparation

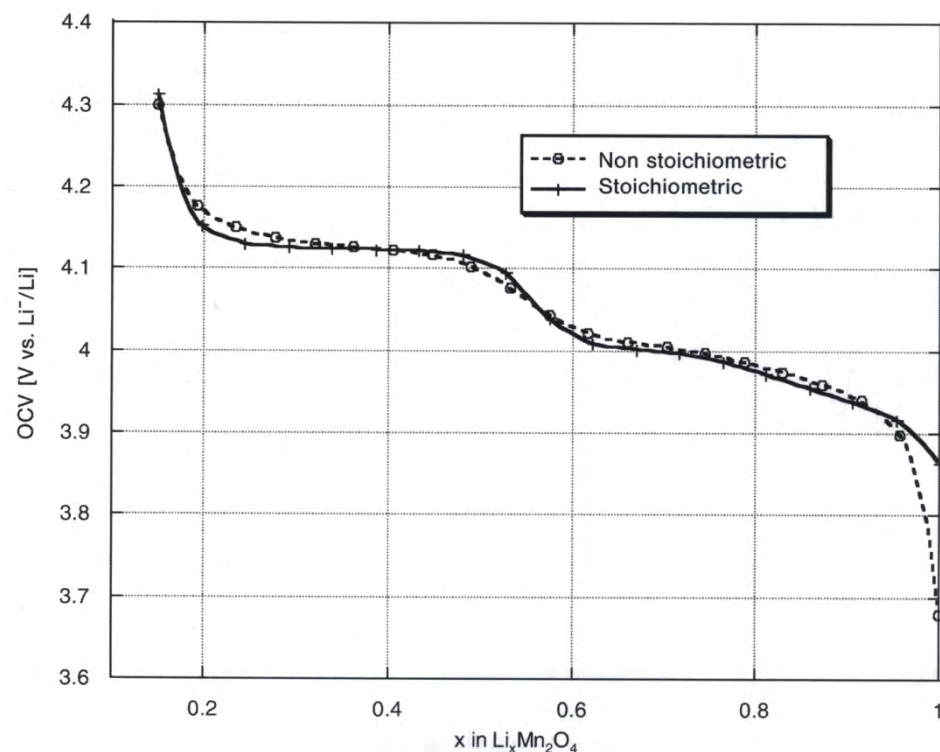


Li-Mn-O System

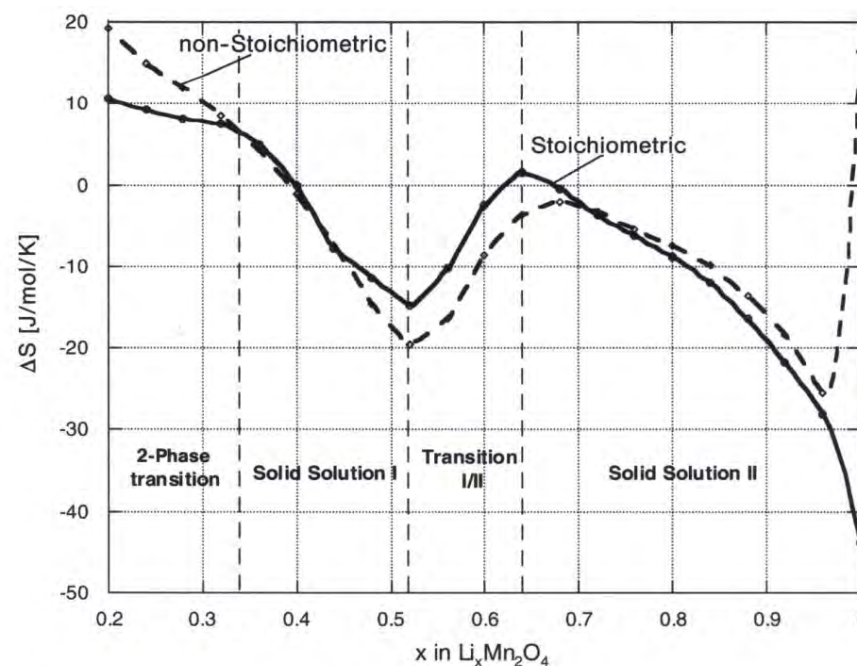
- Decomposition of LiMn_2O_4 in air
- Samples heat treated at 15 hours and quenched in liquid nitrogen



In-situ technique “entropymetry”



Open circuit voltage as a function of Li concentration in LiMn_2O_4

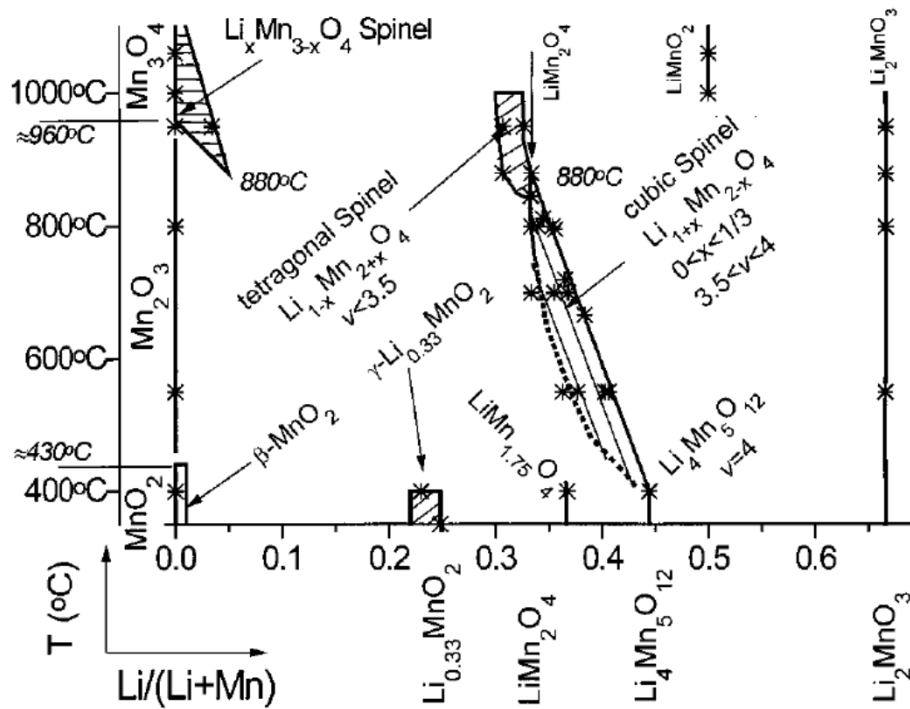


Entropy as a function of Li concentration in LiMn_2O_4

Note: Half cells measured

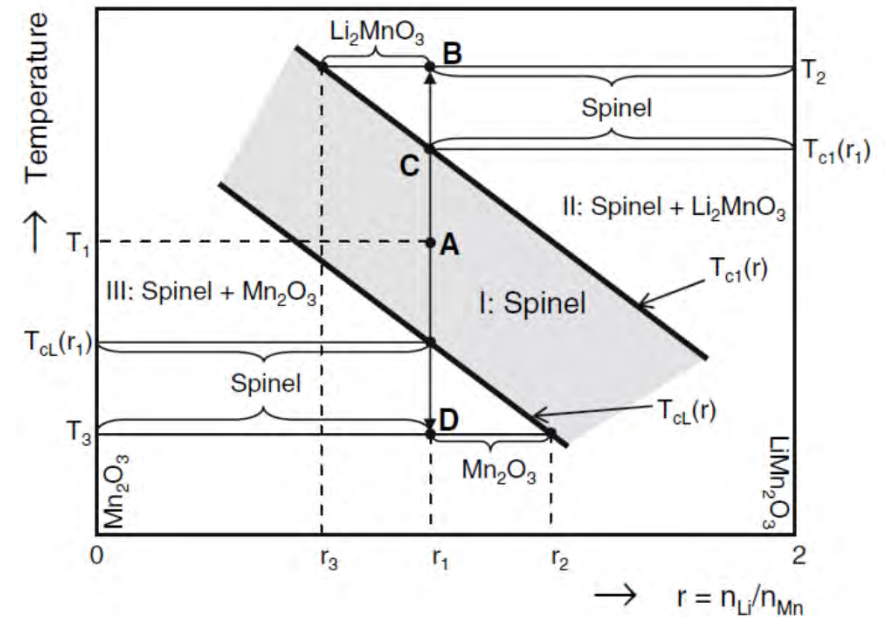
Yazami et al. in Lithium Ion Rechargeable Batteries, WILEY-VCH (2010)

2nd kind phase diagram in the Li-Mn-O system

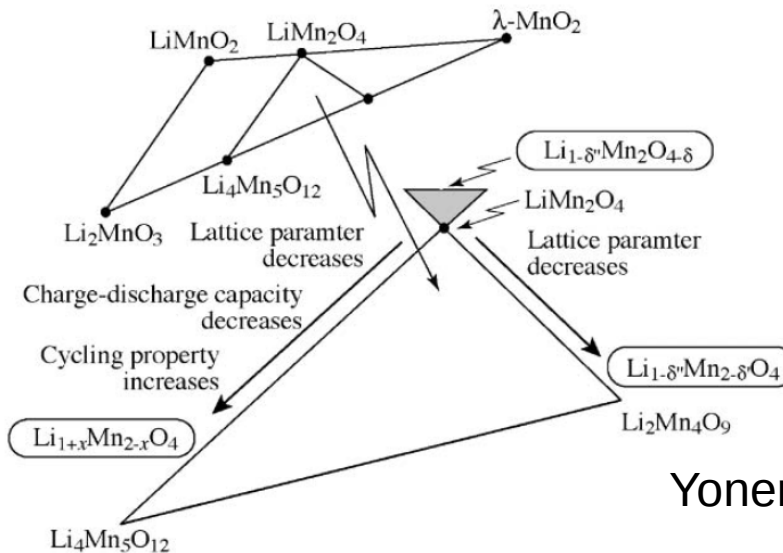


Paulsen and Dahn, 1999

Li-Mn-O System



Luo and Martin, 2007



Yonemura et al. 2004

**German Research Foundation, Priority Program 1473,
Materials with New Design for Improved Lithium Ion Batteries -
WeNDeLIB**

Battery Properties	Thermodynamics and Kinetics
Thermal runaway	Oxygen partial pressure, Gibbs free energies of reactions
Voltage, potential	Chemical potentials (of lithium)
Capacity, energy- and power density	Phase diagrams, Gibbs free energies
Life time	Stability of compounds in battery; Materials constitution
Power- and materials loss during first charge cycle	Formation of SEI; Relative thermochemical stabilities of materials for electrodes and electrolyte

Relationships Thermodynamics and Electrochemistry

Total change in enthalpy and entropy between two electrode compositions x_1 and x_2 :

$$\overline{\Delta S}\Big|_{x_1}^{x_2} = F \left(\int_{x_1}^{x_2} \frac{\partial E_0(x, T)}{\partial T} \Big|_x dx \right)$$

$$\overline{\Delta H}\Big|_{x_1}^{x_2} = F \int_{x_1}^{x_2} \left(-E_0(x, T) + T \frac{\partial E_0(x, T)}{\partial T} \Big|_x \right) dx$$

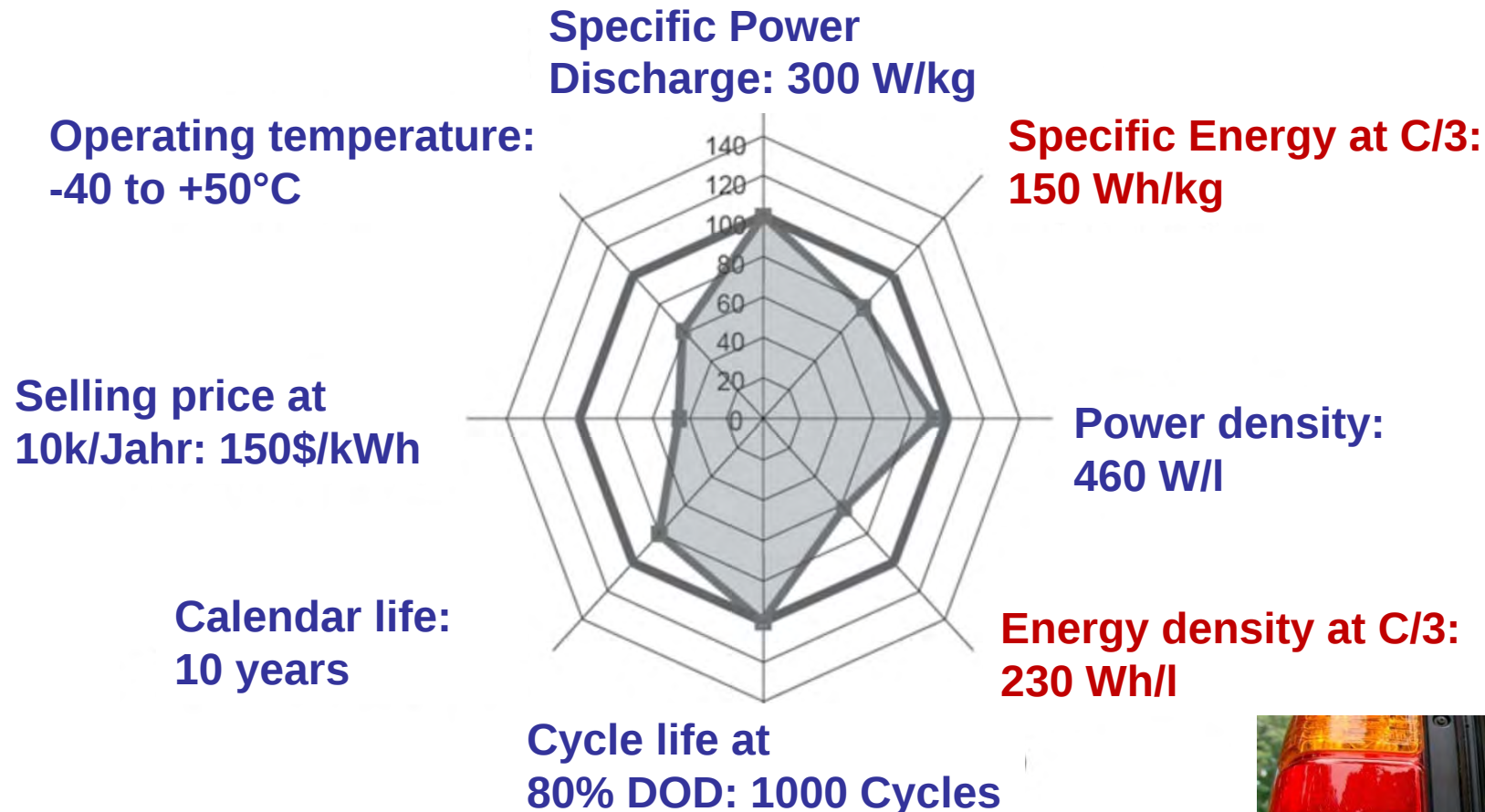
... and with normalization $y = \frac{x}{\Delta x_{\max}}, 0 < y < 1$

$$\overline{\Delta S}\Big|_0^1 = F \left(\int_0^1 \frac{\partial E_0(y, T)}{\partial T} \Big|_y dy \right)$$

$$\overline{\Delta H}\Big|_0^1 = F \int_0^1 \left(-E_0(y, T) + T \frac{\partial E_0(y, T)}{\partial T} \Big|_y \right) dy$$

Thermodynamic functions of active materials are needed

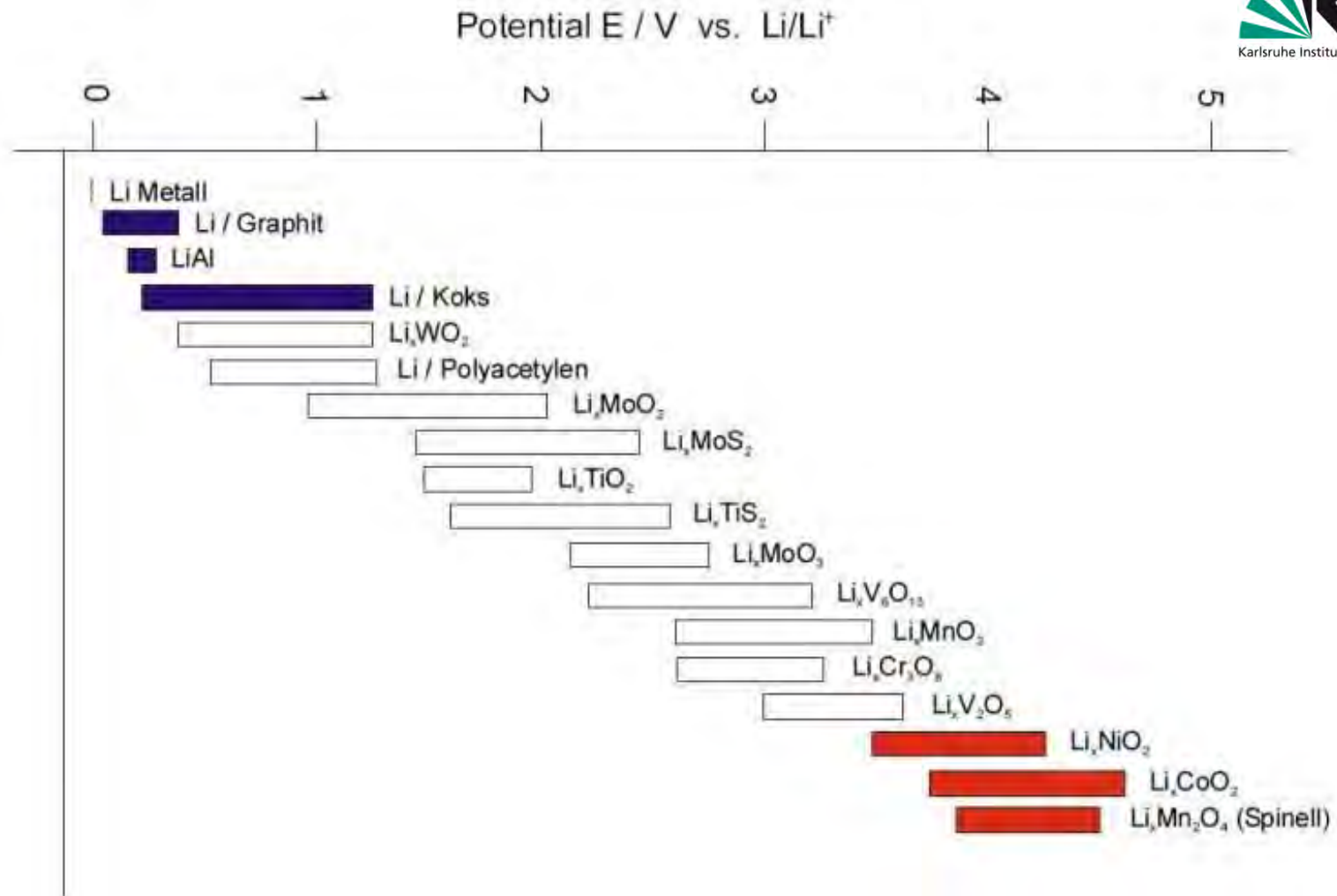
Battery technology spider chart (USABC) for electrical vehicles (EV)



Sources:

- (1) D. Howell, Energy Storage Research and Development, Annual Progress Report 2006 (Washington, D.C.: Office of FreedomCAR and Vehicle Technologies, U.S. Department of Energy, 2007)
- (2) FreedomCAR and Fuel Partnership and **United States Advanced Battery Consortium (USABC)**, Electrochemical Energy Storage Technical Team Technology Development Roadmap (Southfield, MI: USCAR, 2006)





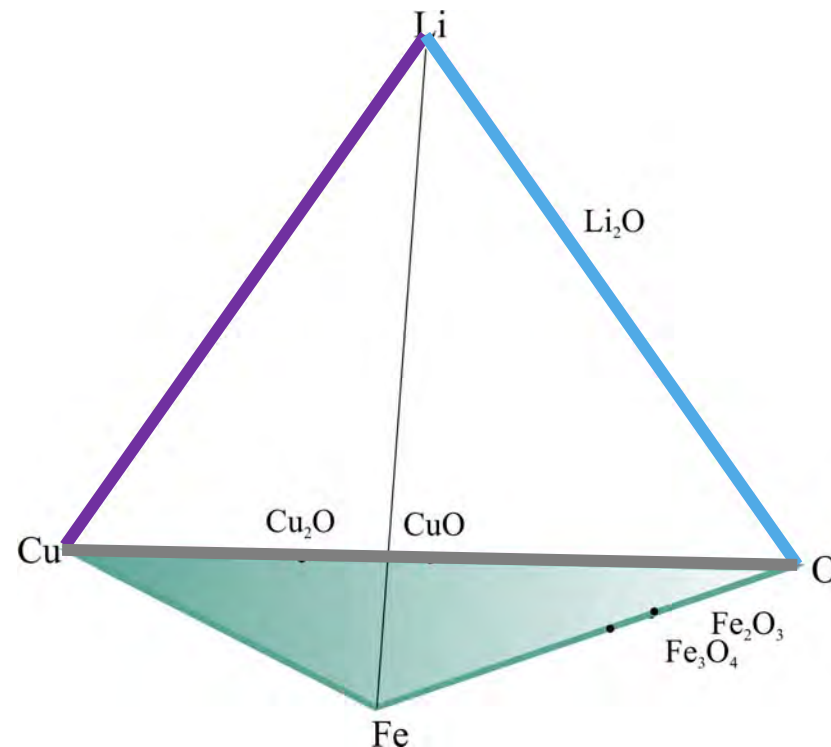
Li-Cu-Fe-O System

- Thermodynamic calculations based on the CALPHAD method
 - predict battery performance
 - equilibrium voltages (OCV)
 - plateau capacities
- Database development for the **Li-Cu-Fe-O** System
 - The **Cu-Fe-O** ternary system assessed by Khvan et al.
 - First calculated phase diagrams in the **Li-Cu-O** system addressed in present work

N. Saunders, I. Ansara (Ed), Cost 507, Report, 1994, 168–169

B. Hallstedt, L.J. Gauckler CALPHAD, 2003, 27:177-191

K. Chang, B. Hallstedt, CALPHAD, 2011, 35:160-164



Isothermal calorimetric measurements on a 16 mAh Lithium ion coin cell

Discharge parameters:

- Method: constant current (CC)
- $U_{\min} = 2.75 \text{ V}$
- $I = 16 \text{ mA} \rightarrow 1\text{C-rate}$

Charge parameters:

- Method: constant current,
constant voltage

(CCCV)

- $U_{\max} = 4.25 \text{ V}$
- $I = 16 \text{ mA} \rightarrow 1\text{C-rate}$
- $I_{\min} = 1.6 \text{ mA}$



Isothermal Battery Calorimeter (IBC)

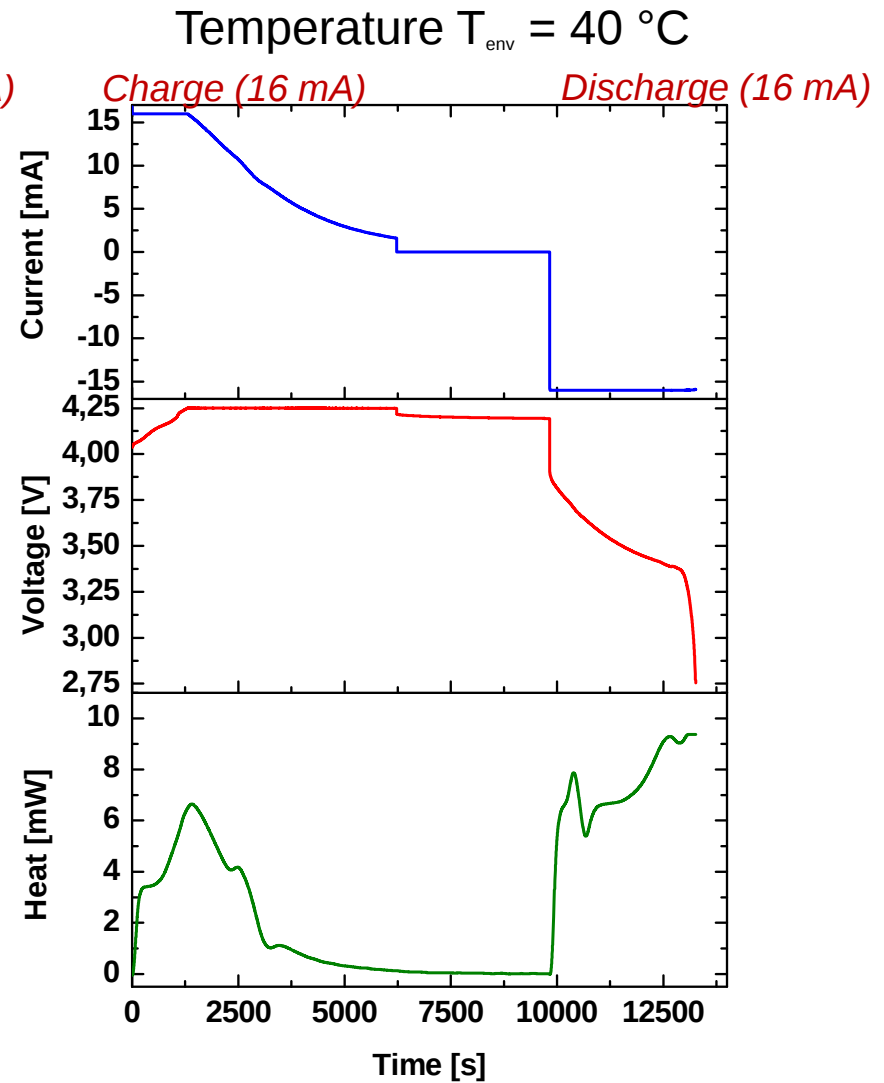
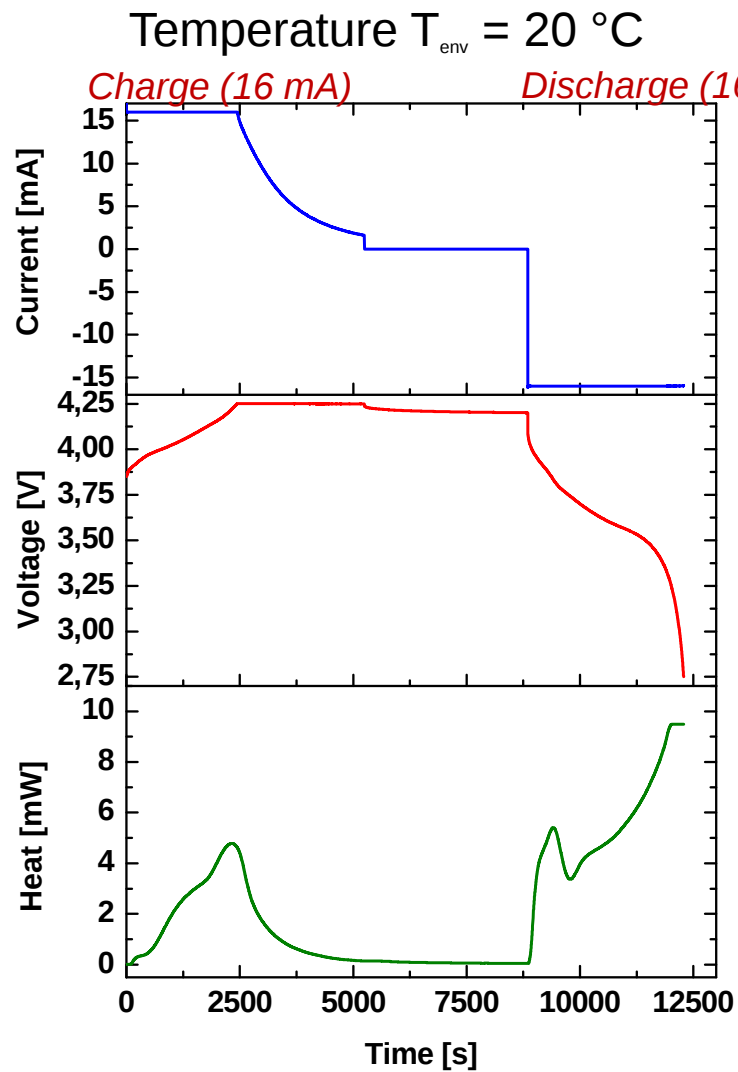
Cell type: coin cell LIR 2016,

Conrad energy (commercial)

Capacity: $20 \pm 5 \text{ mAh}$; Working voltage: 3.6 V



Isothermal calorimetric measurements on a 16 mAh Lithium ion coin cell

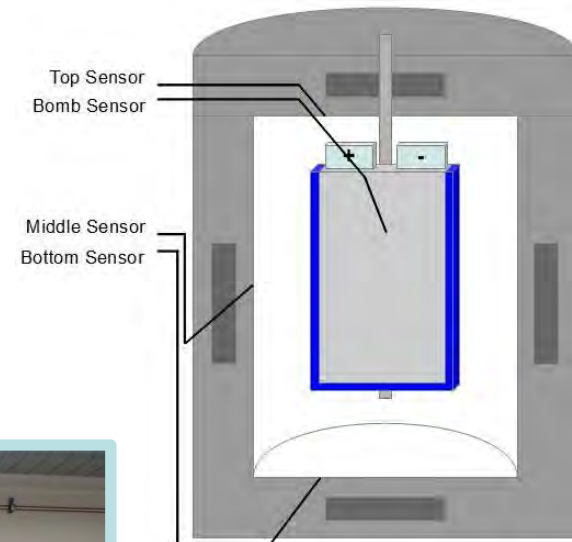


Accelerating Rate Calorimeter (ARC)

ARC provides an adiabatic environment in which a sample may be studied under conditions of negligible heat loss

heat of reaction: $\Delta H = \Delta T_{ad} c_p$

total heat generated: $Q_{\Sigma} = m\Delta H$



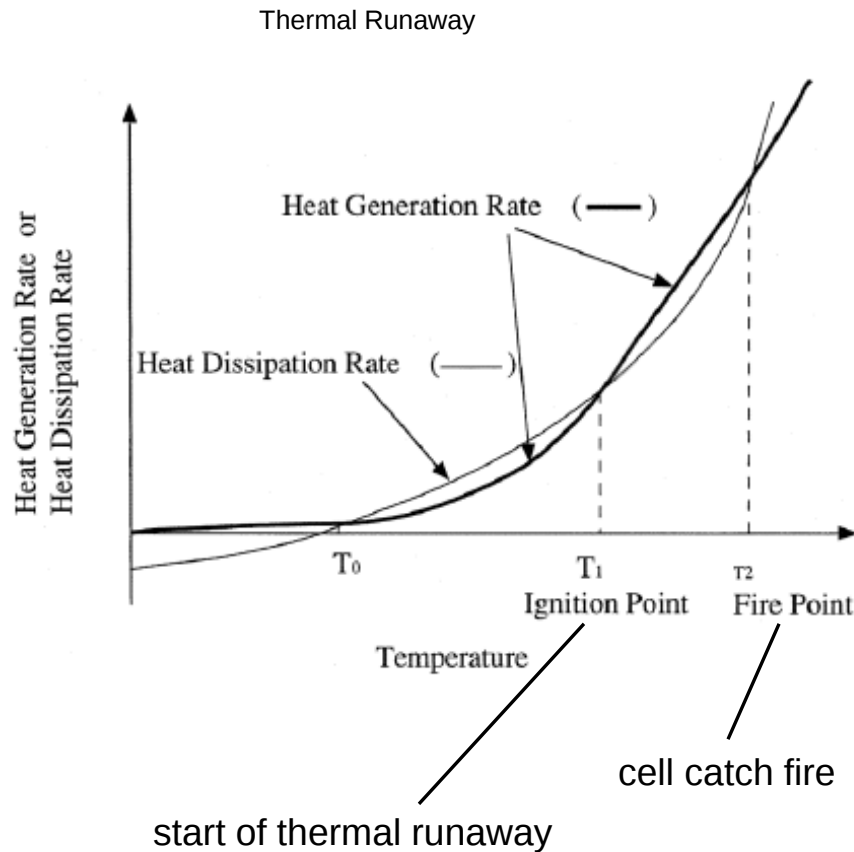
EVARC: Ø: 25cm
h: 50cm

ESARC: Ø: 10cm
h: 10cm



$T = 20 \dots 500^{\circ}\text{C}$
 $\Delta T_{det} = 0,005\text{K}$

Thermodynamics of electrochemical reactions



electrochemical reaction

$$\Delta G = -nFE$$

Gibbs-Helmholtz equation

$$\Delta S = -\left(\frac{\delta \Delta G}{\delta T}\right)$$

entropic change of electrochem. reaction

$$\Delta S = nF\left(\frac{\delta E}{\delta T}\right)$$

reversible heat

$$Q_{rev} = T\Delta S = nFT\left(\frac{\delta E}{\delta T}\right)$$

S. Tobishima, J. Yamaki, J. Power Source 81-82, p. 882–886 (1999)

A.K. Shukla, T.P. Kumar, Current Sci. 94, p. 314-331 (2008)

Enthalpy of Drop Solution of $\text{Li}_{1+x}\text{Mn}_{2-x}\text{O}_{4-\delta}$



Al_2O_3 plug

SiO_2 glass dropping tube for sample introduction

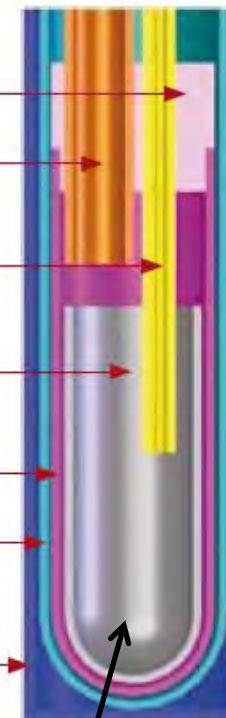
Platinum tube for bubbling gas introduction

Platinum crucible where solvent is introduced

SiO_2 glass crucible

SiO_2 glass liner

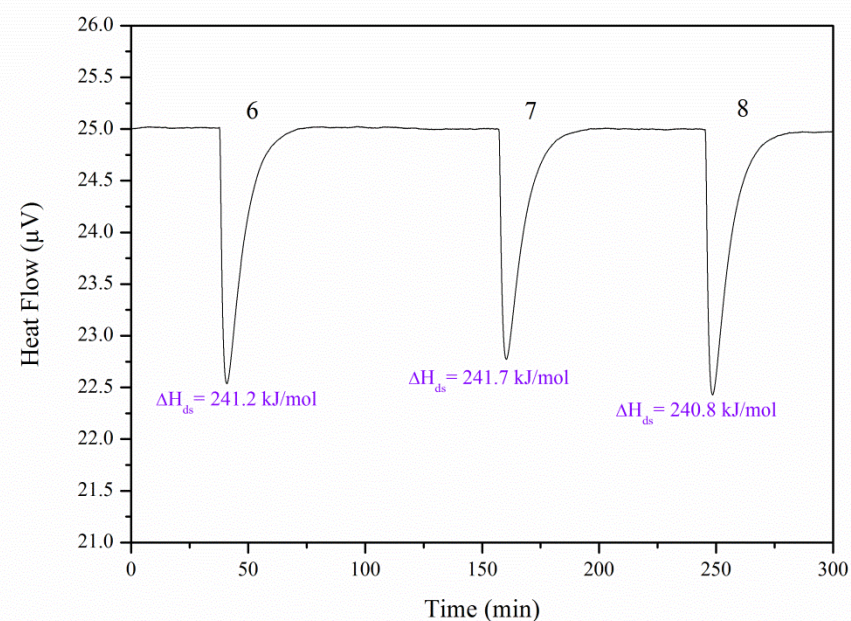
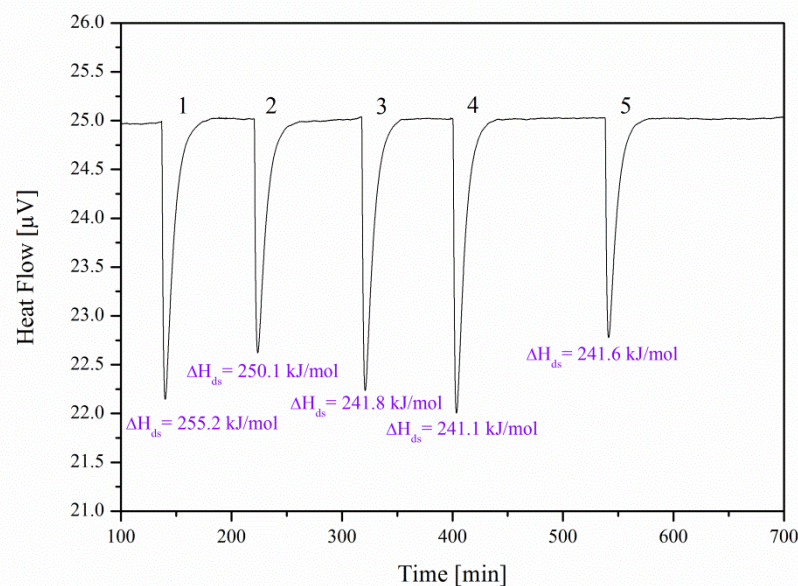
Inconel protection tube



Sodium Molybdate, 700°C

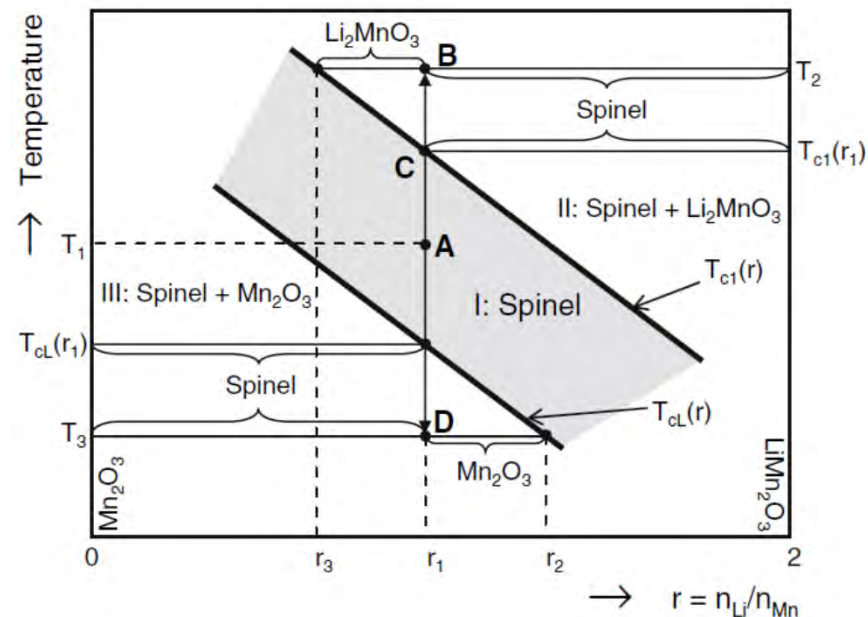
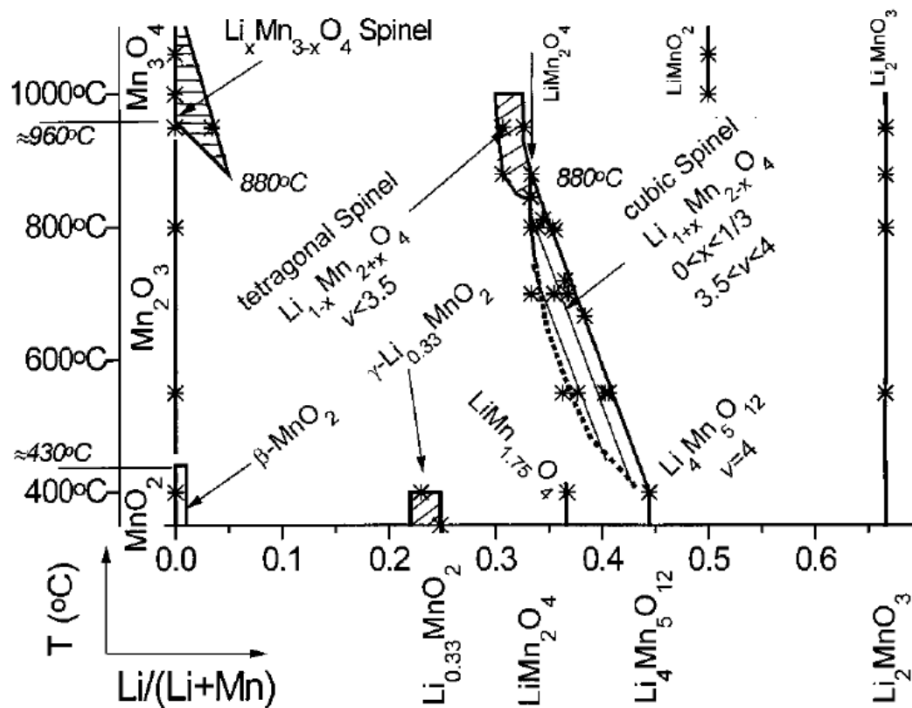
AlexSys 1000, SETARAM
High Temperature Calvet Calorimeter

Enthalpy of Drop Solution of $\text{Li}_{1+x}\text{Mn}_{2-x}\text{O}_{4-\delta}$



Sample Number	DROP 1	DROP 2	DROP 3	DROP 4	DROP 5	DROP 6	DROP 7	DROP 8
Date	08. Mai	08. Mai	08. Mai	08. Mai	08. Mai	09. Mai	09. Mai	09. Mai
Mass pellet (mg)	6,00	5,14	6,10	6,62	4,85	5,35	4,83	5,59
T(room) (°C)	23,90	24,10	24,20	24,10	24,20	24,50	24,30	24,20
T(cal.) (°C)	700,40	700,40	700,40	700,40	700,40	700,40	700,40	700,40
Formula weight (g/mol)	180,815	180,815	180,815	180,815	180,815	180,815	180,815	180,815
Moles of LiMn_2O_4 (mol)	0,0000332	0,0000284	0,0000337	0,0000366	0,0000268	0,0000296	0,0000267	0,0000309
Peak Area [μV.s]	1832,4170	1538,5640	1765,6030	1910,2030	1402,3320	1544,6110	1397,2290	1611,2630
Calibration factor from Al_2O_3 calibration[J/μV.s]	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077	0,00462077
Measured Heat Effect (kJ/mol)	255,1652	250,0926	241,8308	241,0849	241,5781	241,2203	241,6957	240,8258
Accepted Measurement	0	0	1	1	1	1	1	1

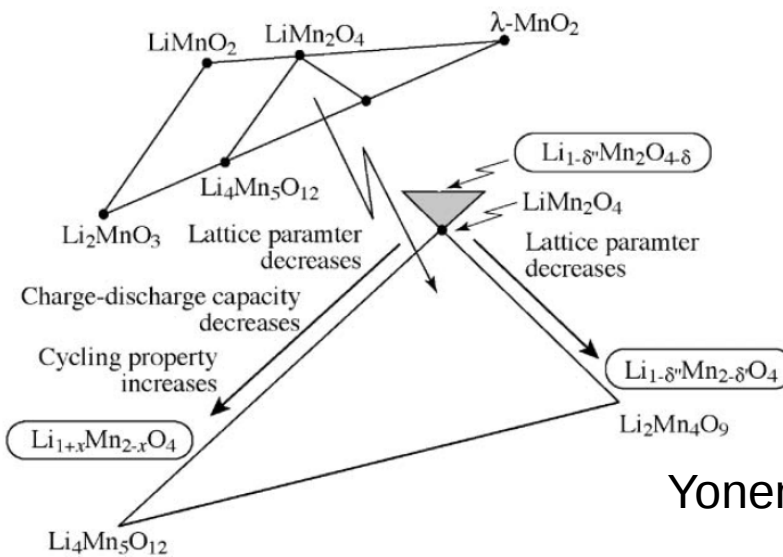
2nd kind phase diagram in the Li-Mn-O system



Luo and Martin, 2007

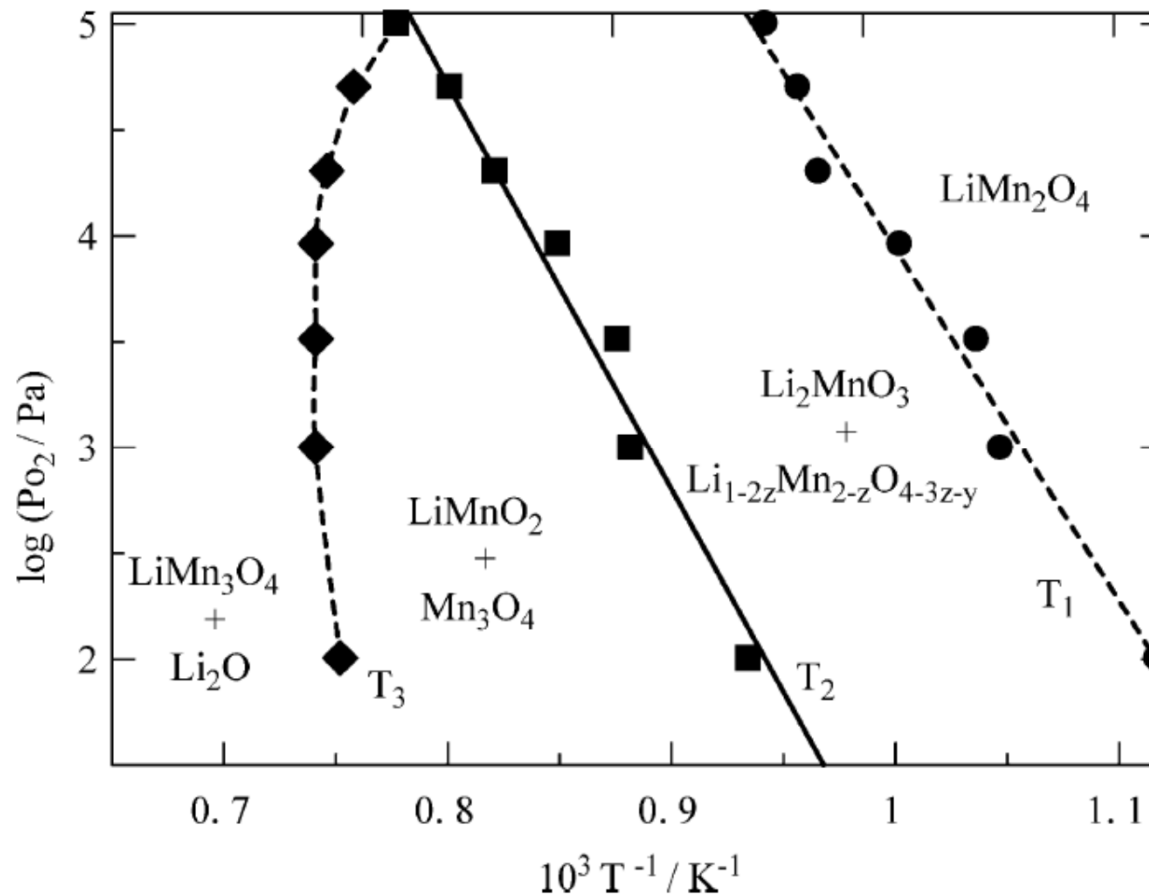
Paulsen and Dahn, 1999

Li-Mn-O System



Yonemura et al. 2004

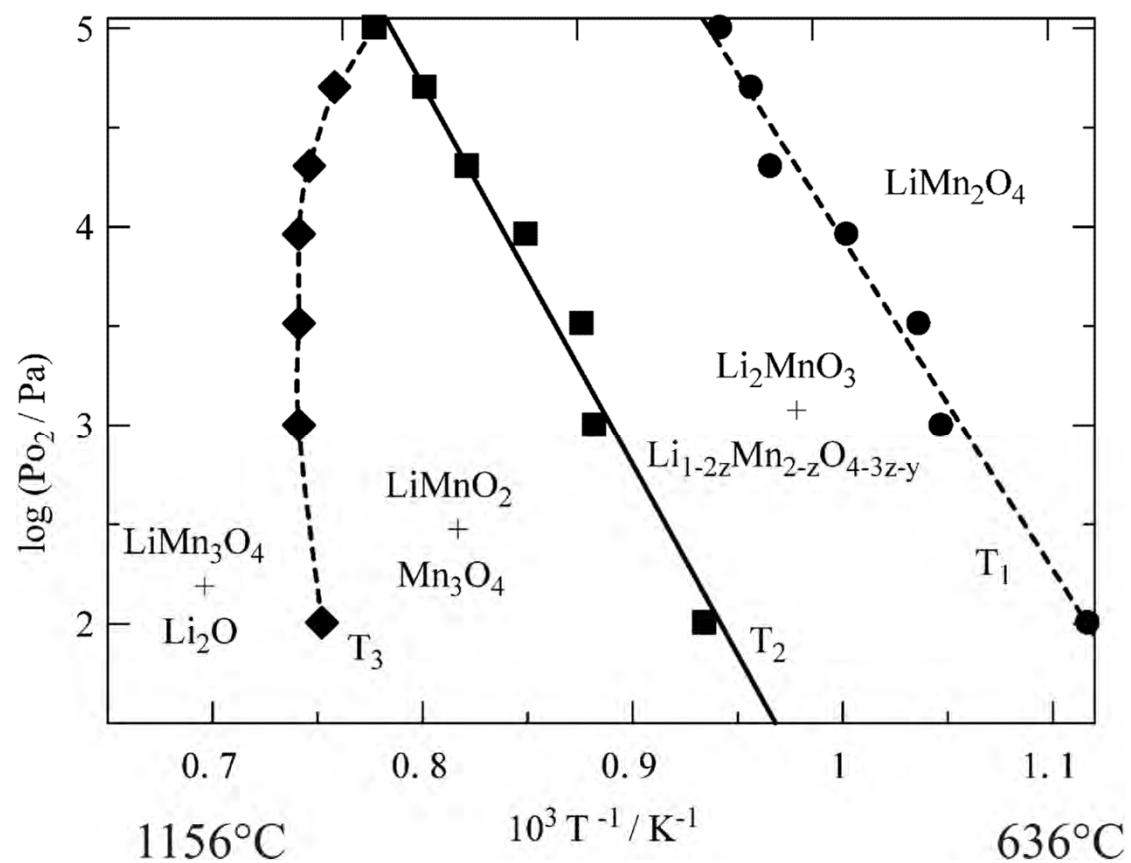
Li-Mn-O System



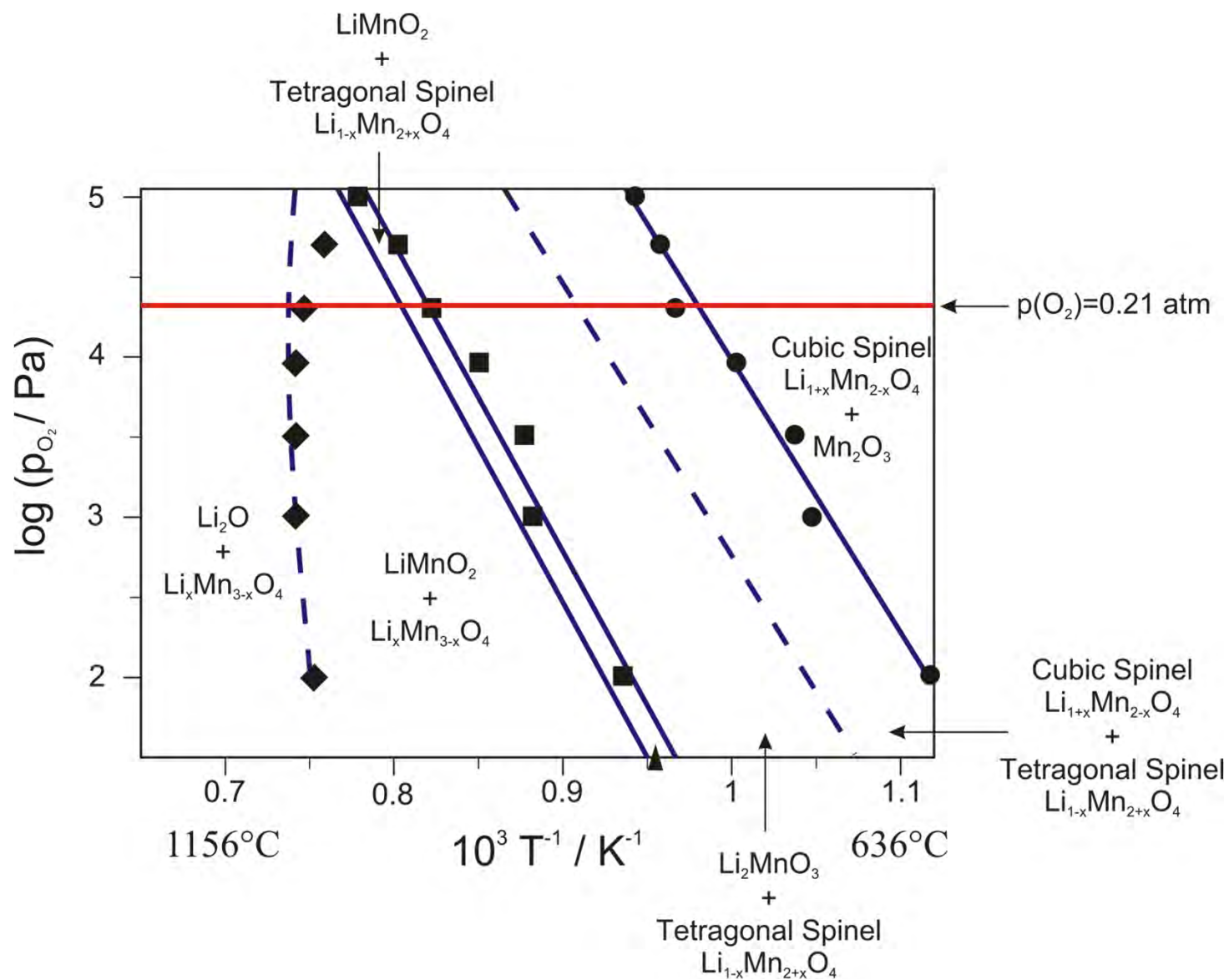
Chemical potential diagram in the Li-Mn-O system (Tsuji et al. 2005).

**What to do next: (1) Evaluation; (2) Solution phase modeling;
(3) Thermodynamic optimization**

Li-Mn-O System

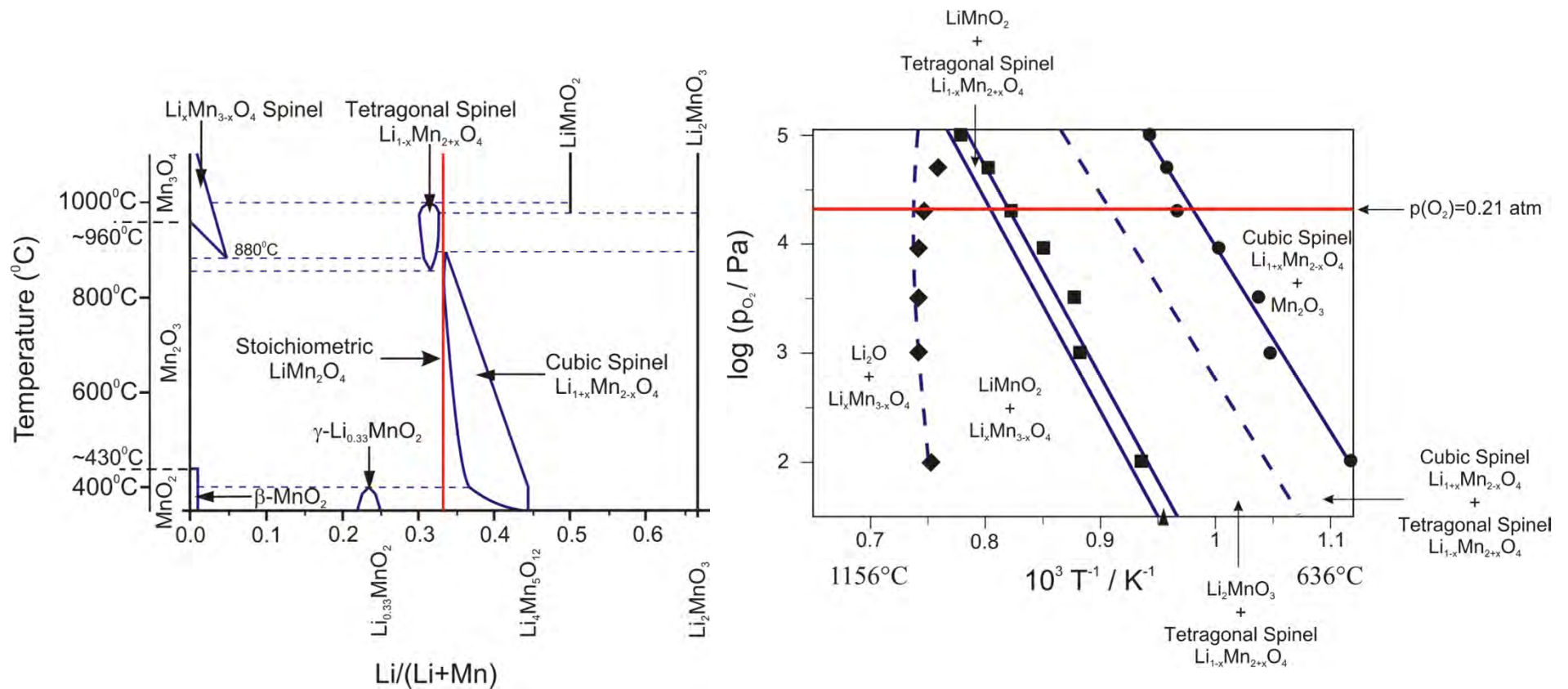


Li-Mn-O System



Li-Mn-O System

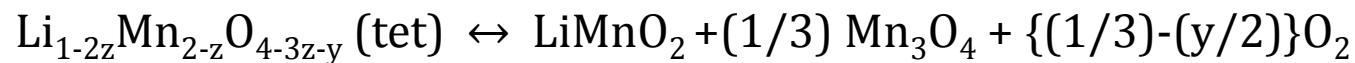
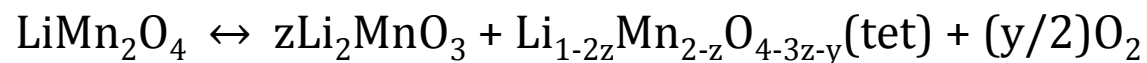
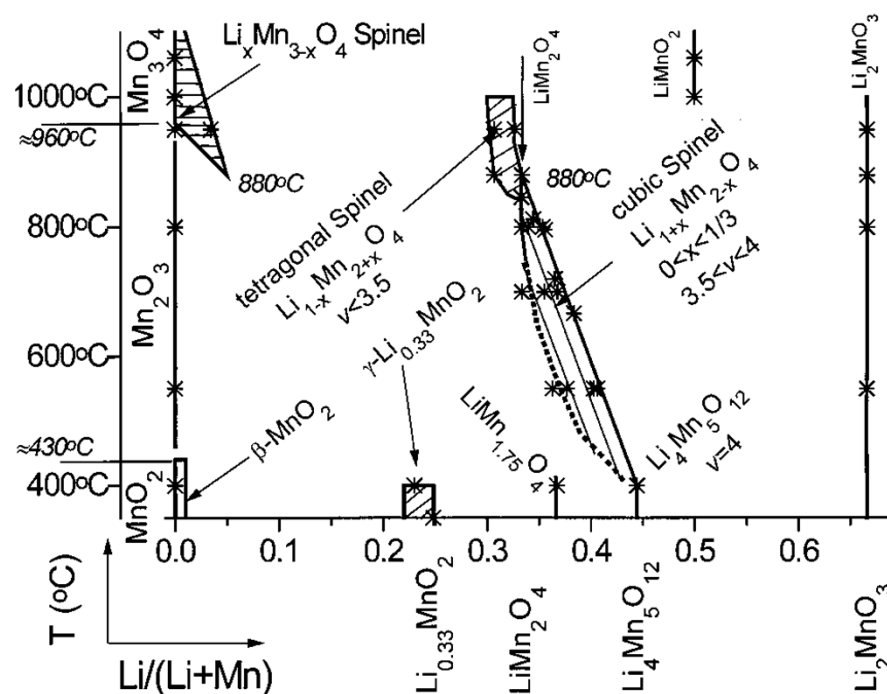
- LiMn_2O_4 composition is a vertical line in the temperature-composition ratio diagram
- $p(\text{O}_2)=0.21$ atm is a horizontal line in the potential diagram



Li-Mn-O System

$p(\text{O}_2)=0.21 \text{ atm}$

Li/Mn ratio for LiMn_2O_4

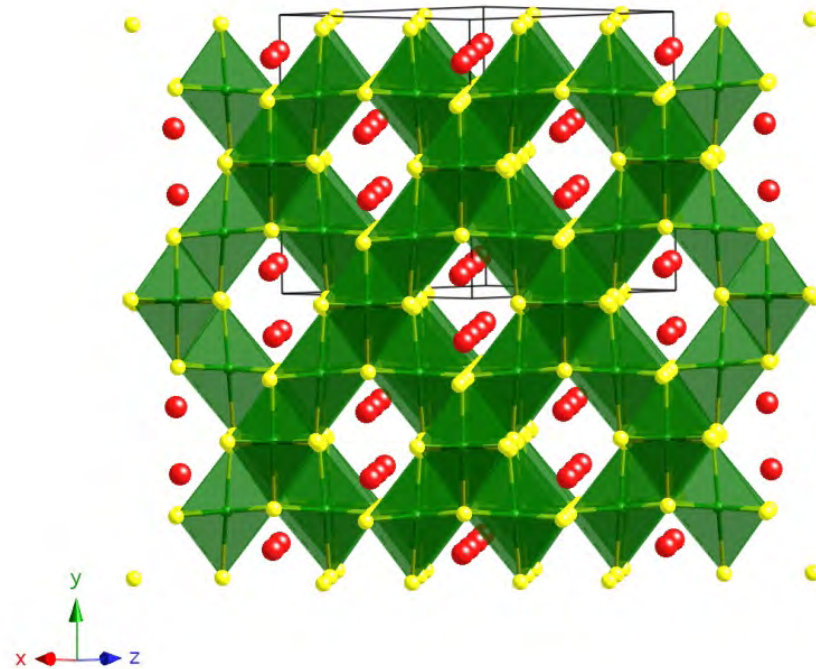


[1999 Pau] *Chem. Mater.*, 11 (1999), 3065-3079.

[2005 Tsu] *J. Phys. Chem., Solids*. 66 (2005), 283-287.

Commercial cathode material LiMn_2O_4

Spinel structure



LiMn_2O_4 : $\approx 100 \text{ mAh/g}$

Gravimetric energy density (capacity)

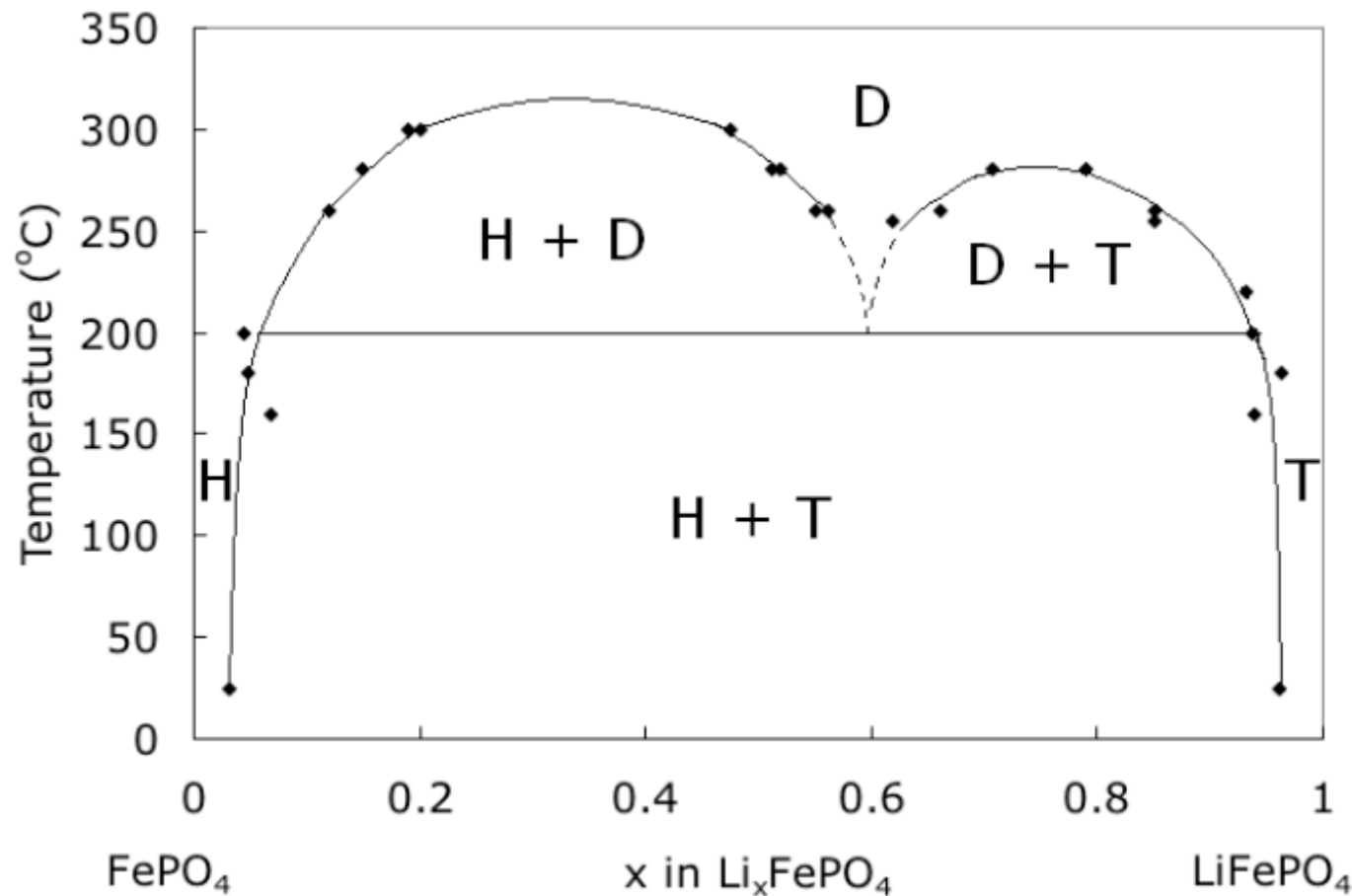


Figure 6. Phase diagram of LiFePO_4 (T, for triphylite) and FePO_4 (H, for heterosite) phases showing their merging to a solid solution (D, for disordered) in a eutectoid system. Data points at 25°C are based on published work by Yamada [10]. The eutectoid point is around the composition $x = 0.6$ and temperature 200°C . Above 200°C , mixtures of heterosite or triphylite and the disordered phase were seen up to around 300°C . Above 300°C , the disordered phase dominates.

Dodd et al. (2006)

Li-Fe-P-O System

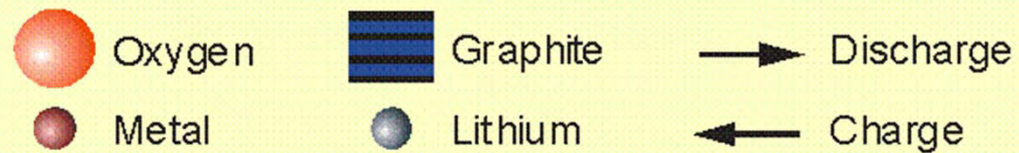
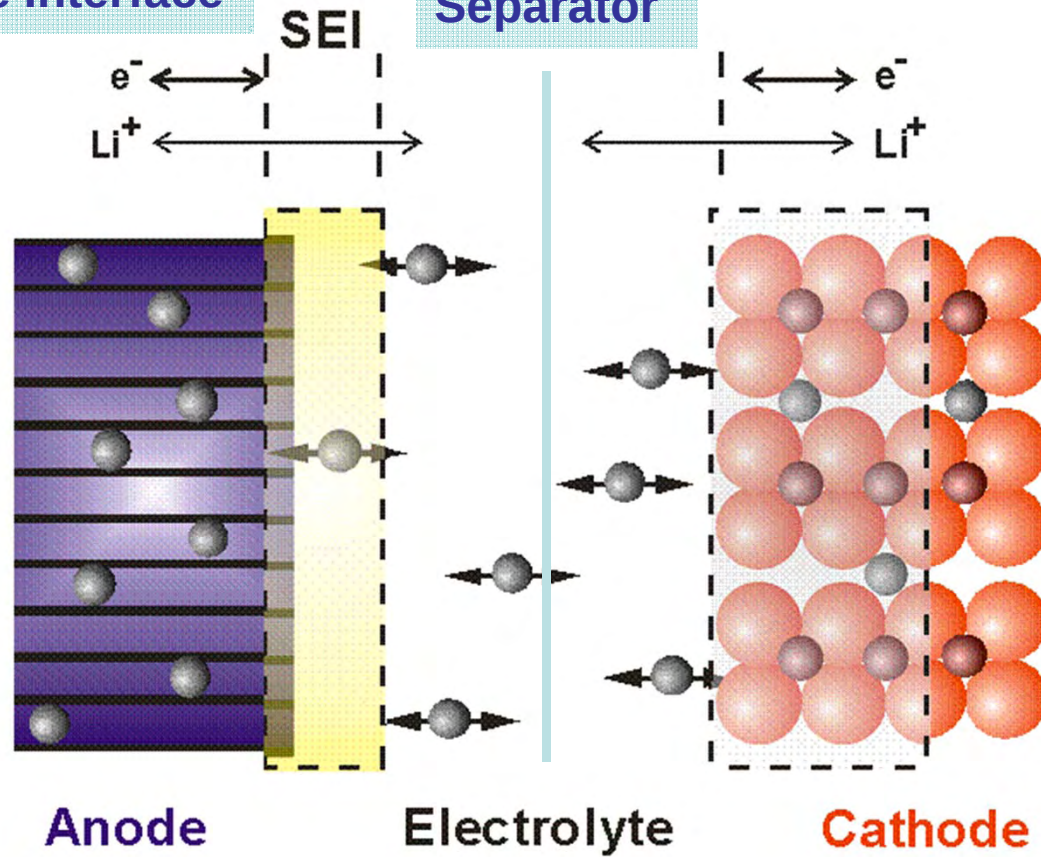
Lithium Ion Batteries – Operation

Solid Electrolyte Interface

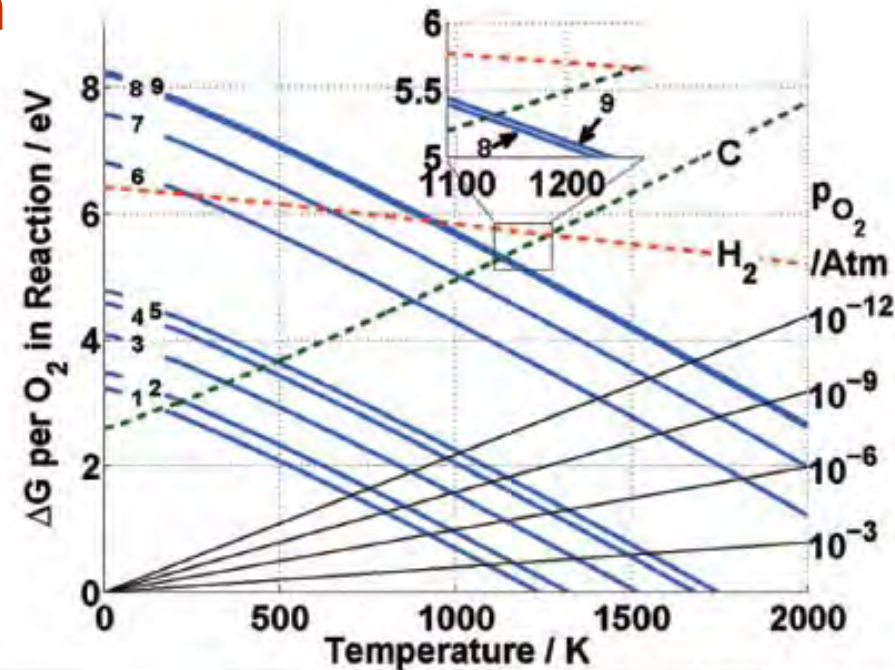
Separator

Graphite

LiCoO_2



Li-Fe-P-O System

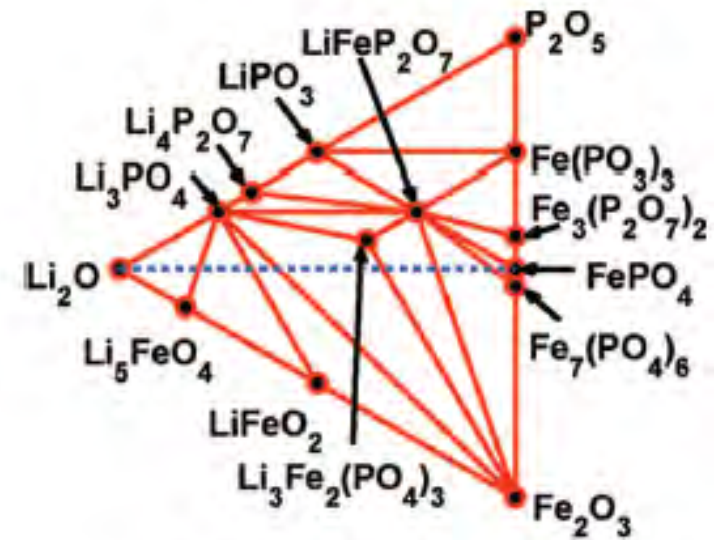
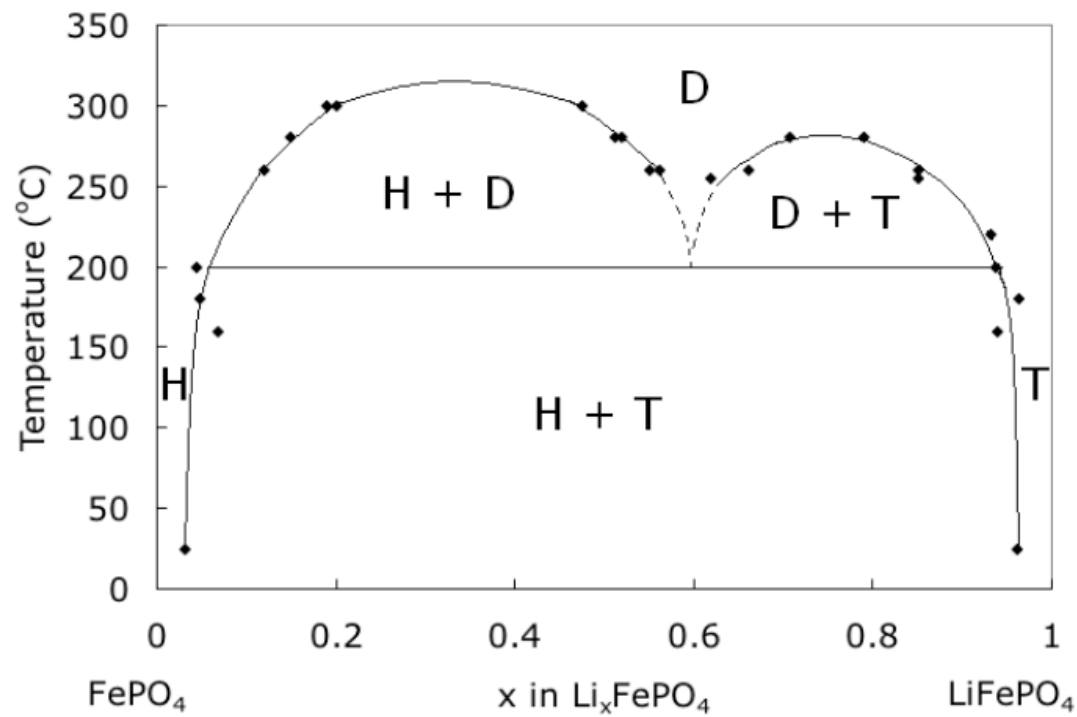


Reaction	Line Label
$3 \text{Li}_3\text{Fe}_2(\text{PO}_4)_3 = 4 \text{LiFePO}_4 + 2 \text{LiFeP}_2\text{O}_7 + \text{Li}_3\text{PO}_4 + \text{O}_2$	1
$\frac{3}{2} \text{Fe}_7(\text{PO}_4)_6 = \text{Fe}_3(\text{P}_2\text{O}_7)_2 + \frac{5}{2} \text{Fe}_3(\text{PO}_4)_2 + \text{O}_2$	2
$2 \text{Fe}_3(\text{P}_2\text{O}_7)_2 = 2 \text{Fe}_2\text{P}_2\text{O}_7 + \text{Fe}_2\text{P}_4\text{O}_{12} + \text{O}_2$	3
$4 \text{LiFeP}_2\text{O}_7 = 4 \text{LiPO}_3 + 2 \text{Fe}_2\text{P}_2\text{O}_7 + \text{O}_2$	4
$6 \text{Fe}_2\text{O}_3 = 4 \text{Fe}_3\text{O}_4 + \text{O}_2$	5
$2 \text{Fe}_3\text{O}_4 = 6 \text{FeO} + \text{O}_2$	6
$\frac{6}{5} \text{Fe}_2\text{P}_2\text{O}_7 = \frac{4}{5} \text{Fe}_3(\text{PO}_4)_2 + \frac{4}{5} \text{P} + \text{O}_2$	7
$2 \text{FeO} = 2 \text{Fe} + \text{O}_2$	8
$\frac{1}{4} \text{Fe}_3(\text{PO}_4)_2 = \frac{1}{28} \text{FeP}_4 + \frac{5}{14} \text{Fe}_2\text{P} + \text{O}_2$	
$\frac{3}{4} \text{LiFePO}_4 = \frac{1}{4} \text{Li}_3\text{PO}_4 + \frac{5}{14} \text{Fe}_2\text{P} + \frac{1}{28} \text{FeP}_4 + \text{O}_2$	9
$2\text{CO} = 2\text{C} + \text{O}_2$	C
$2\text{H}_2\text{O} = 2\text{H}_2 + \text{O}_2$	H₂

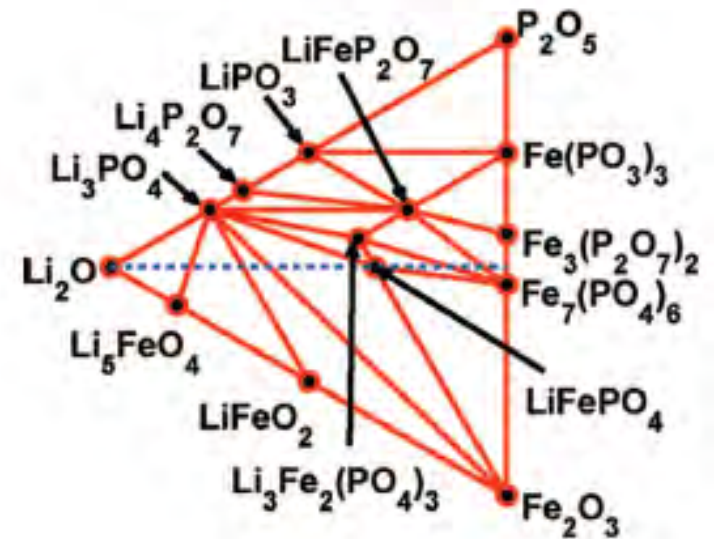
Figure 6. Modified Ellingham diagram for reduction reactions in the Li-Fe-P-O₂ system.

Ong et al. (2008)

Li-Fe-P-O System



(a) $\mu_{\text{O}_2} = -10.50 \text{ eV}$, $\text{Fe}_7(\text{PO}_4)_6$ appears



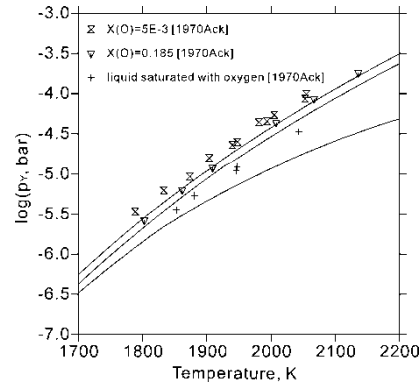
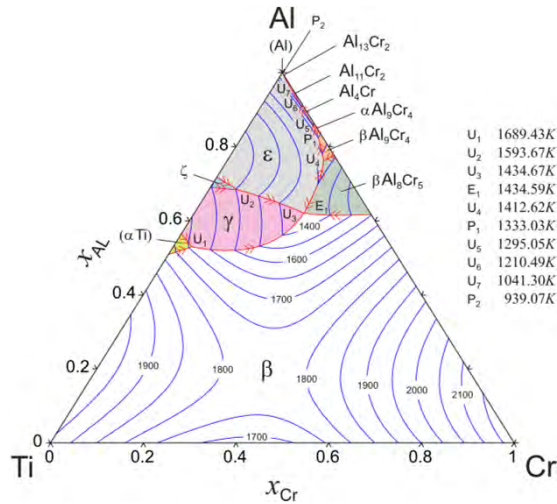
(b) $\mu_{\text{O}_2} = -11.52 \text{ eV}$, LiFePO_4 appears

Figure 2. Phase diagrams at less reducing environments.

CALPHAD

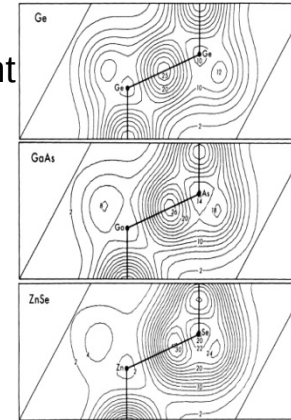
Modelling and Simulation

Ab-initio

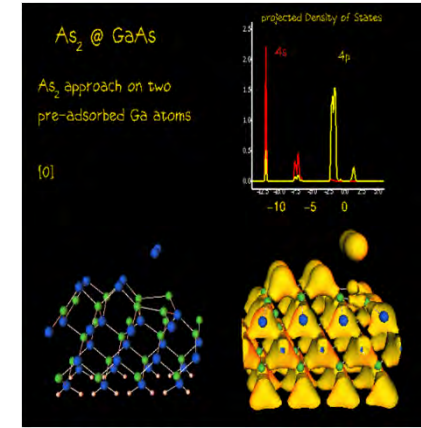


covalent

ionic



Kratzer et al.,
<http://www.fhi-berlin.mpg.de>



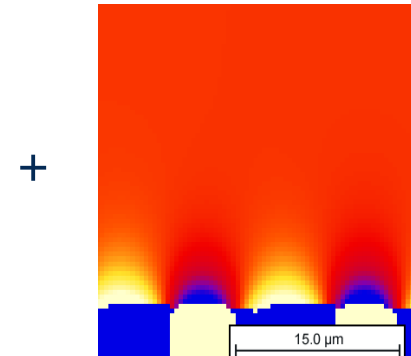
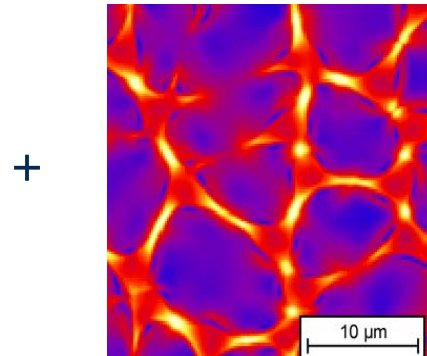
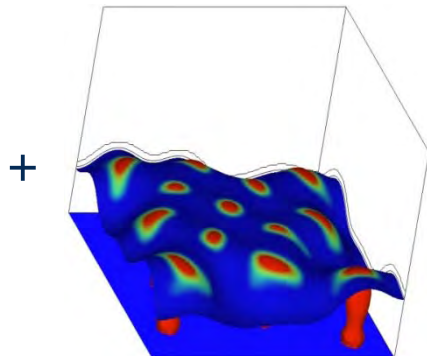
Chelikowsky et al.,
Phys. Rev. B 14, 556 (1976)

Phase Field

interfaces
(length scale)

mechanical equilibrium
(energy scale)

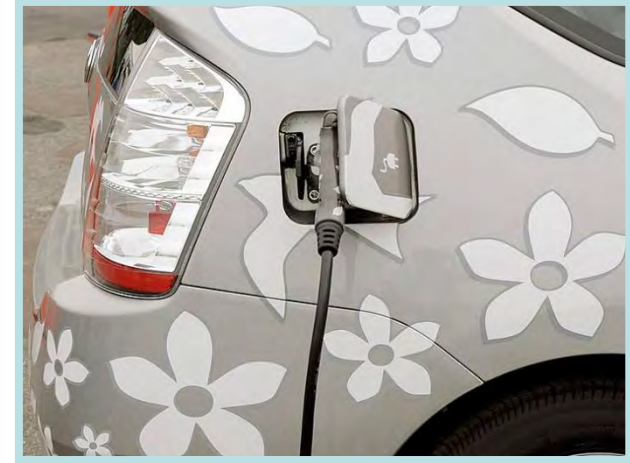
transport / diffusion
(time scale)



Accidents with lithium ion batteries



Rechargeable battery
of a laptop
– overheating or
internal short circuit



Fire 3 days after
crashtest with EV
– mechanical impact



stationary energy storage
– overcharging