

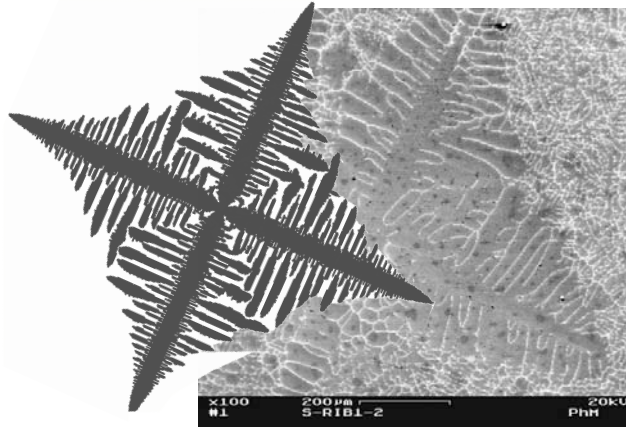


# Global and local equilibrium during solidification - modelling of microsegregation

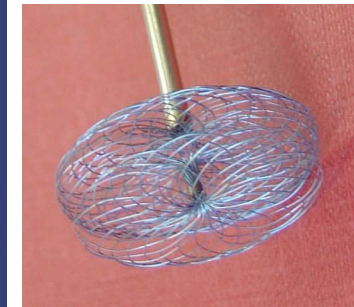
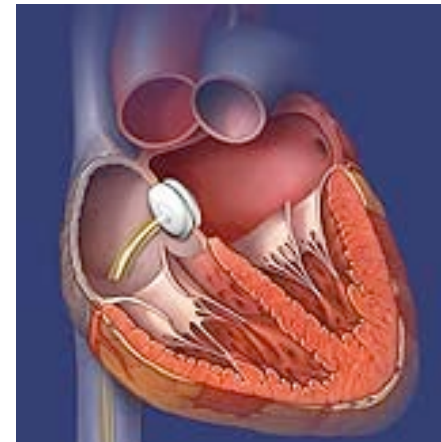
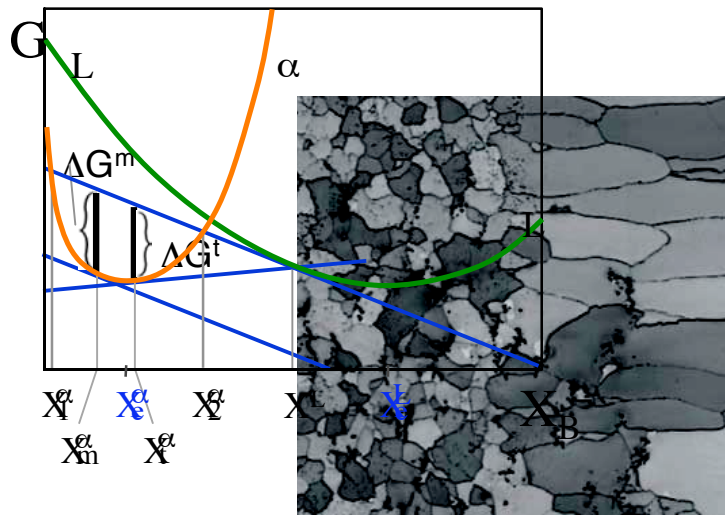
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Institute of Materials Science and Technology  
Metallic Materials

Prof. H.E. Exner, Prof. A. Roosz, Dr. T. Kraft, Dr. B. Dutta

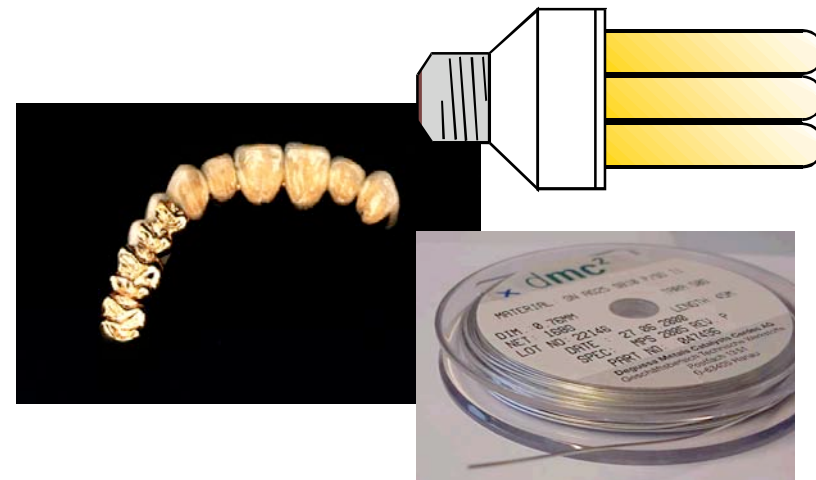
Aachen, June 2007



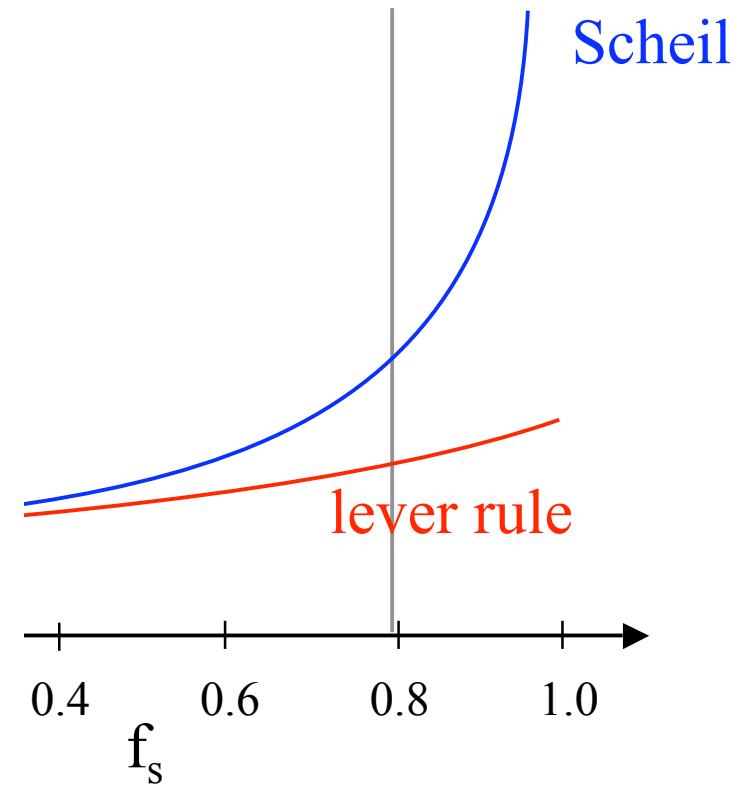
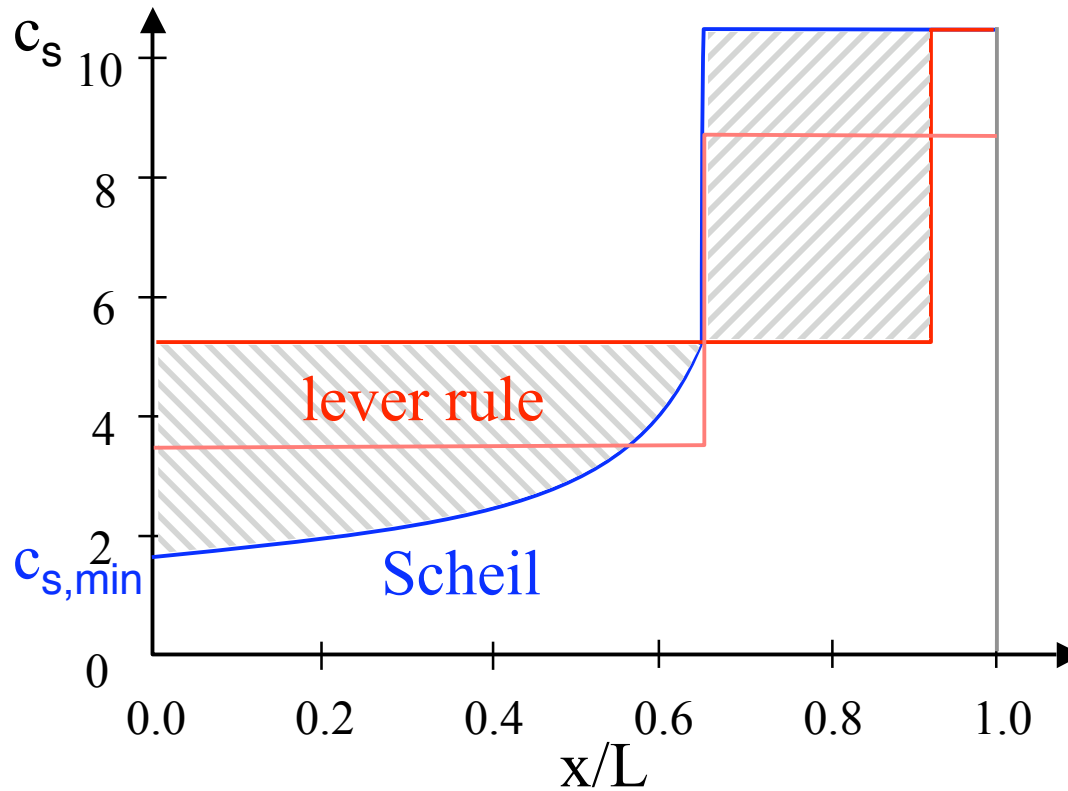
structure formation  
(non-equilibrium) thermodynamics



implant alloys



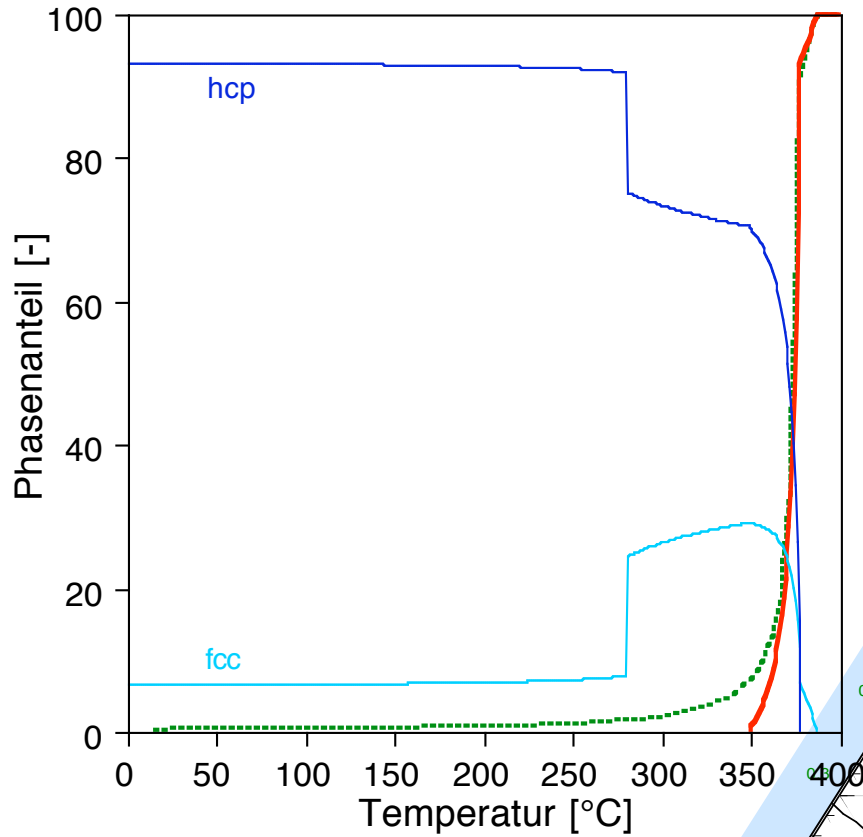
alloy development



Scheil:

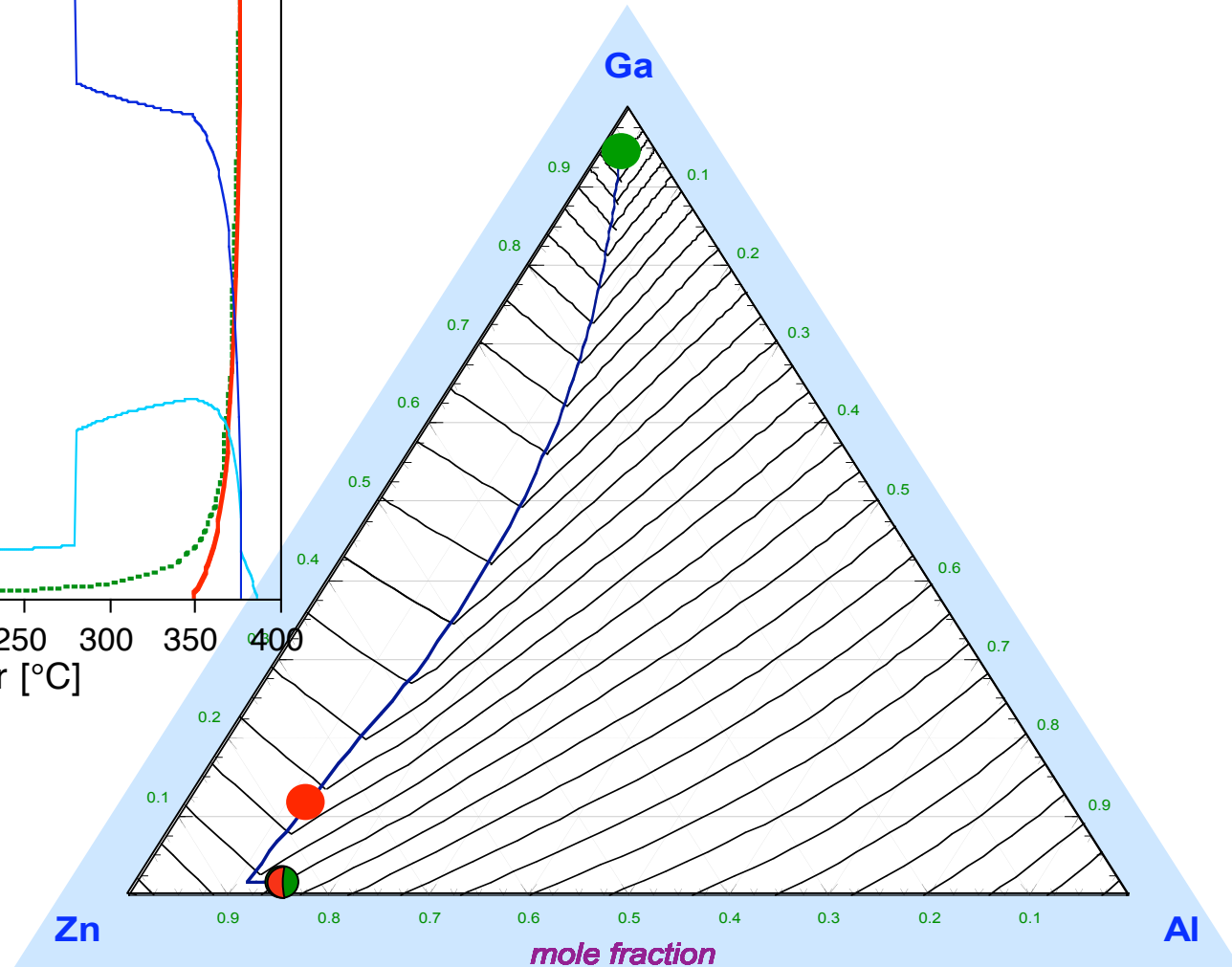
- starts at  $c_{s,\min} = k_{\text{eq}} \cdot c_0$
- ends at  $c_{s,\max} = \infty$  ( $\Rightarrow$  divergent)

Scheil:  $c^*(t)$  and  $c(x)$   
 lever rule:  $c^*(t)$



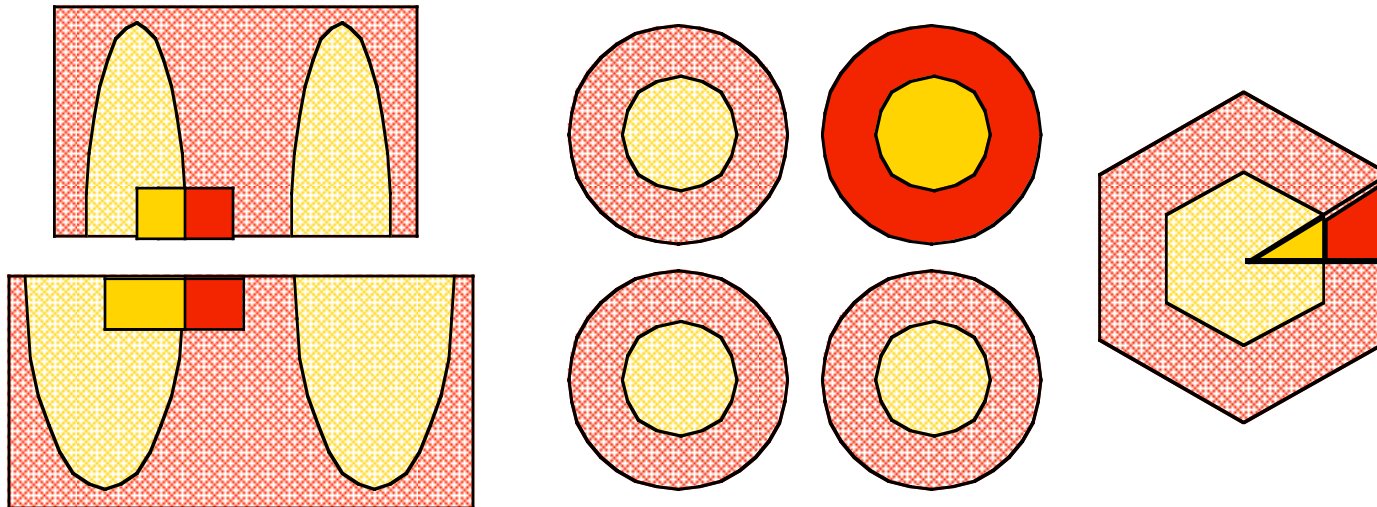
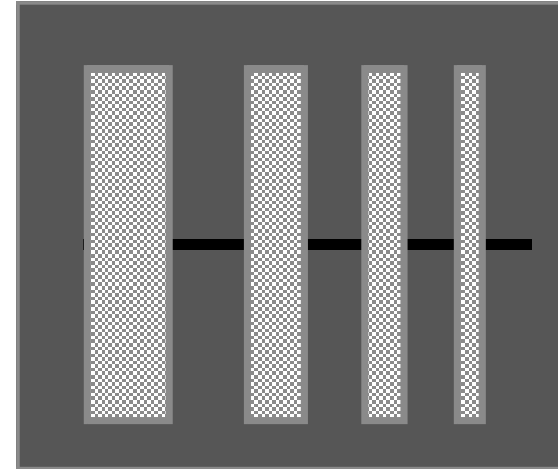
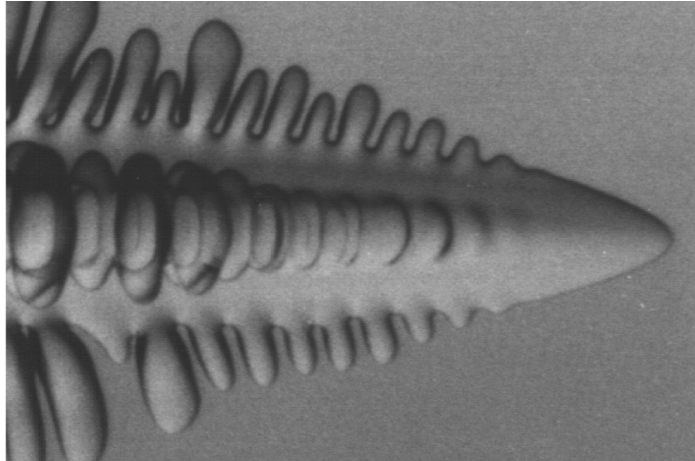
liquid Ga-rich phase at room temperature

- lever rule
- Scheil

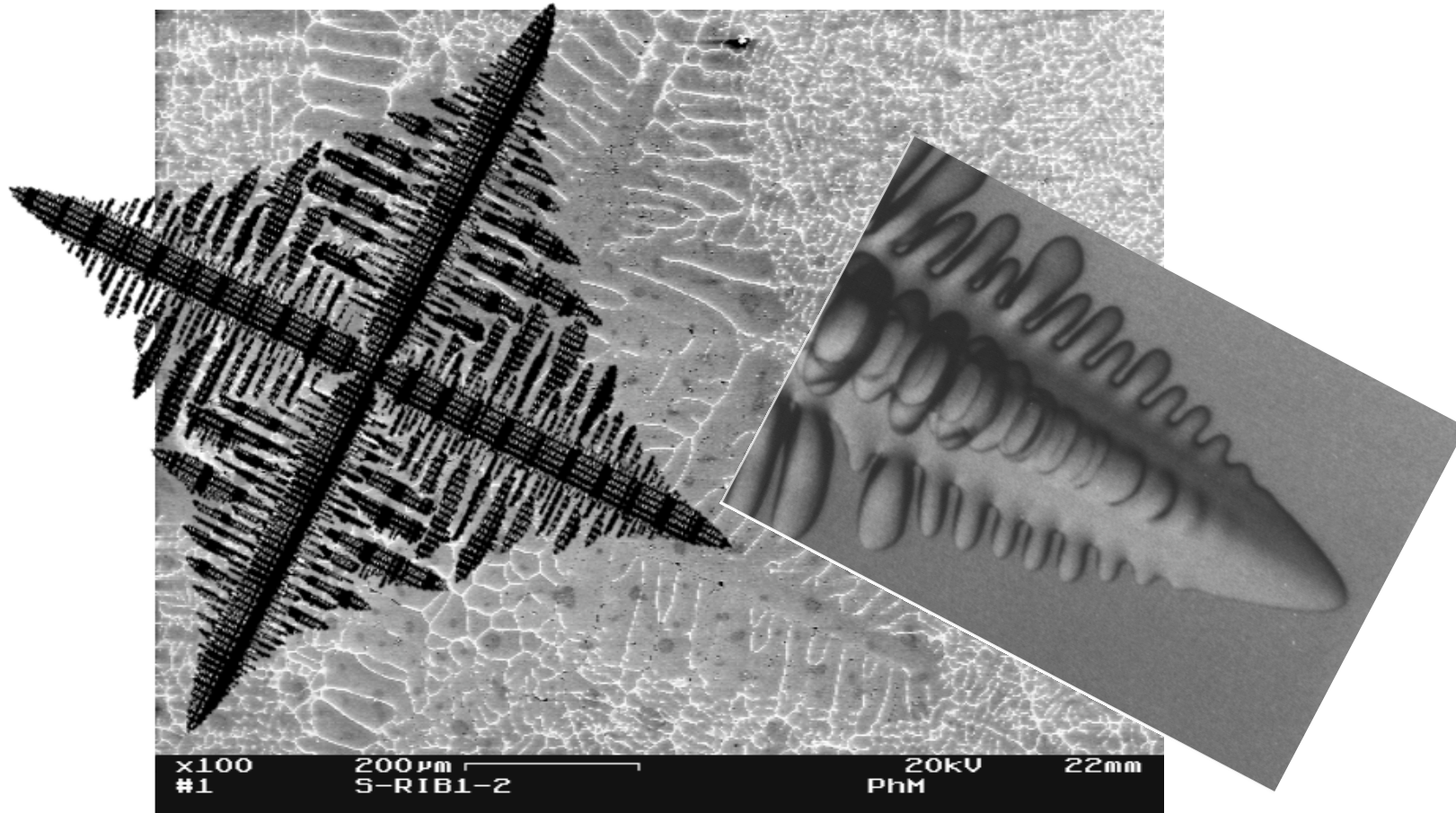




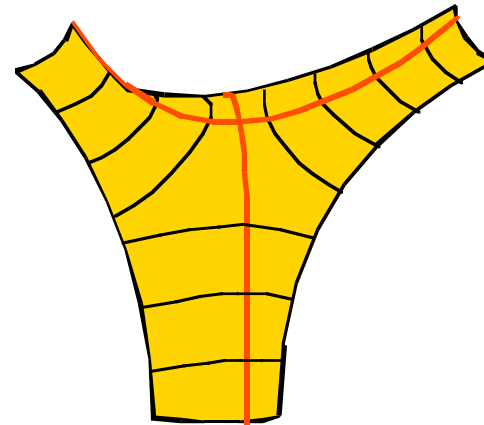
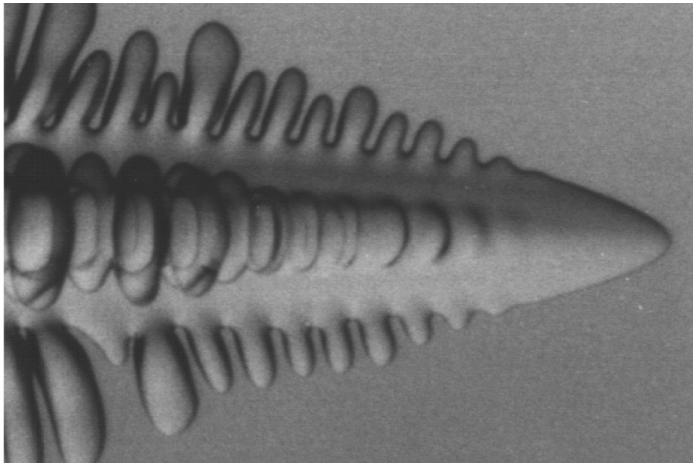
'plate model'



symmetry elements



2D models tend to overestimate the local solid fraction

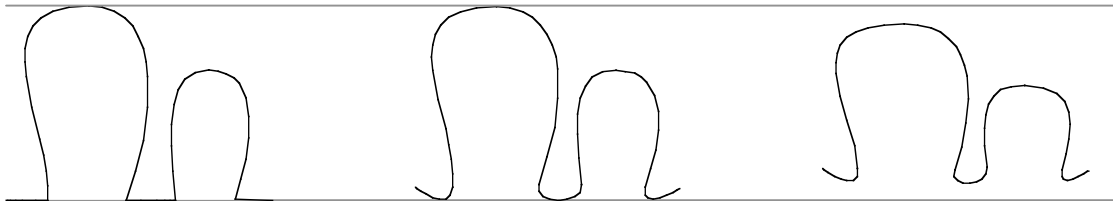


$$K = \frac{1}{r_1} + \frac{1}{r_2}$$

⇒ saddle points

experimental observations:

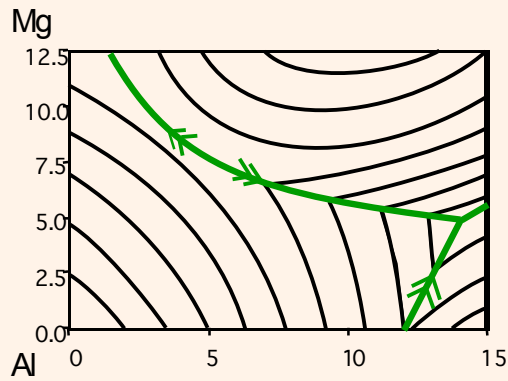
- tip of secondary arm is thicker than root
- equilibration occurs at root



2D coarsening?

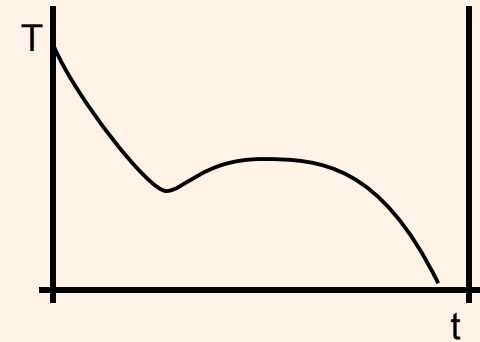
⇒ curvature in 2D is qualitatively wrong!

effects of curvature in 1D can be considered statistically

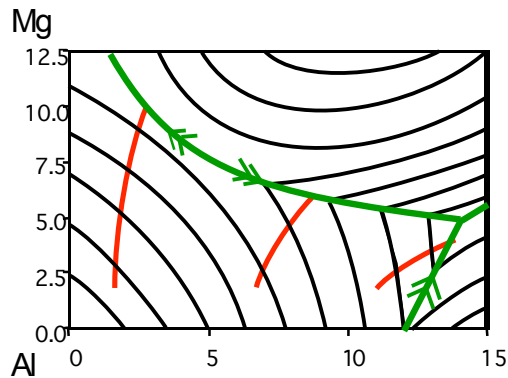
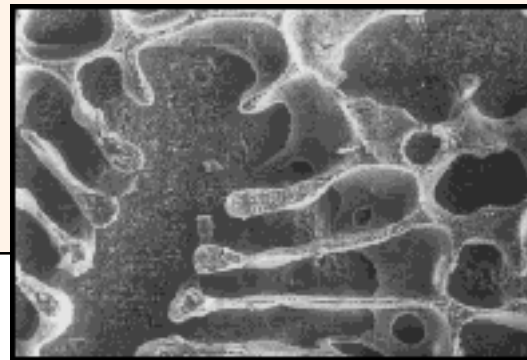


phase diagram  
(tie lines)

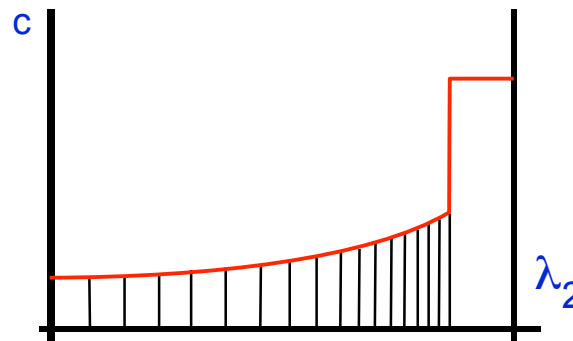
$D_s(T), D_\ell(T)$  diffusion  
 $\sigma, \Delta S_f$  coarsening  
 $\sigma, \Delta S_f$  growth undercoolings  
 $\phi_i$   $\Delta T_E$   
 ...



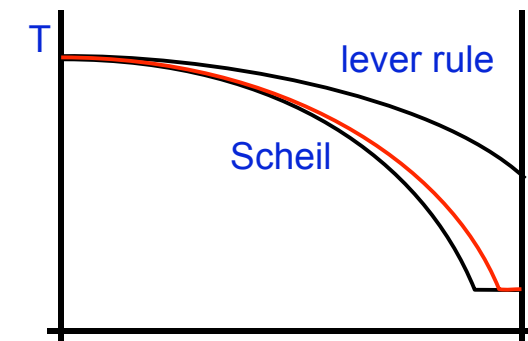
cooling curve



solidification path



concentration profile  
phase fractions



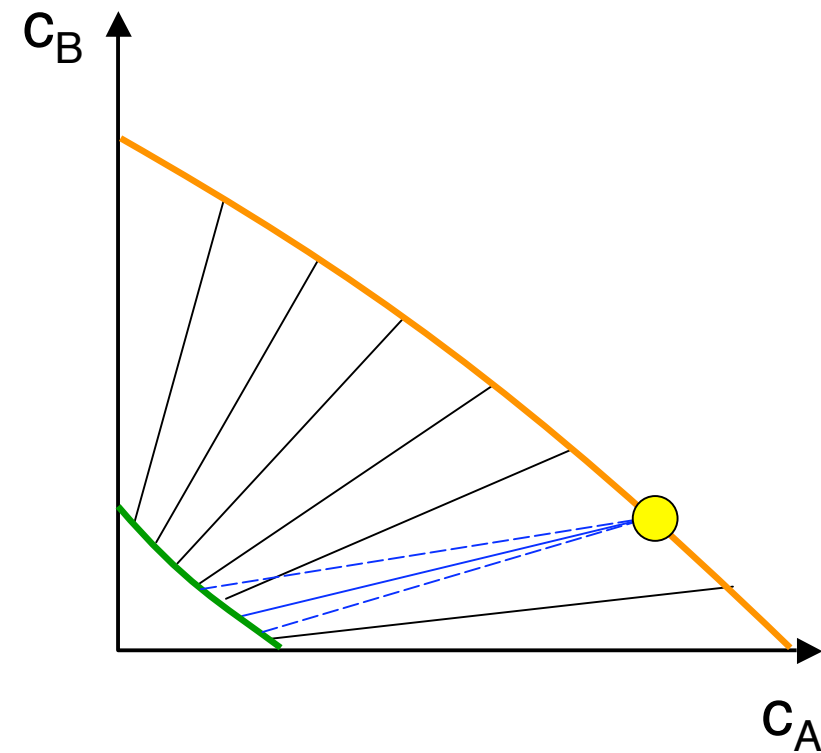
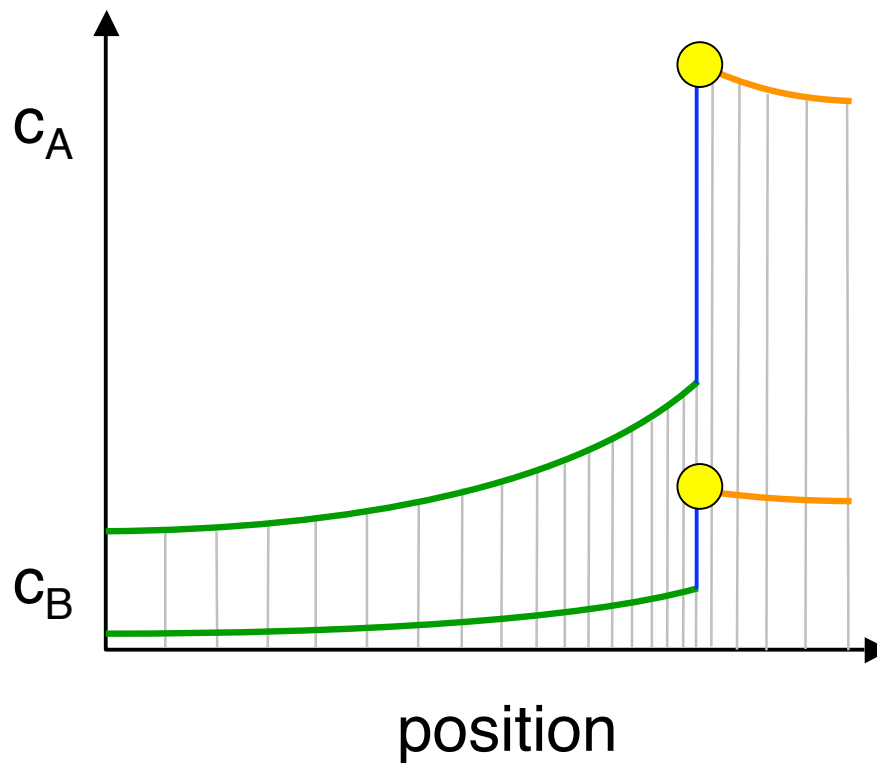
solid fraction  
solidification temperature





- evolution of concentration profile  
diffusion controlled
- interface concentrations connected  
through phase diagram

empirical phase diagram:  
tie-lines not defined  
⇒ calculate tie-lines with ChemApp



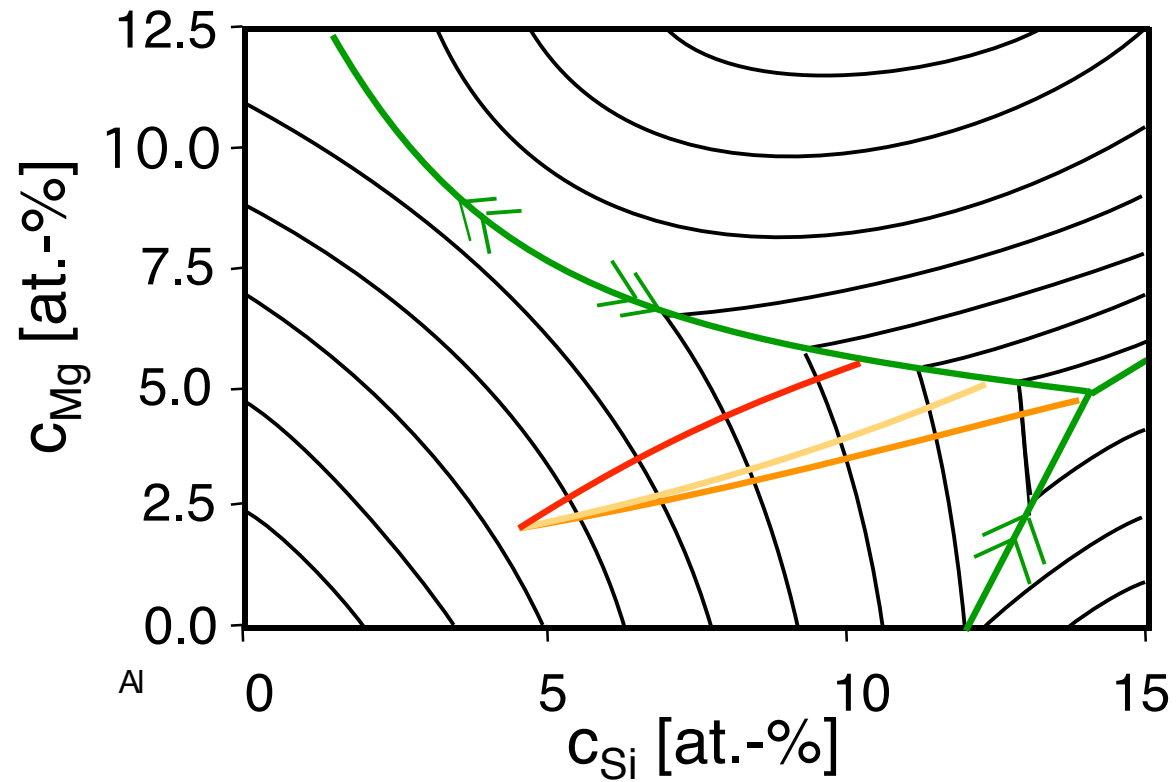


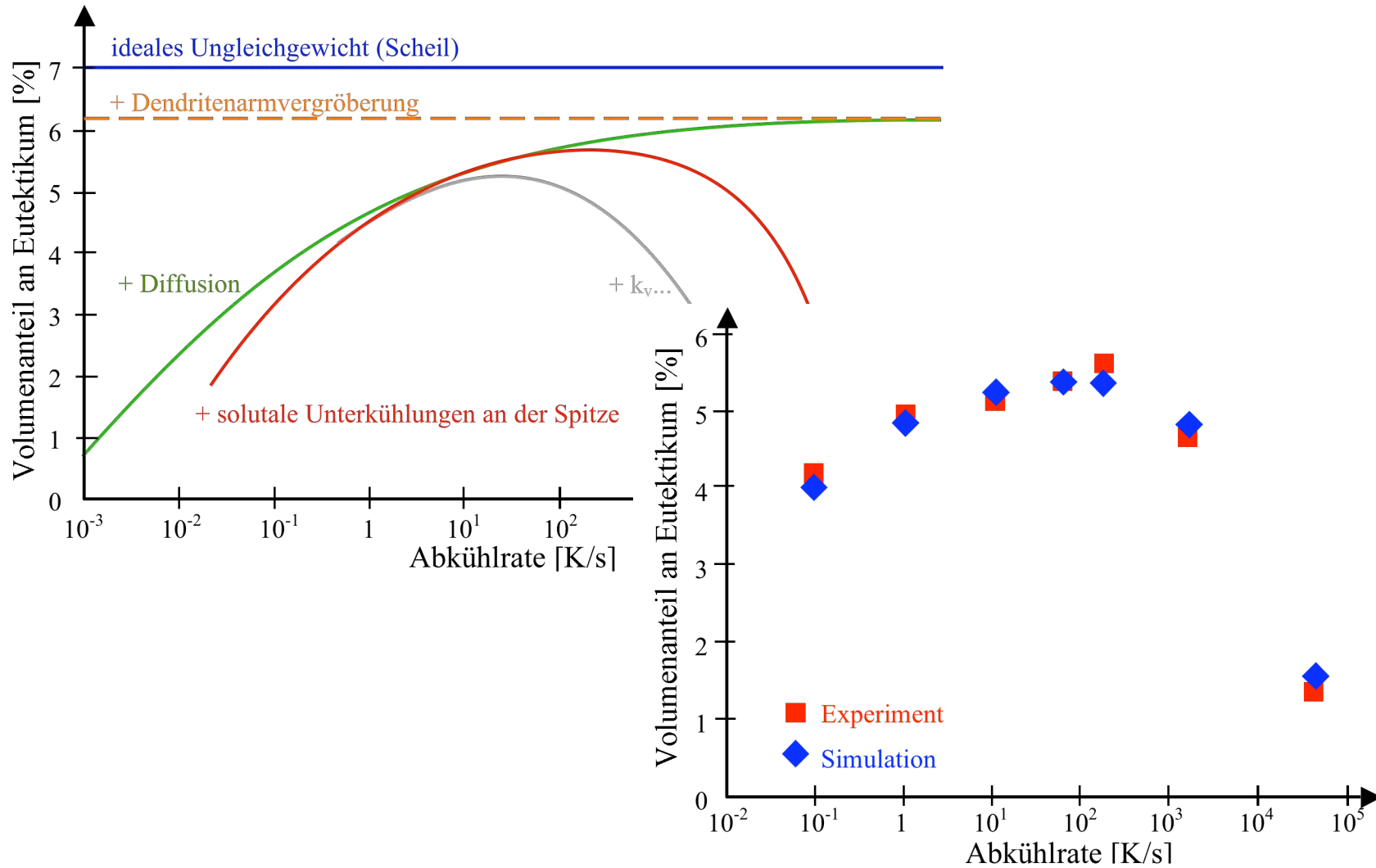
## solidification paths:

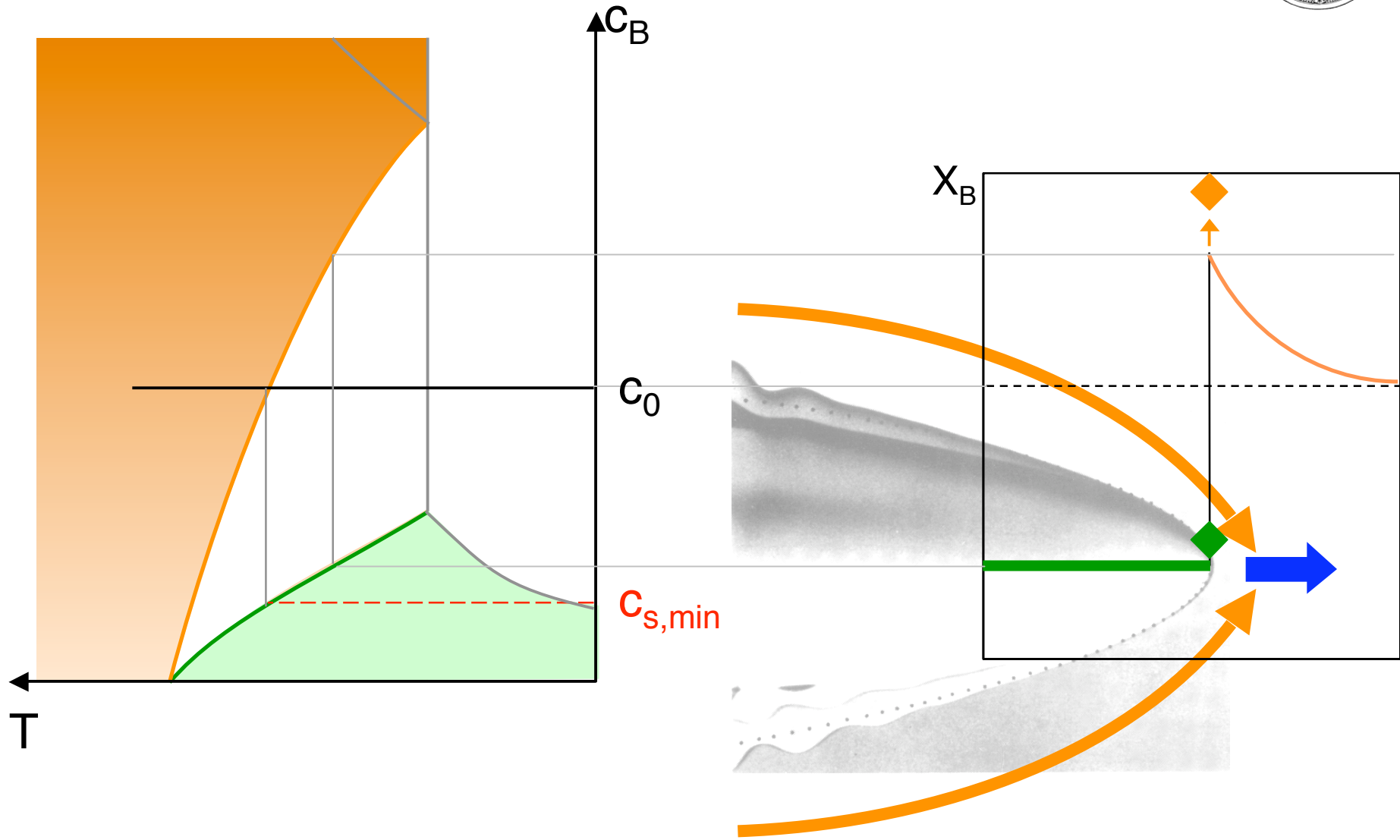
**estimated (steepest slope)**

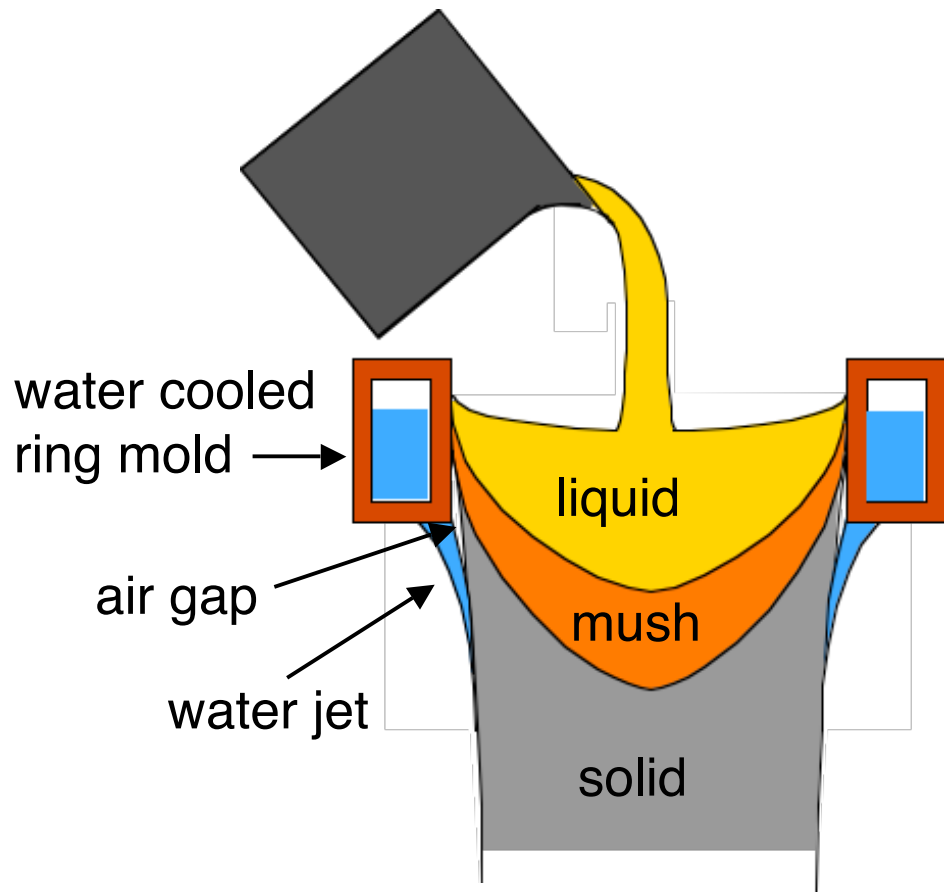
calculated  $D_{s,Mg} = 0, D_{s,Si} = \infty$

calculated  $D_{s,Si} = 0, D_{s,Mg} = \infty$





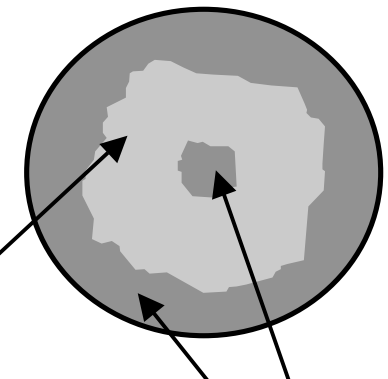
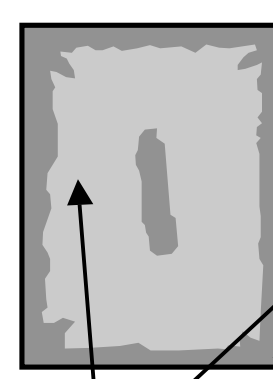
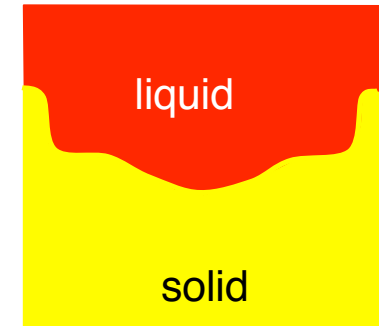
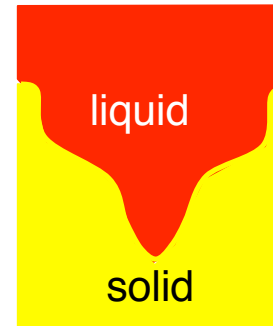




form of liquid pool

sheet ingot

extrusion ingot



stable

metastable

secondary phases

Materials

Al-0.8Fe-0.8Si

Al-1.3Fe-0.1Si

+ Cu, Mn, Cr, Zn & Ti

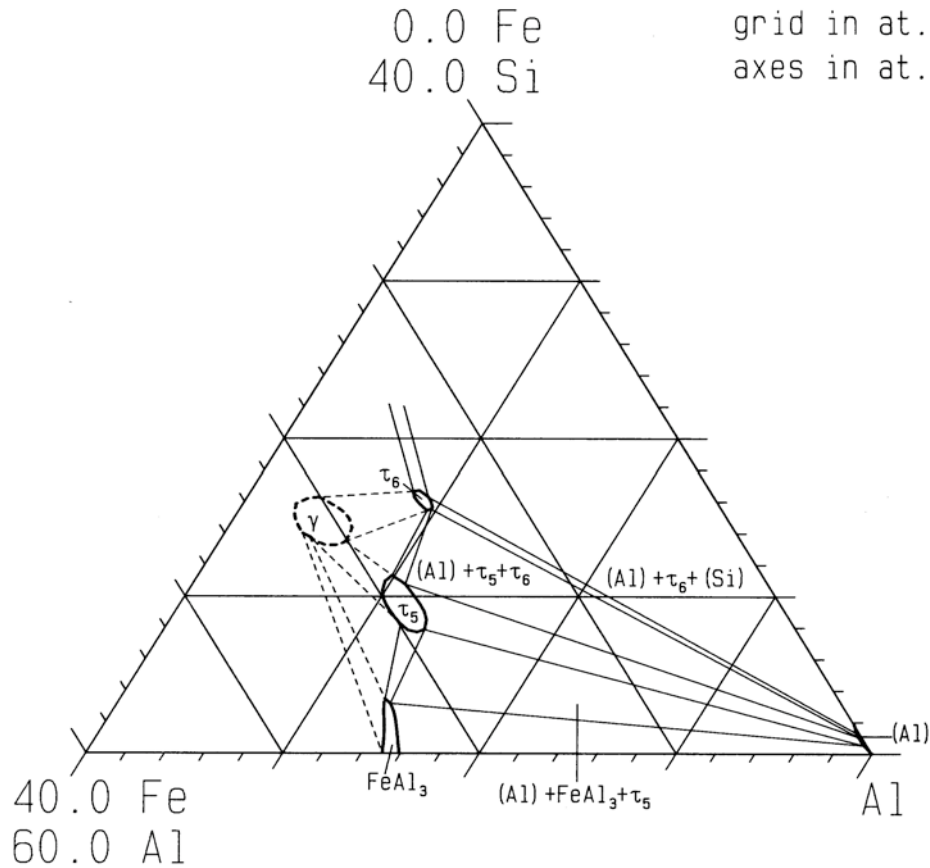


Figure 9: Isothermal section of the Al-corner at 570°C/600°C, see text

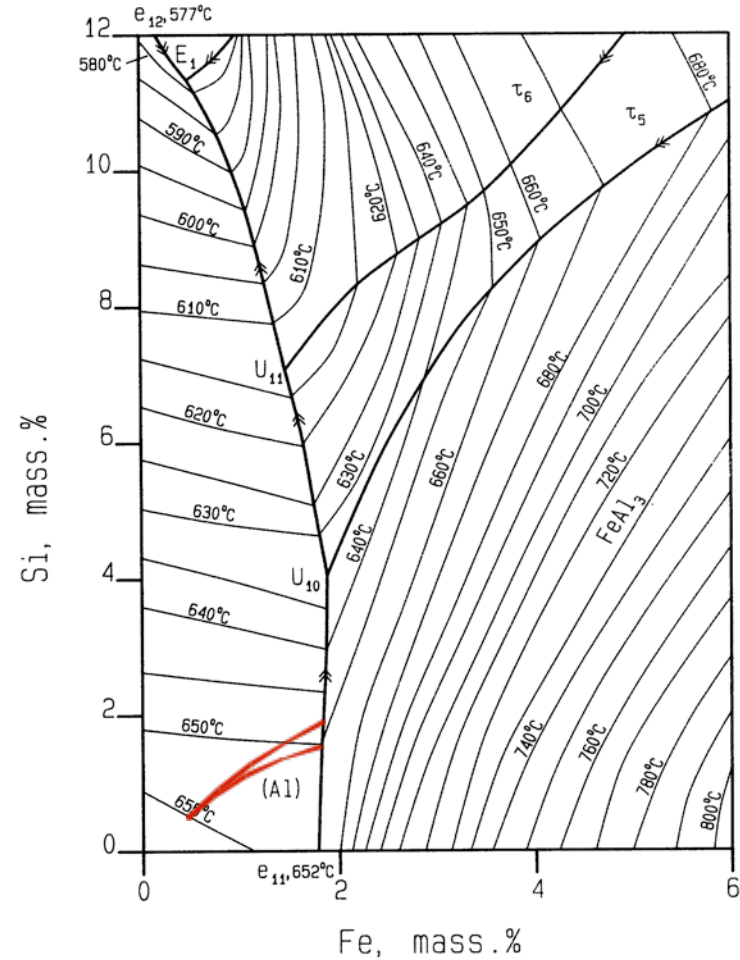
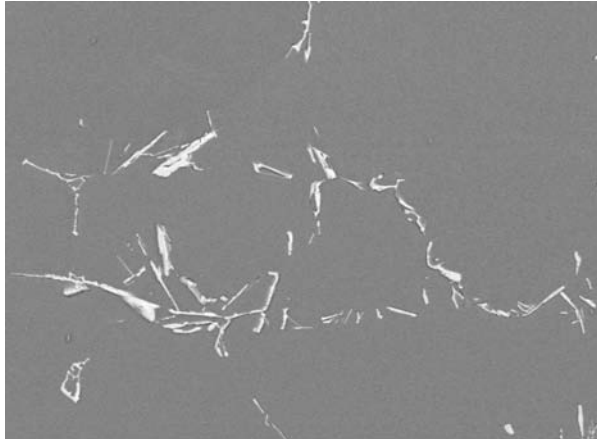
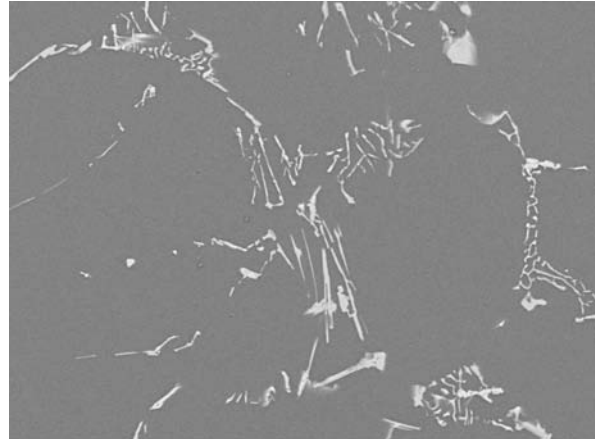


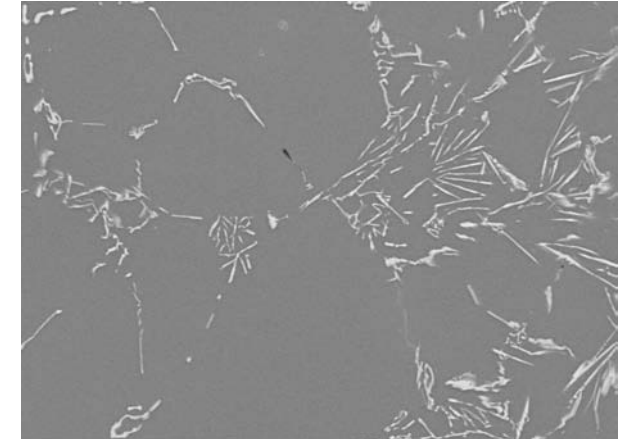
Figure 5: Liquidus surface of the Al-corner of the Al-Fe-Si system



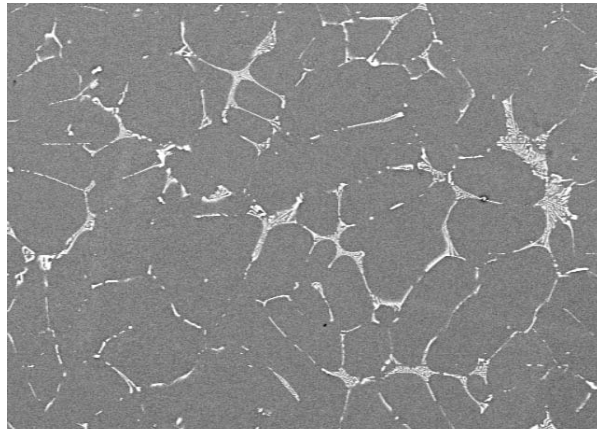
furnace



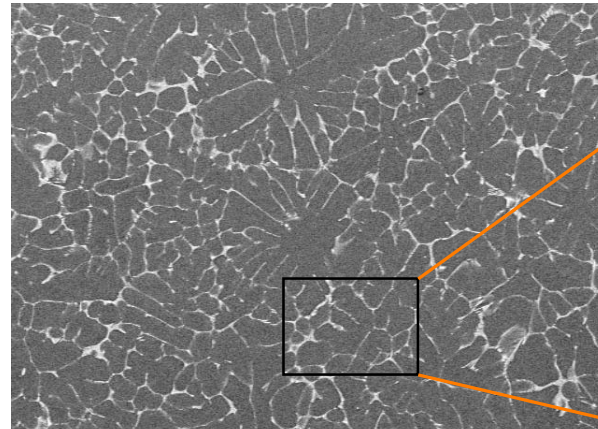
air



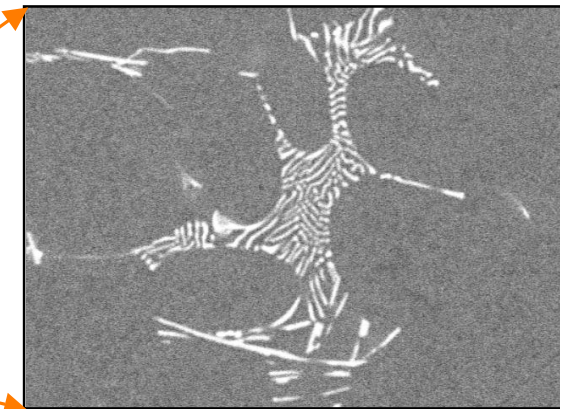
forced air

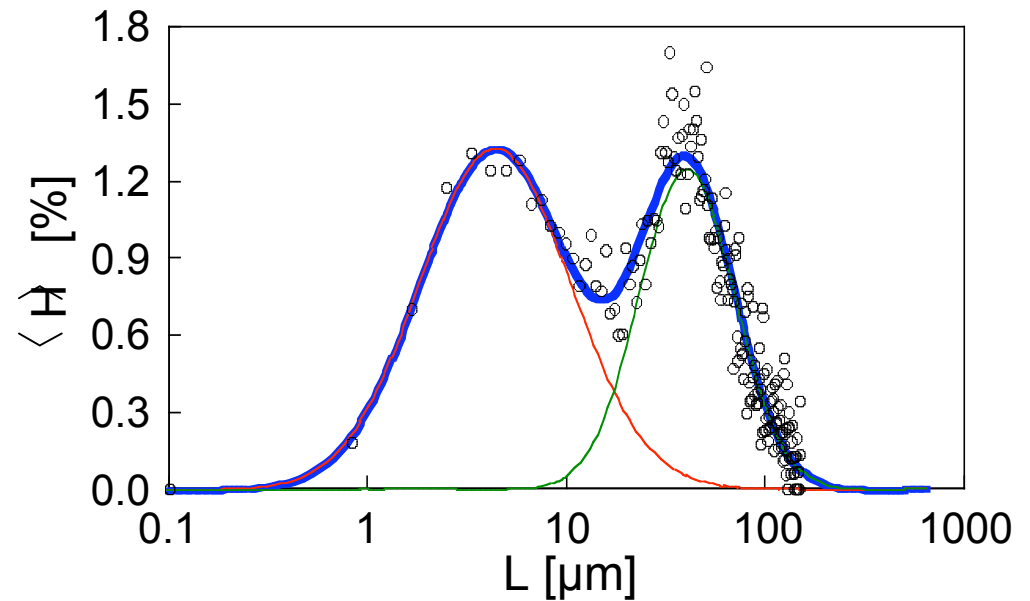
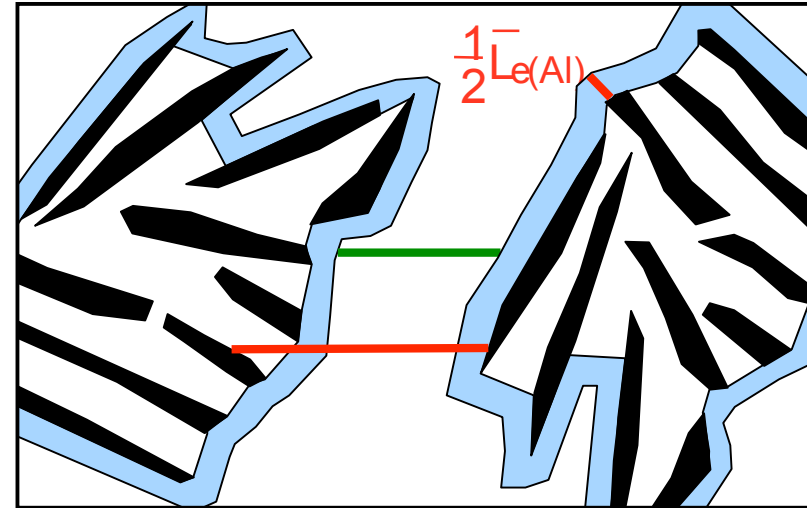
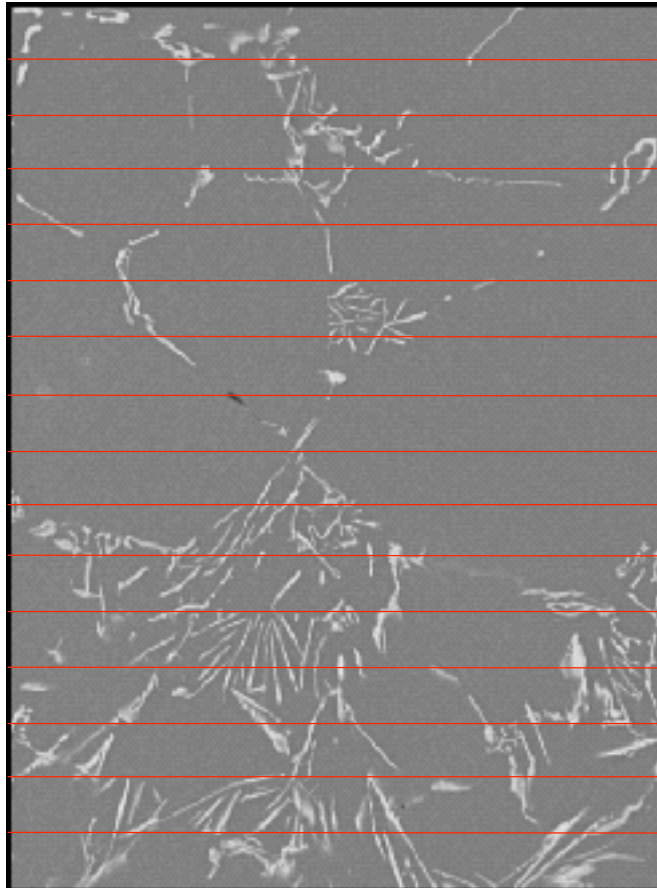


oil

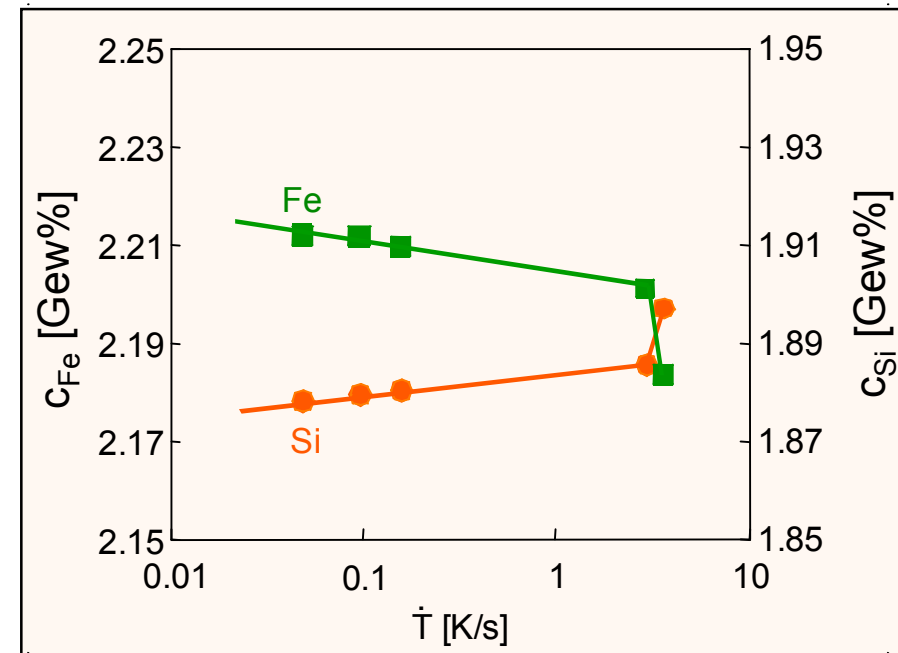
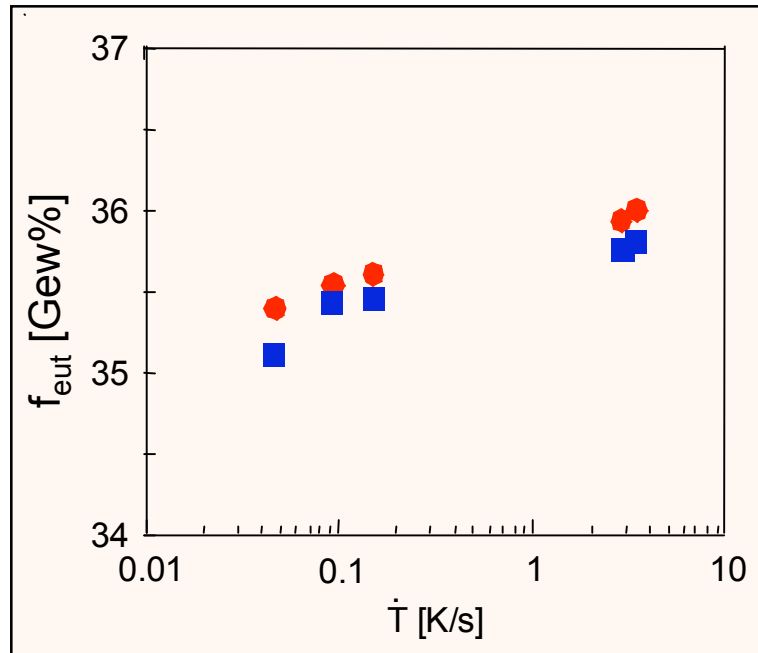


water



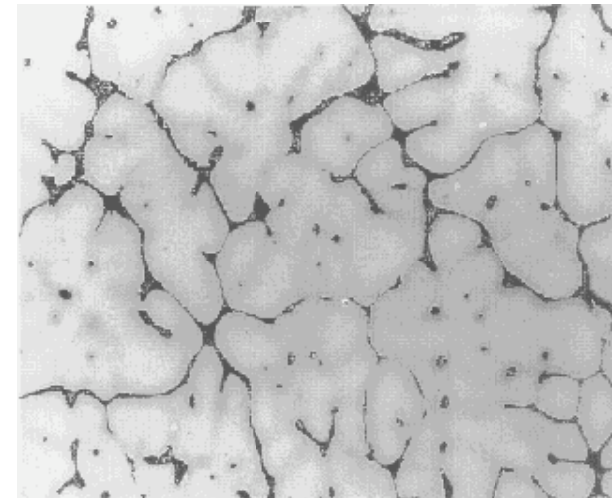
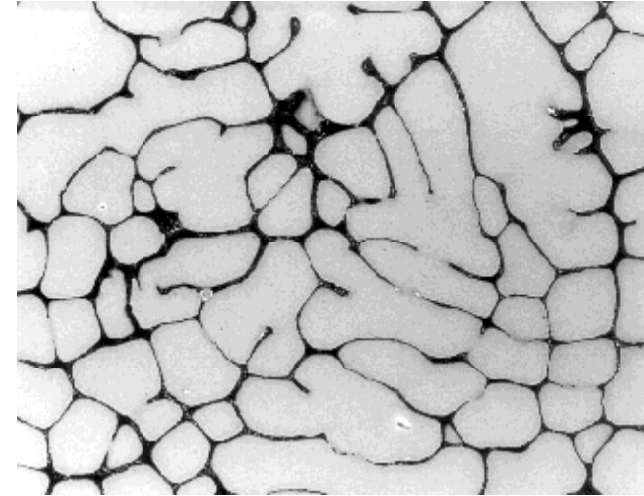
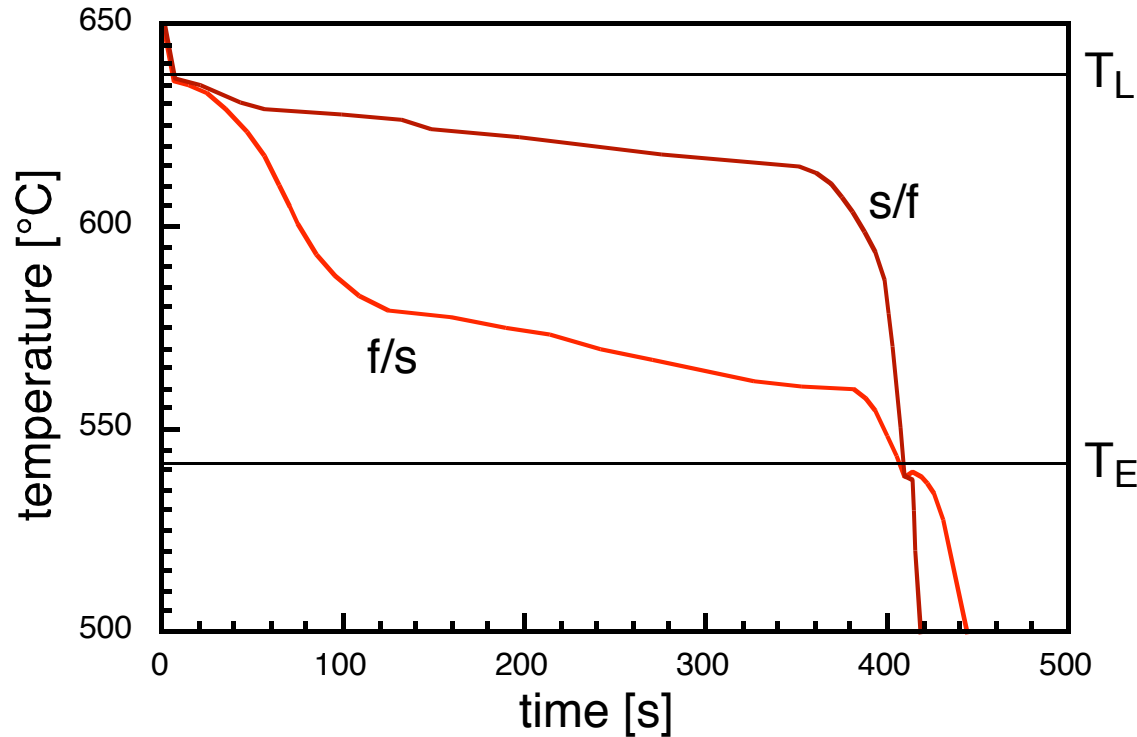








- reduce segregation, e.g. by cooling schedule
- optimize annealing time



eutectic  
fractions

	measured	calculated
s/f	12.0	12.2
lin	10.9	10.7
f/s	9.6	9.6



reliable phase diagrams are a prerequisite for solidification simulation  
kinetic calculations are not meaningful if phase diagram is only estimated

visualization (2D-simulation) is a tool for better understanding  
but: beautiful pictures do not imply accuracy or scientific profoundness

accurate predictions of phase fractions are possible  
measurements are as tedious as modelling  
both lever rule and *analytical* Scheil equations are not sufficient  
⇒ apply Scheil *conditions* ( $D_s = 0$ ,  $D_\ell = \infty$ ) and CALPHAD

technically important features can be determined  
qualitative predictions most important (solidifying phases, solidification path)  
quantitative predictions for design of further processing steps