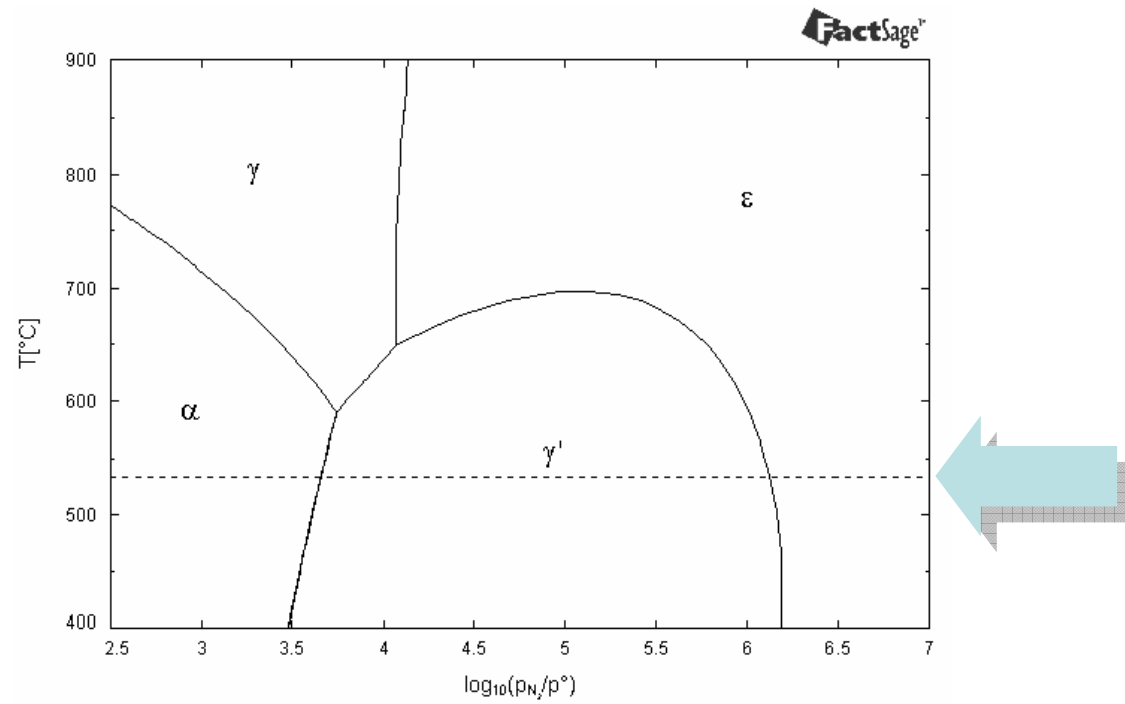


"Gas nitriding of a Fe–C–Mn Alloy – a thermodynamic analysis"

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Fe-N Lehrer diagram
Nitriding of Fe

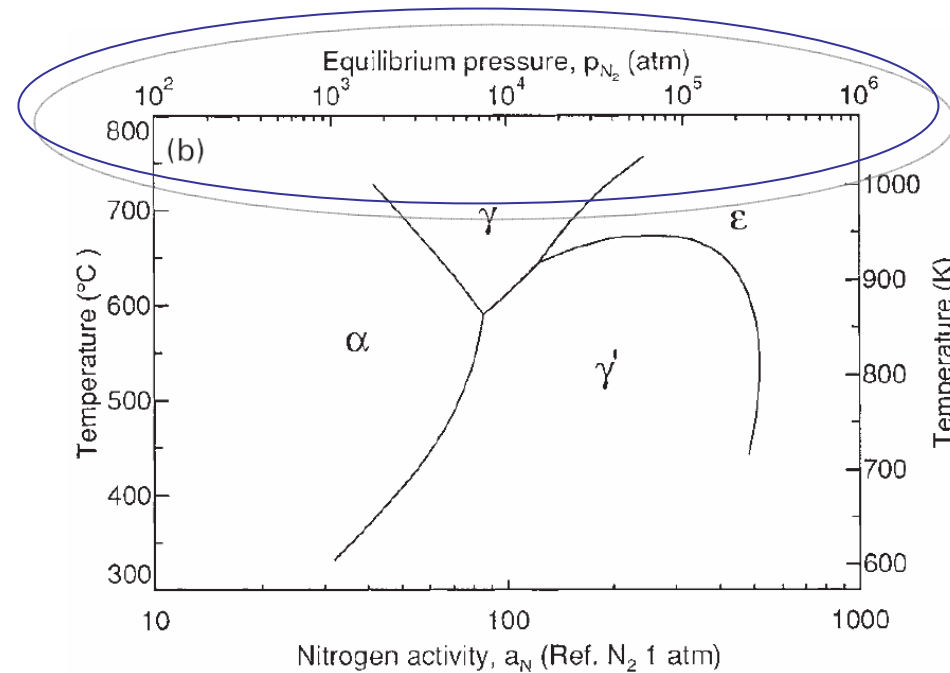
$$G_{N_2} = G_{N_2}^{\circ} + RT \ln P_{N_2}$$

$$\mu_N = \mu_N^{\circ} + RT \ln a_N$$

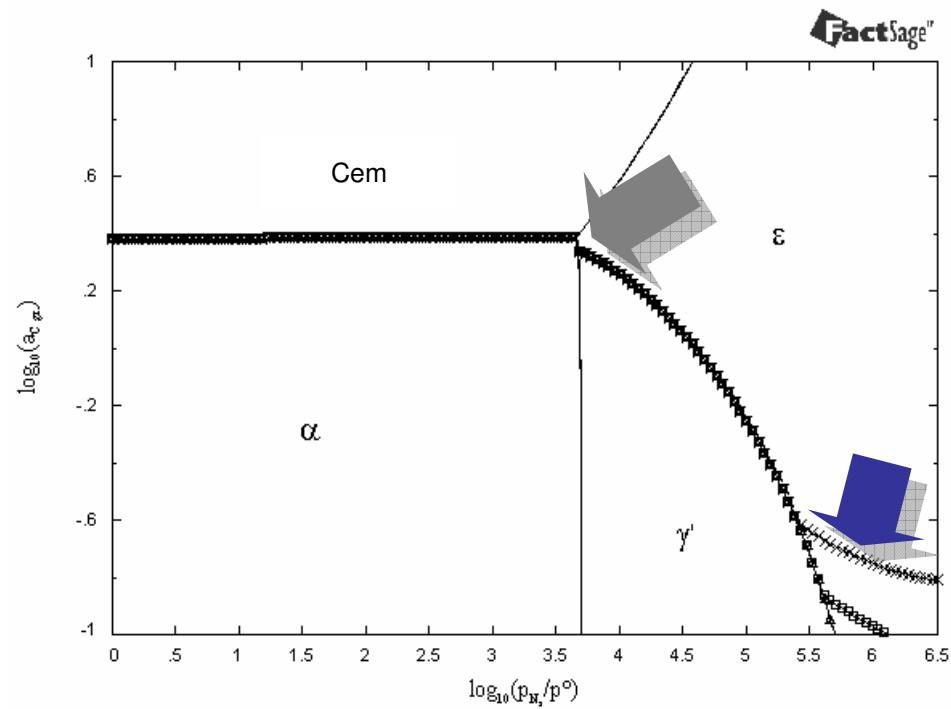
$$\mu_N = \frac{1}{2} \mu_{N_2}^{\circ} + RT \ln a_N$$

$$\frac{1}{2} G_{N_2} = \frac{1}{2} G_{N_2}^{\circ} + RT \ln(P_{N_2}^{1/2})$$

$$a_N = P_{N_2}^{1/2}$$



Mittlemeijer and Slycke. Potentials and activities in gaseous nitriding and carburising. Surface Engineering 1996 Vol. 12 No. 2



Fe-N-C Isothermal section of **Lehrer** diagram; T = 560 [°C]
Nitriding of Fe-C alloy

(x = 1%C, \square = 0.8%C, Δ = 0.4%C and \circ = 0.2%C)

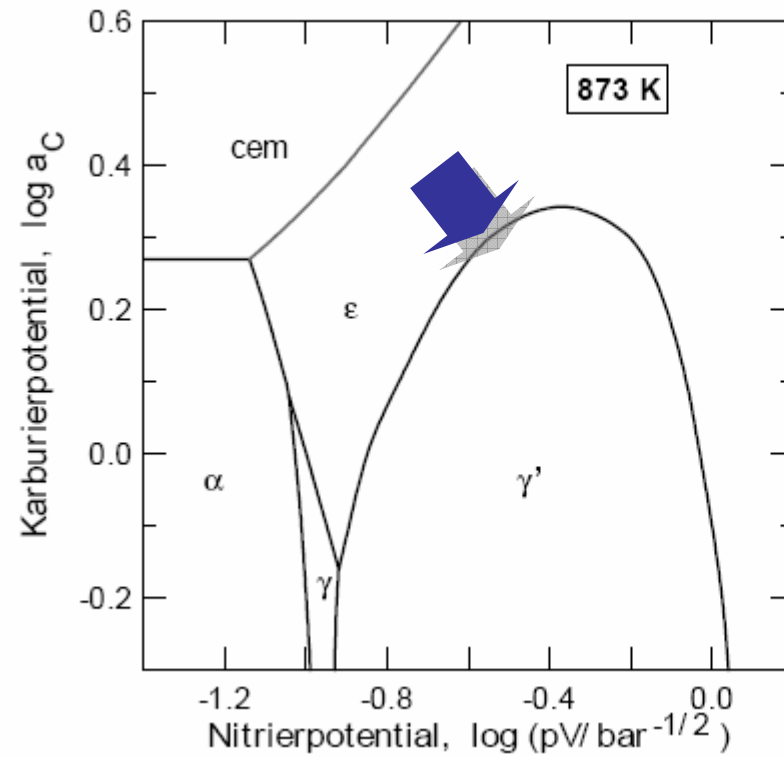
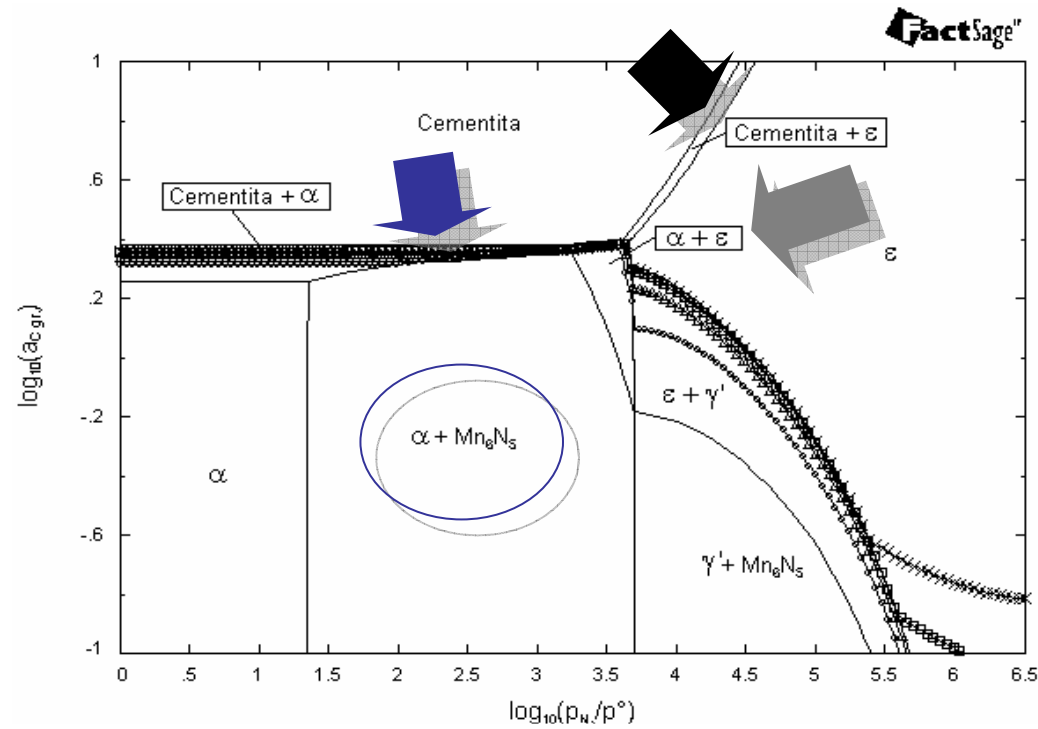


Abb. 16:
Stabilitätsbereiche der Phasen
bei 600 °C in Abhängigkeit von
Nitrier- und Carburierpotentialen

Dr.-Ing. habil. Joachim Kunze
Physikalisch-chemische Grundlagen der
Wärmebehandlung und Randschichttechnik
Lecture Notes

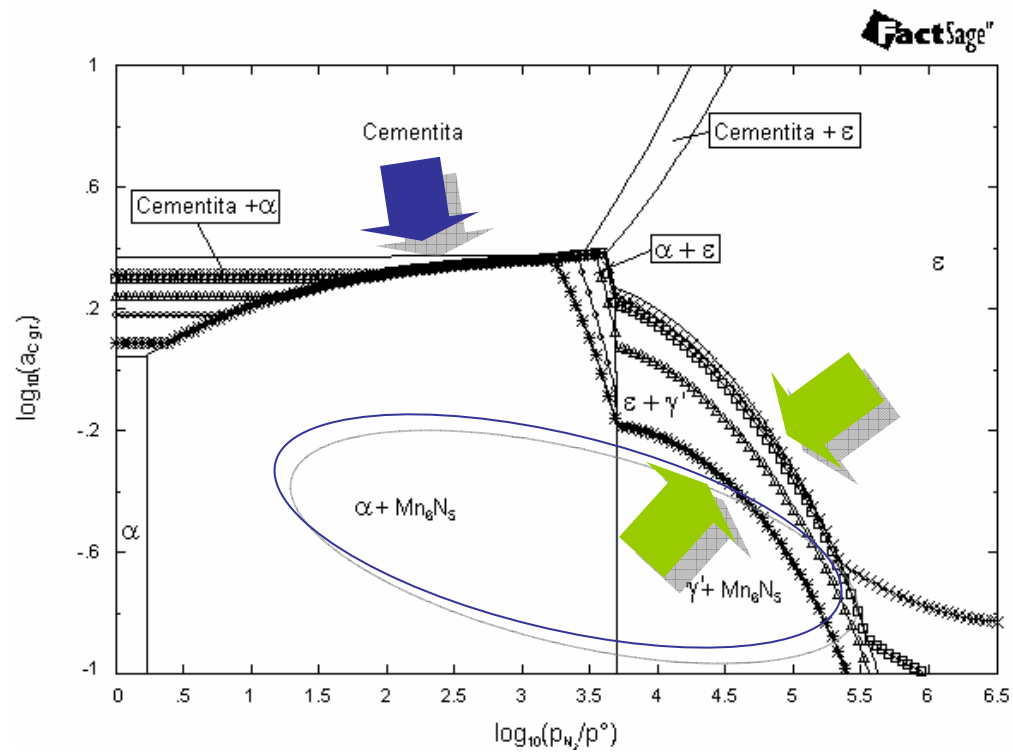


Fe-N-C-Mn T = 560 [°C]

Alloy composition: 99,7%Fe, 0,3%Mn, with several wt.% C

Nitriding of Fe-Mn-C

$x = 1\%C$, $\square = 0,8\%C$, $\Delta = 0,4\%C$ e $\circ = 0,2\%C$

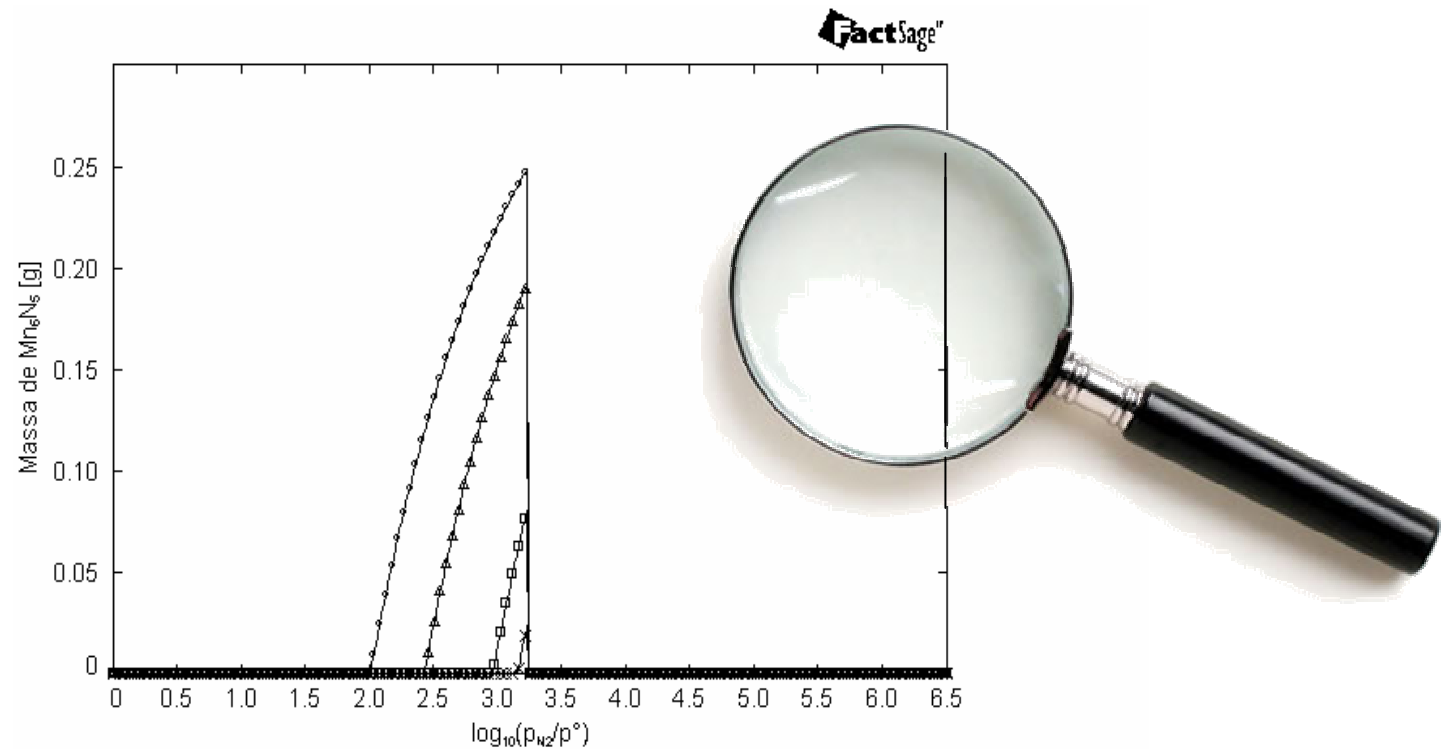


Fe-N-C-Mn T = 560 [°C]

Alloy composition: 99,1%Fe, 0,9%Mn, with several wt.% C

Nitriding of Fe-Mn-C

$x = 1\%C$, $\square = 0,8\%C$, $\Delta = 0,4\%C$ e $\circ = 0,2\%C$

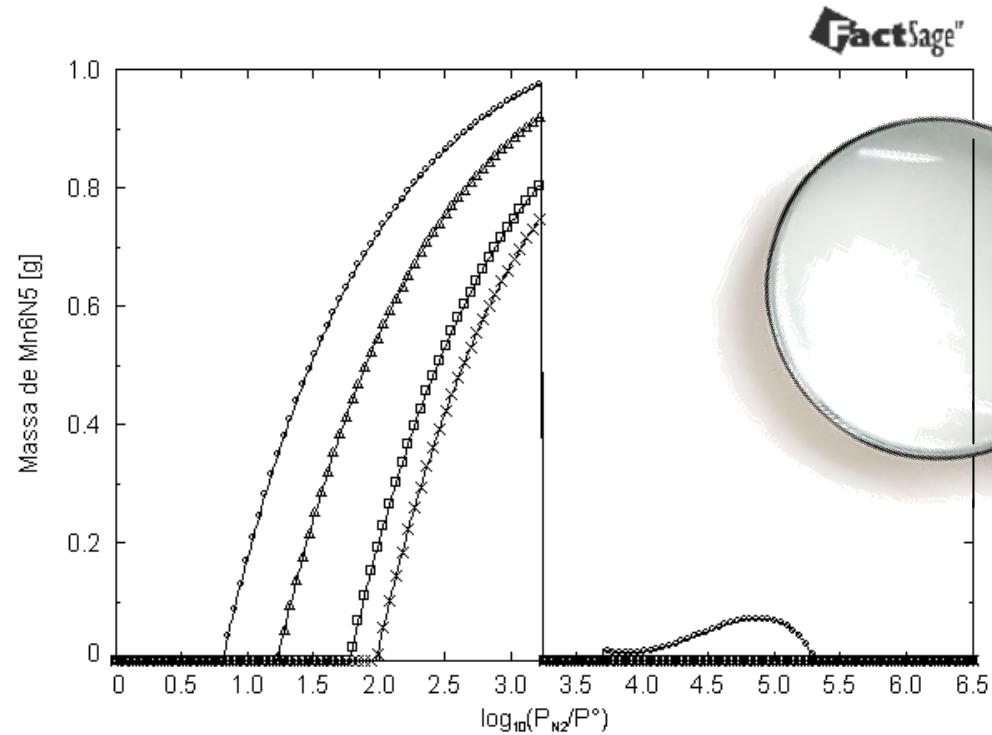


Mn₆N₅ amount, Fe-N-C-Mn T = 560 [°C]

Alloy composition: 99,1%Fe, 0,3%Mn, with several wt.% C

Nitriding of Fe-Mn-C

x = 1%C, □ = 0,8%C, Δ = 0,4%C e ◊ = 0,2%C

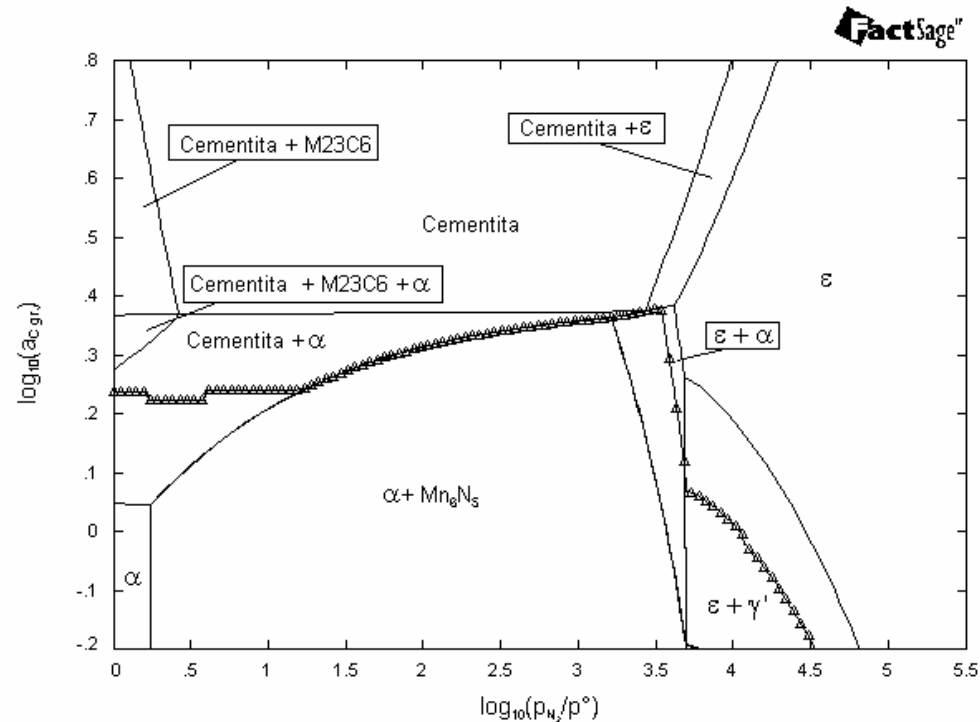


Mn6N5 amount, Fe-N-C-Mn T = 560 [°C]

Alloy composition: 99,1%Fe, 0,9%Mn, with several wt.% C

Nitriding of Fe-Mn-C

x = 1%C, □ = 0,8%C, Δ = 0,4%C e ○ = 0,2%C



Fe-N-C-Mn-Cr-Mo-Si $T = 560$ [°C]

Ref. states: $N_2(g)$, $p^\circ = 1$ [atm], graphite

CrN and Si₃N₄ present in all phase fields

Δ nitriding of a 0,4%C, **0,95%Cr**, **0,2%Mo**, 0,9%Mn e 0,3%Si, rest Fe alloy

~ SAE 4140

Danke!

