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Coupling diffusion and local equilibrium in modelling oxidation, nitridation and carburisation

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People Involved

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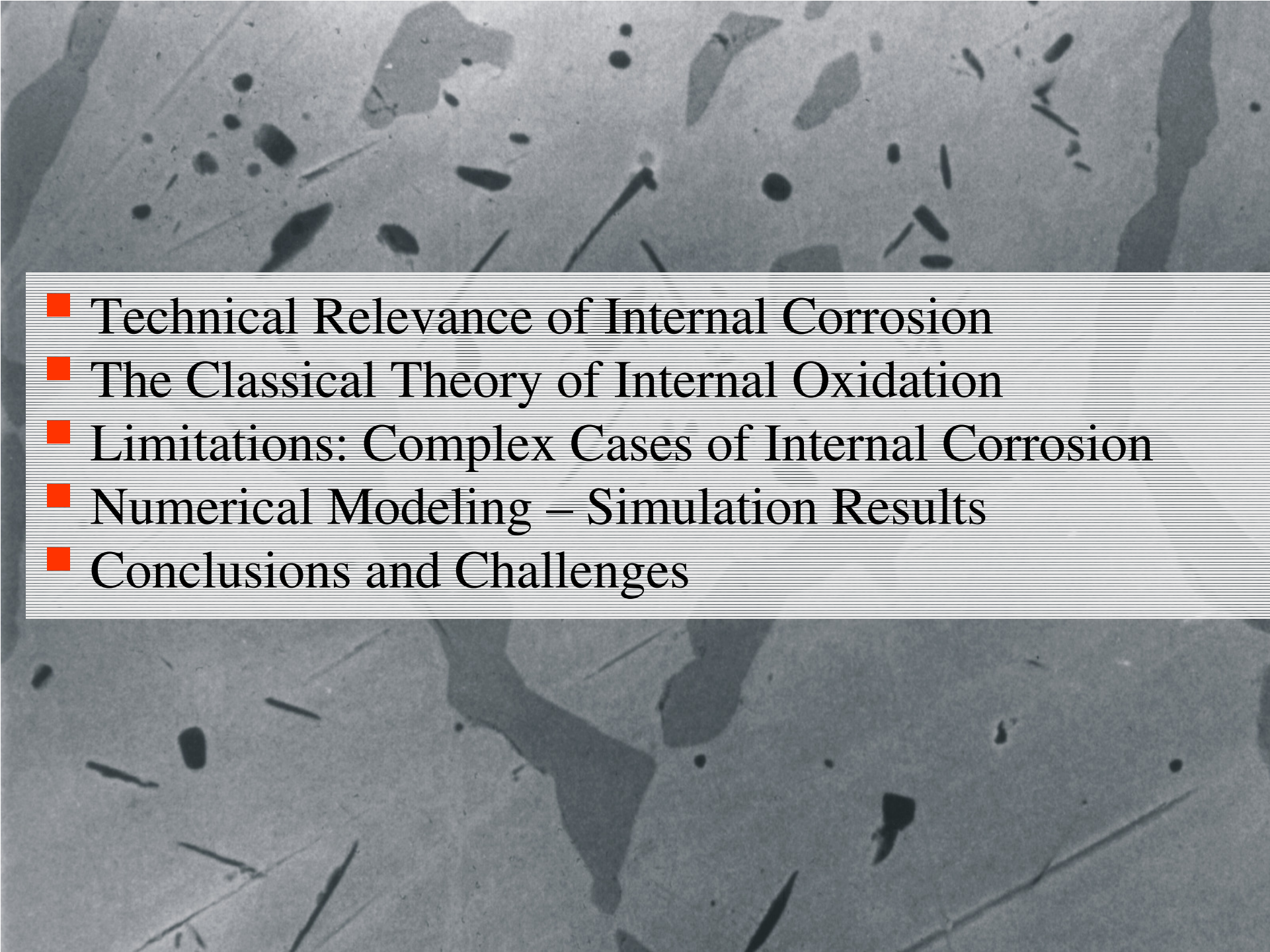
Dr. Klaus Hack

and others

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DFG

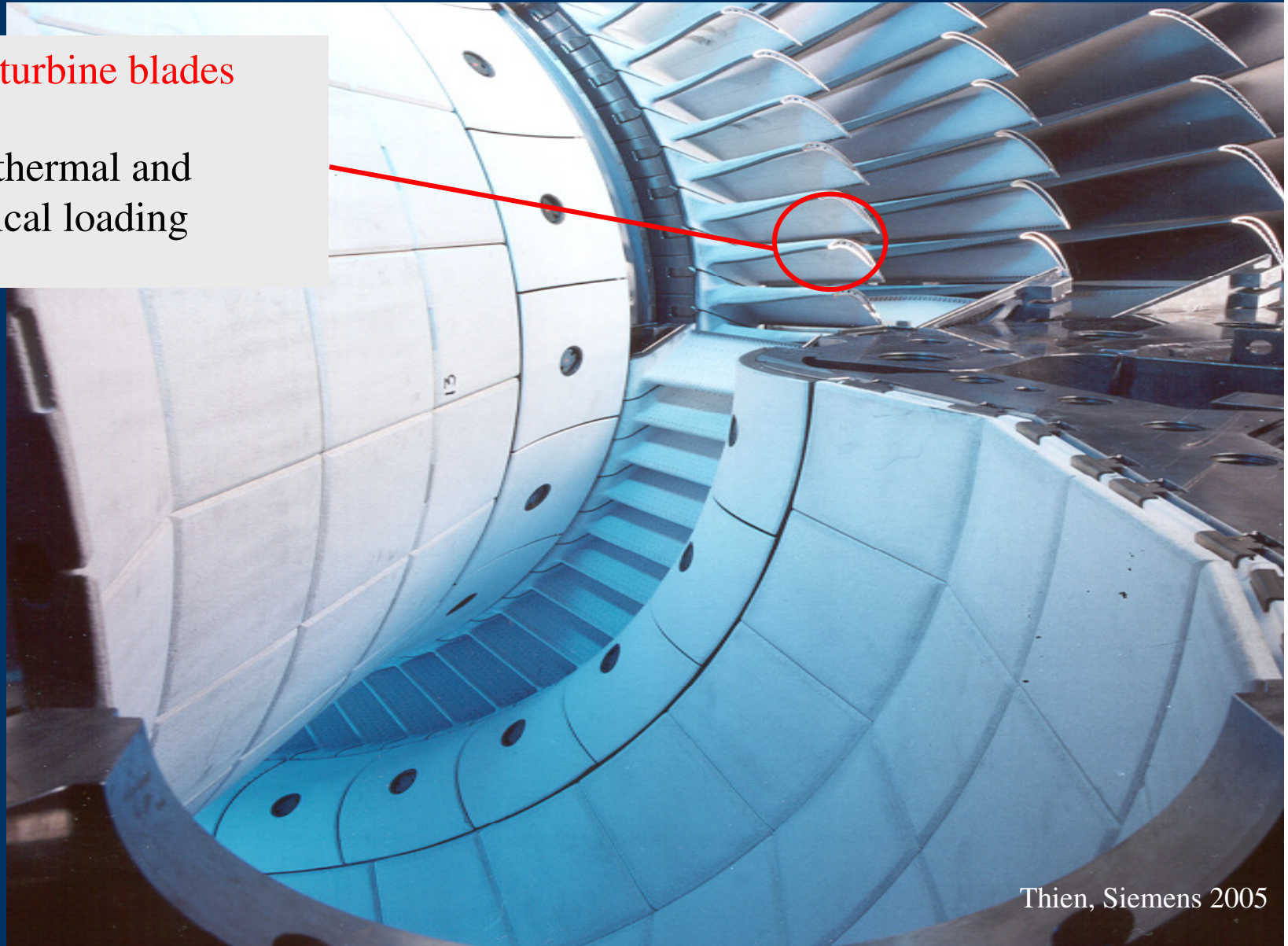
EU project OPTICORR

- 
- Technical Relevance of Internal Corrosion
 - The Classical Theory of Internal Oxidation
 - Limitations: Complex Cases of Internal Corrosion
 - Numerical Modeling – Simulation Results
 - Conclusions and Challenges

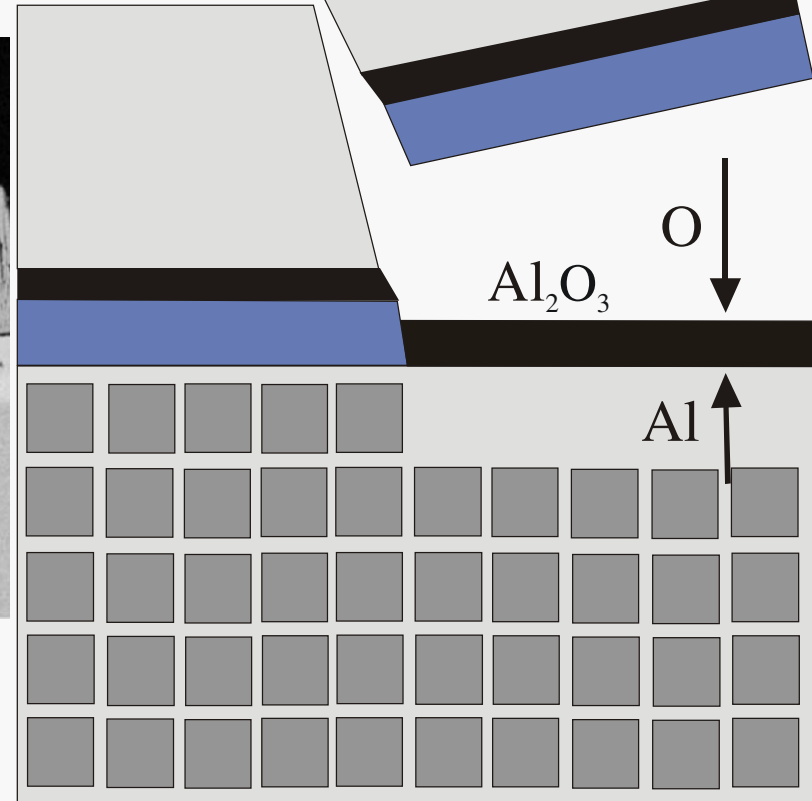
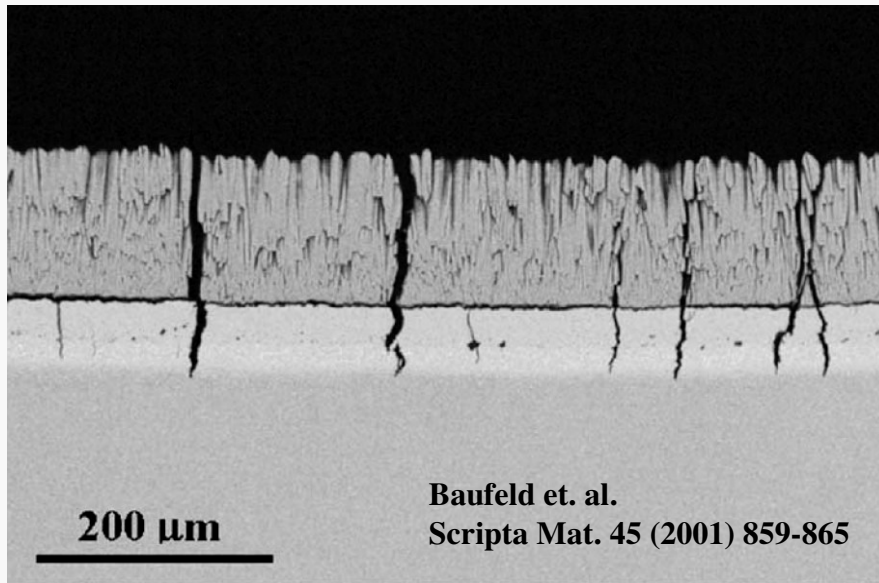
Internal Corrosion of Gas Turbine Blades

1st stage turbine blades

highest thermal and
mechanical loading

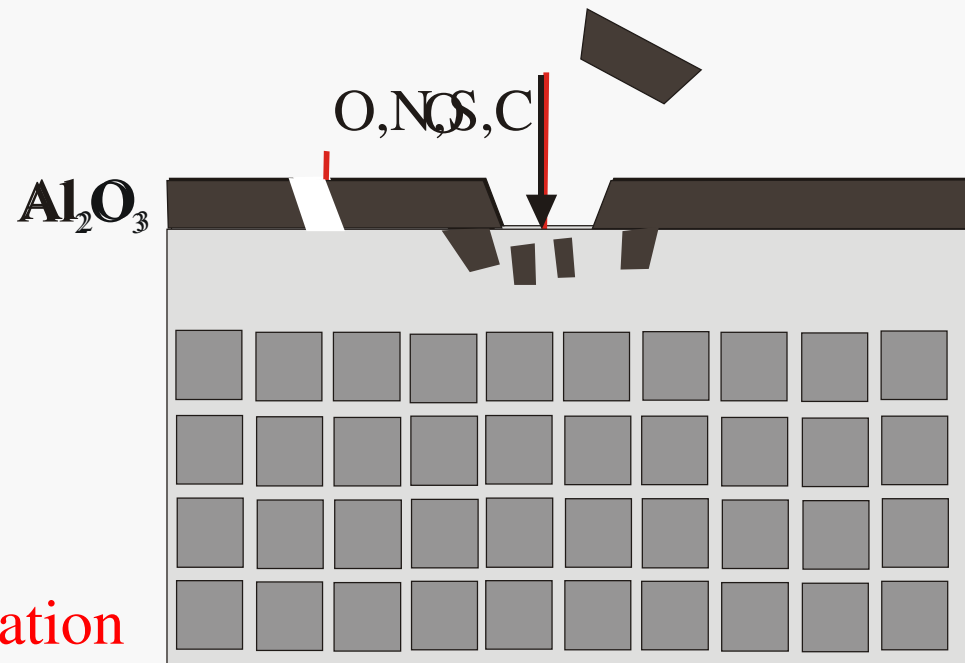


Internal Corrosion as a Consequence of Protective-Scale



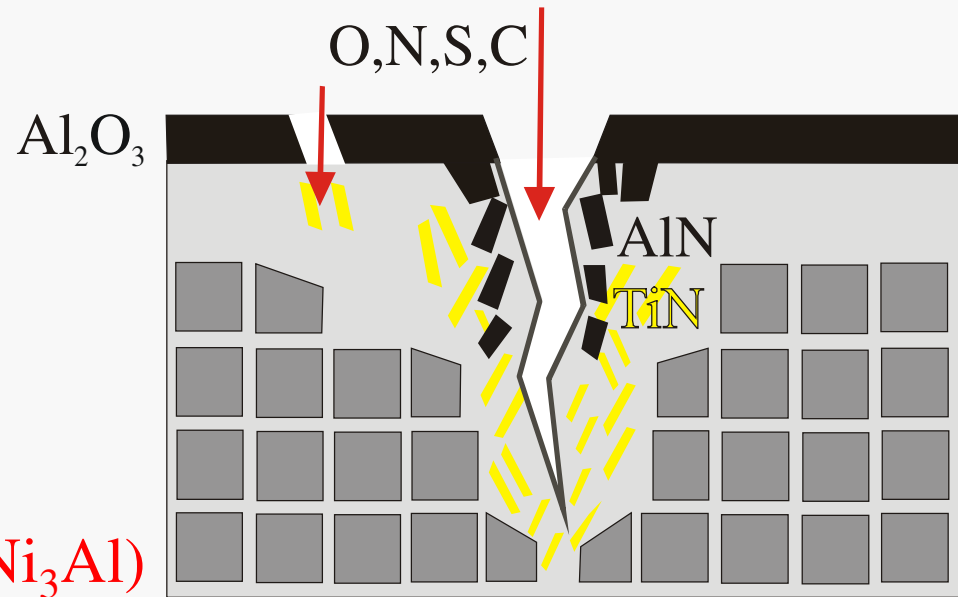
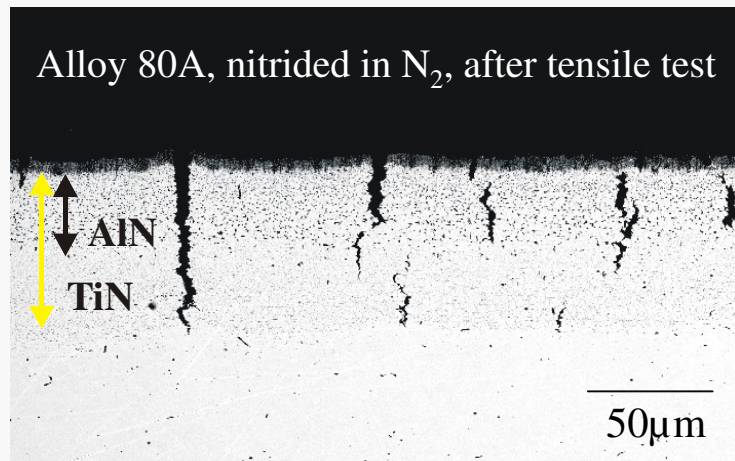
scale spalling/cracking
oxidation of the substrate

Internal Corrosion as a Consequence of Protective-Scale Failure



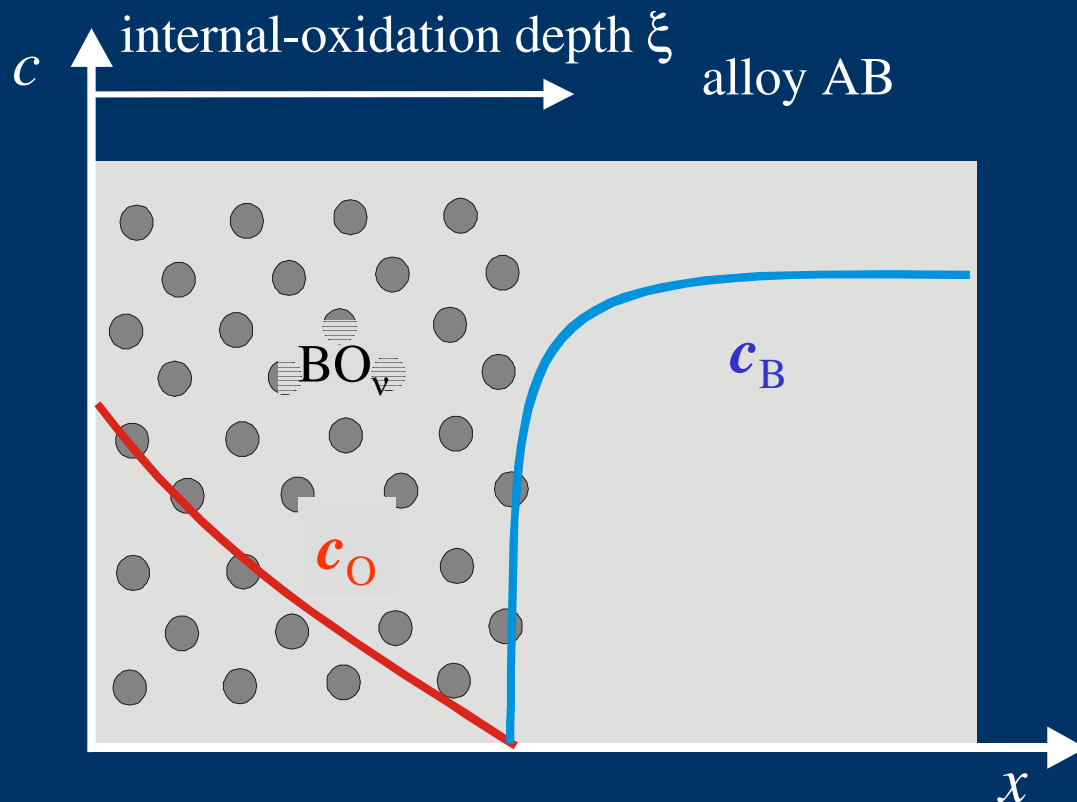
Al depletion
=>transition to internal oxidation
and internal corrosion, e.g., nitridation

Internal Corrosion as a Consequence of Protective-Scale Failure



dissolution of the γ' phase (Ni_3Al)
embrittlement + crack formation

Carl Wagner's Theory of Internal Oxidation



parabolic progress:

$$\xi(t) = 2\gamma\sqrt{D_O t}$$

diffusion PDEs:

$$\frac{\partial c_{O/B}}{\partial t} = D_{O/B} \frac{\partial^2 c_{O/B}}{\partial x^2}$$

solution ($c_{O/B}(x=\xi) = 0$)

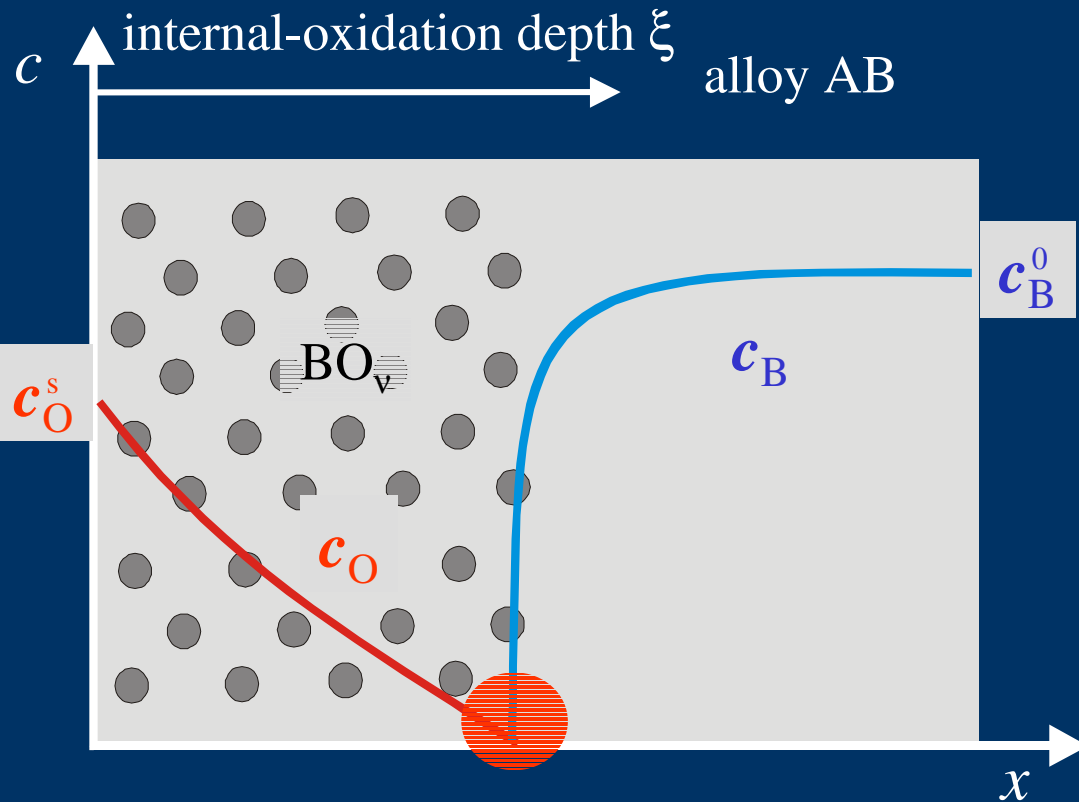
$$c_O = c_0^s \left(1 - \frac{\operatorname{erf}\left(x/2\sqrt{D_O t}\right)}{\operatorname{erf} \gamma} \right)$$

$$c_B = c_B^0 \left(1 - \frac{\operatorname{erfc}\left(x/2\sqrt{D_B t}\right)}{\operatorname{erfc}\left(\gamma\sqrt{D_O/D_B}\right)} \right)$$

C. Wagner, Z. Elektrochemie, 21 (1959) 773

G. Böhm, M. Kahlweit, Acta Met., 12 (1964) 641

Carl Wagner's Theory of Internal Oxidation



diffusional flux at ξ

$$\lim_{\varepsilon \rightarrow 0} \left[-D_O \left(\frac{\partial c_O}{\partial x} \right)_{x=\xi-\varepsilon} \right] = v D_B \left(\frac{\partial c_B}{\partial x} \right)_{x=\xi+\varepsilon}$$

precipitation depth ξ :

$$\xi^2 = \frac{\varepsilon 2 c_O^s D_O}{v c_B^0} t$$

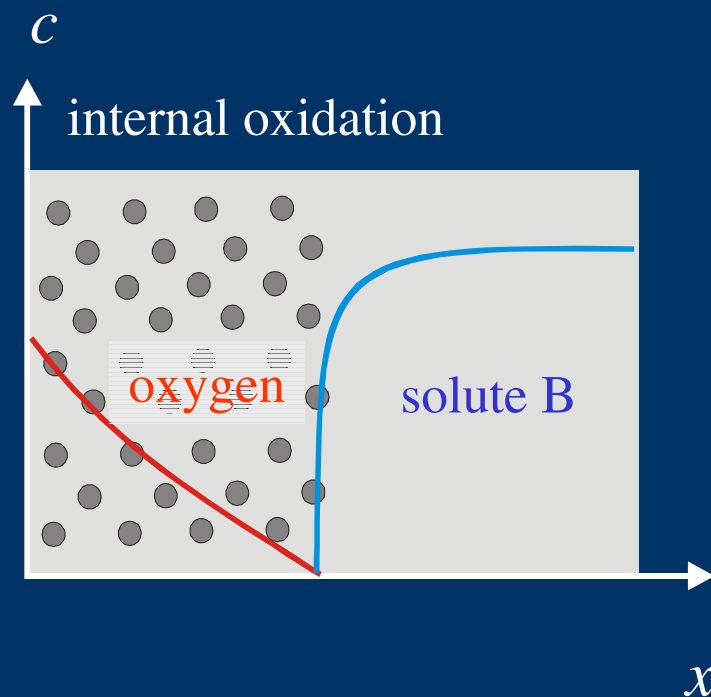
for:

$$D_B / D_O \ll c_O^s / c_B^0 \ll 1$$

ε : labyrinth factor

Carl Wagner's Theory of Internal Oxidation

Limitations:

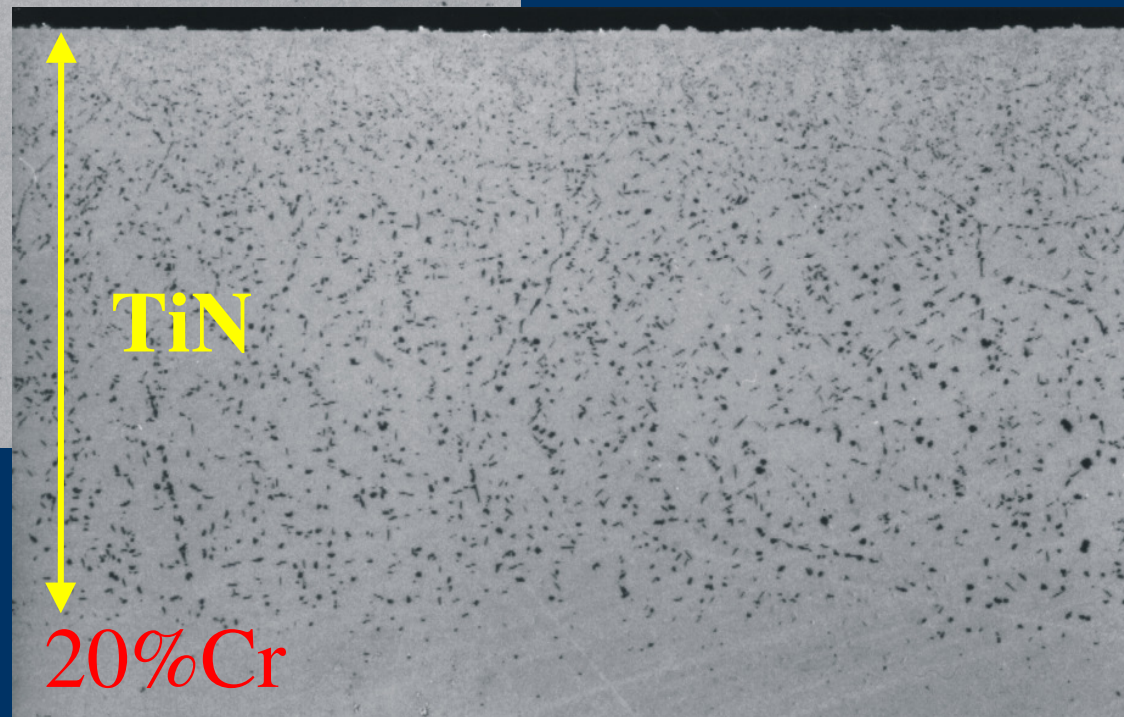
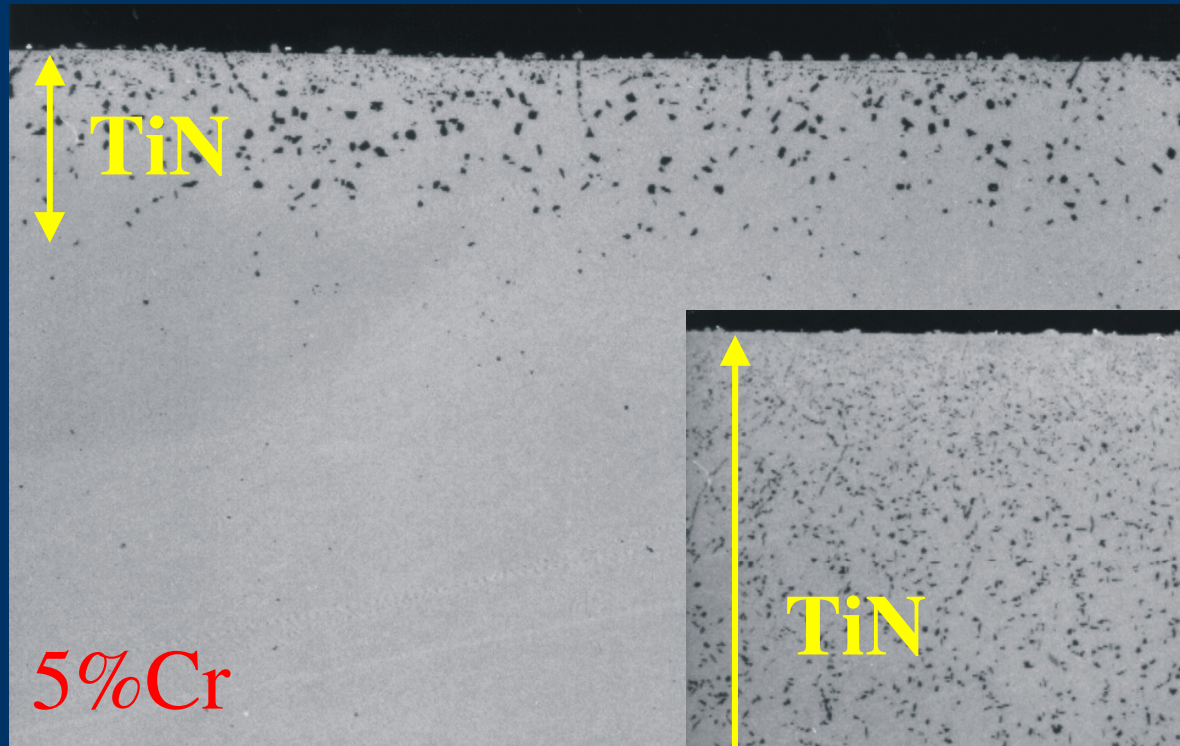


- only one type of precipitating compound
- of high thermodynamic stability (solubility product ≈ 0)
- constant surface concentration of corrosive species (no change in atmosphere or temperature)
- constant diffusivities of the reacting species

compare

J.L. Meijering, *Adv. Met. Res.*, Vol. 5, Wiley 1971, and D. L. Douglass, *Ox. Met.*, 44 (1994) 81

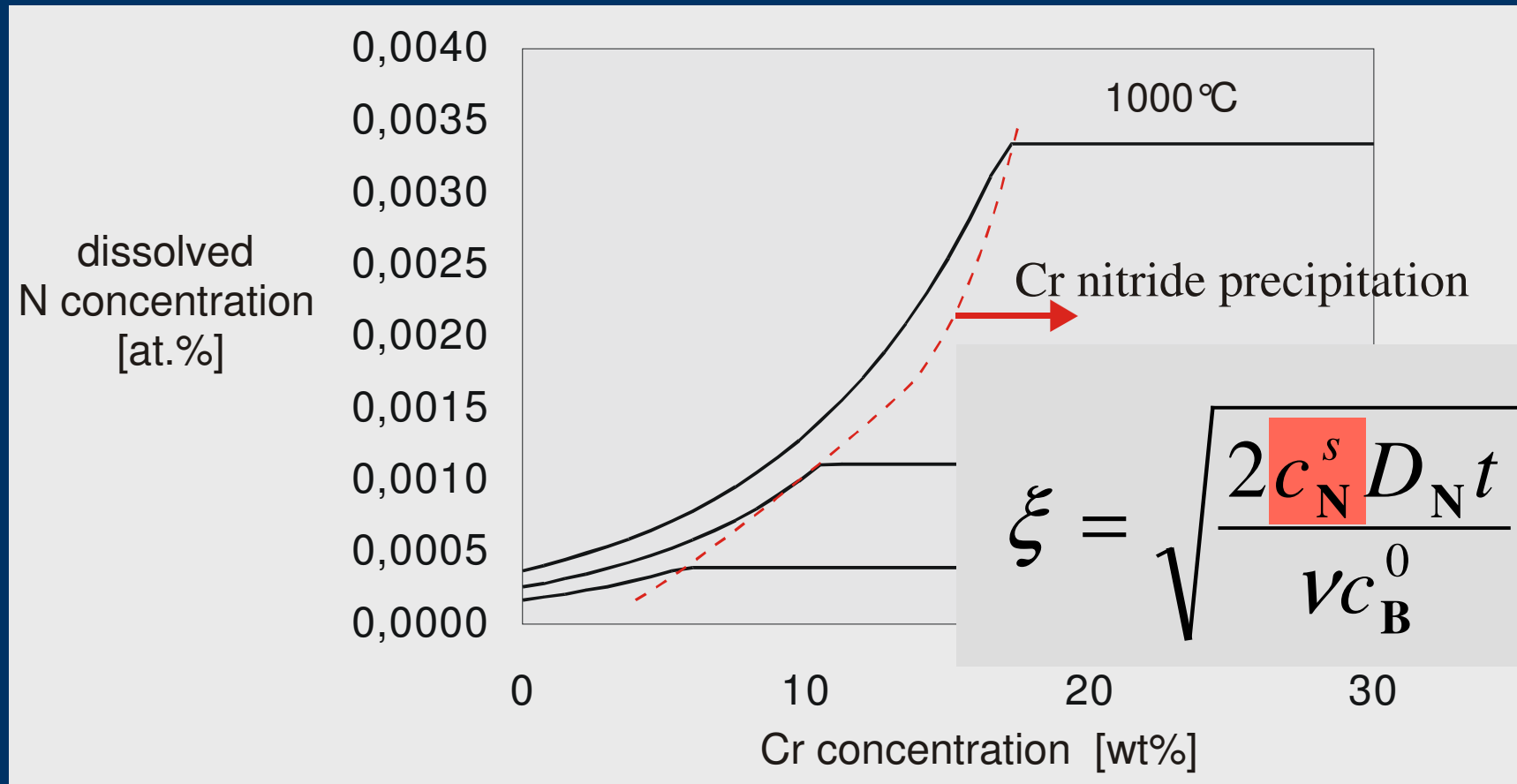
Internal Nitridation of Ni-*x*Cr-2Ti Alloys



— 100 μ m
100h, 1100°C, N₂ atmosphere

Nitrogen Solubility in Ni-Cr Alloys

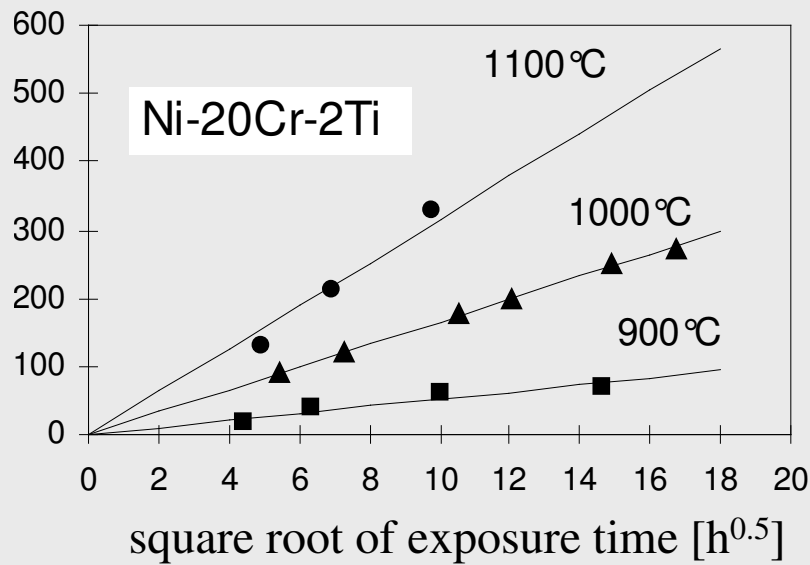
calculated by ChemApp + Ni-Cr-Al-Ti-N data set



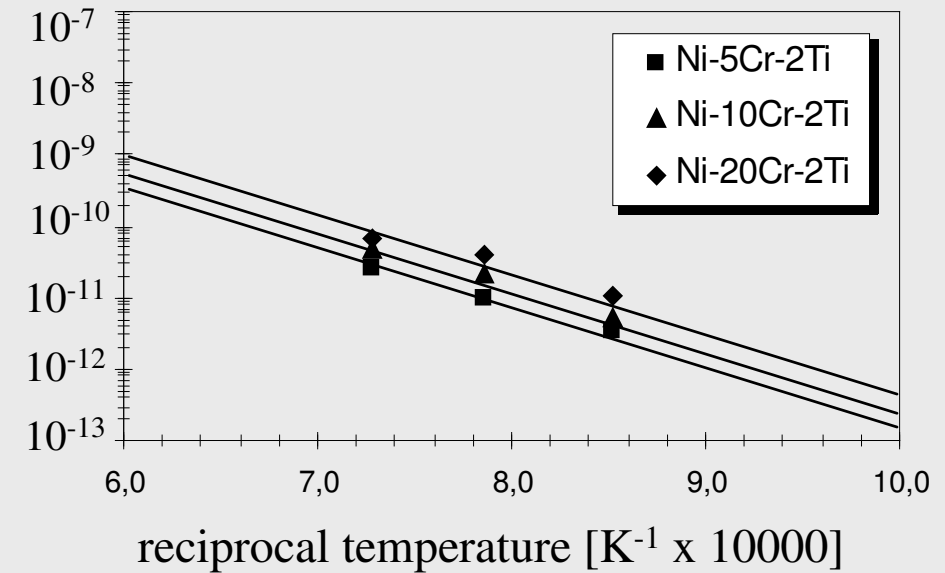
Cr enhances N solubility in Ni base alloys

Nitrogen Diffusion in Ni-Cr Alloys

precipitation depth ξ [μm]

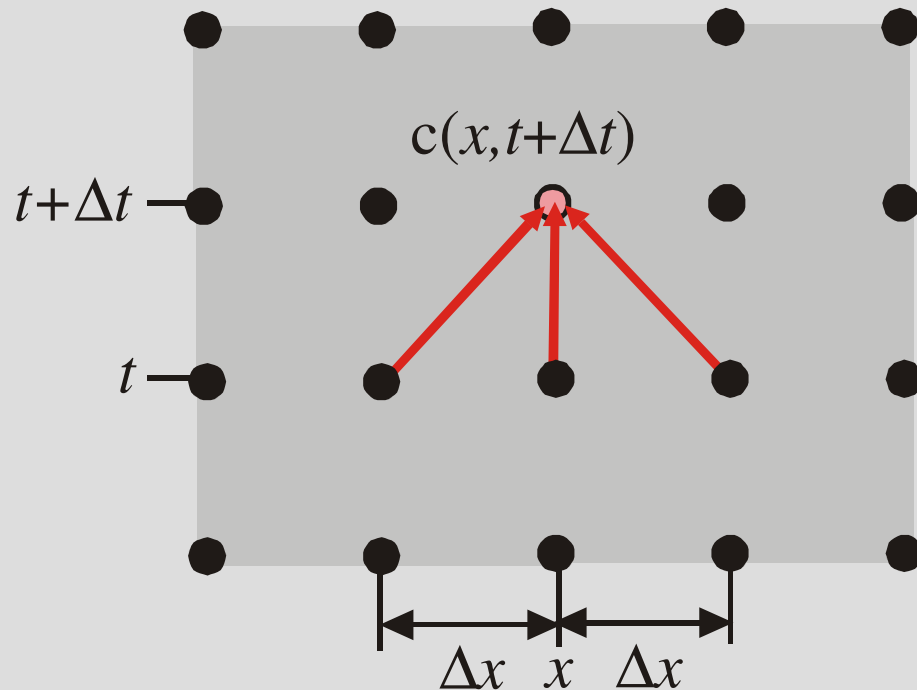


diffusion coefficient D_N [m^2/s]



$$\xi = \sqrt{\frac{2c_N^s D_N t}{v c_B^0}}$$

Finite-Difference Simulation of Diffusion Processes



$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2}$$

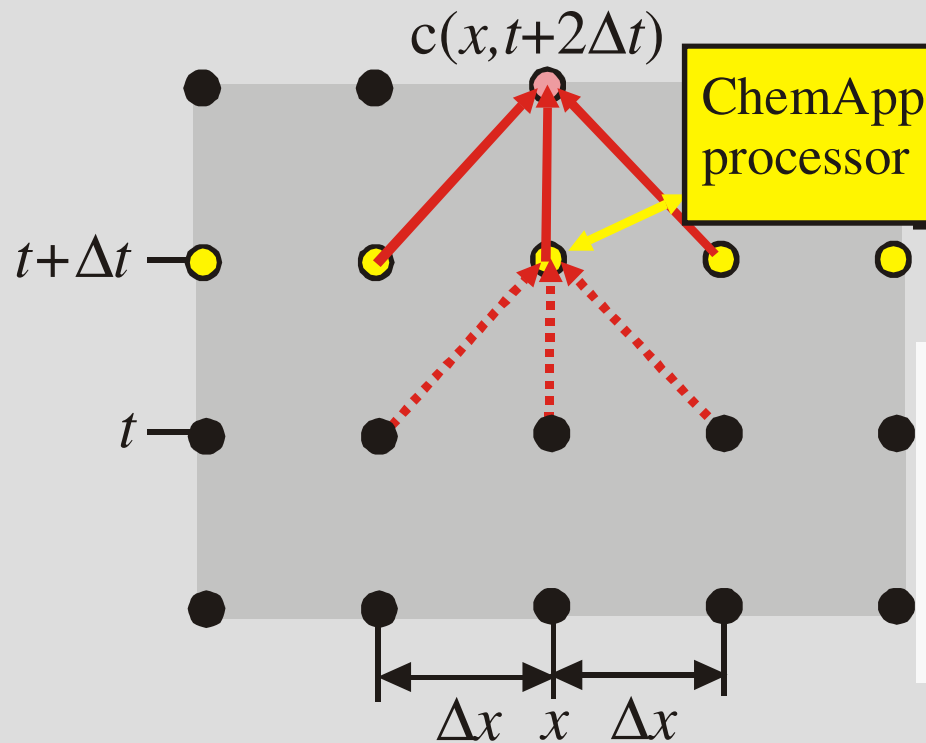
$$\left(\frac{\partial c}{\partial t} \right)_{x,t} \approx \frac{c(x, t + \Delta t) - c(x, t)}{\Delta t}$$

$$\left(\frac{\partial^2 c}{\partial x^2} \right)_{x,t} \approx \frac{c(x + \Delta x, t) - 2c(x, t) + c(x - \Delta x, t)}{\Delta x^2}$$

$$c_i(x, t + \Delta t) = c(x, t) + \frac{D\Delta t}{\Delta x^2} [c(x - \Delta x, t) - 2c(x, t) + c(x + \Delta x, t)]$$

for all species i

Finite-Difference Simulation of Diffusion Processes + Precipitation



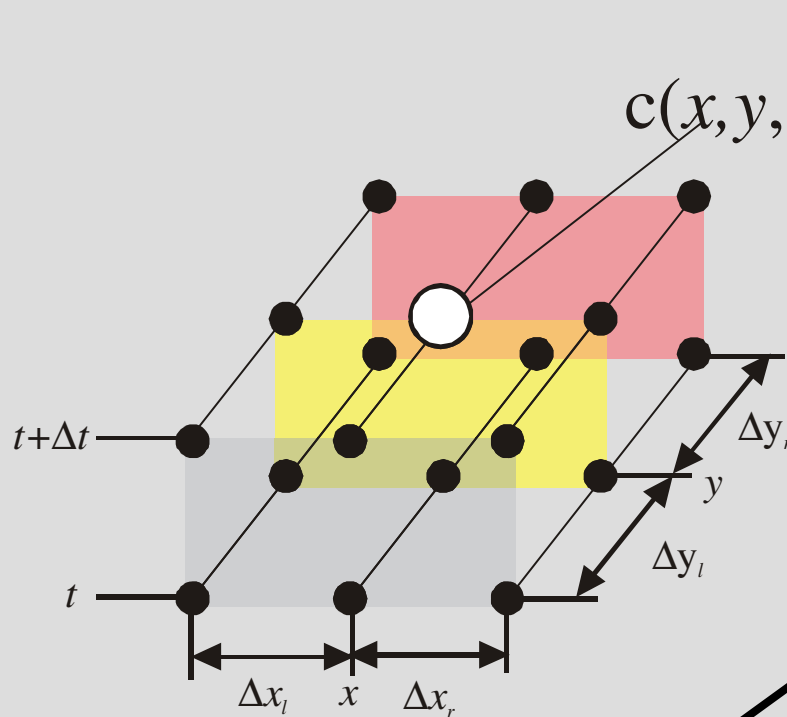
local thermodynamic equilibrium
ChemApp
+ tailored system data base

$$G = \sum_{j=1}^m c_j (G_{j,\text{pure}} + G_{j,\text{id}} + G_{j,\text{non-id}})$$

= min !

$$c(x, t + \Delta t) = c(x, t) + \frac{D\Delta t}{\Delta x^2} [c(x - \Delta x, t) - 2c(x, t) + c(x + \Delta x, t)]$$

2D Finite-Difference Treatment of Diffusion (Crank Nicolson implicit approach)



variable diffusion coefficient
(e.g., location-dependent)

$$\frac{\partial c_{O/B}}{\partial t} = D_{O/B} \frac{\partial^2 c_{O/B}}{\partial x^2}$$

$$\begin{aligned} & \frac{c(x, y, t + \Delta t) - c(x, y, t)}{\Delta t} \\ &= \frac{D_x(x, y)}{2} \left(\frac{c(x - \Delta x, y, t) - 2c(x, y, t) + c(x + \Delta x, y, t)}{\Delta x_l(x, y) \cdot \Delta x_r(x, y)} \right. \\ & \quad \left. + \frac{c(x - \Delta x, y, t + \Delta t) - 2c(x, y, t + \Delta t) + c(x + \Delta x, y, t + \Delta t)}{\Delta x_l(x, y) \cdot \Delta x_r(x, y)} \right) \\ & \quad + \frac{D_y(x, y)}{2} \left(\frac{c(x, y - \Delta y, t) - 2c(x, y, t) + c(x, y + \Delta y, t)}{\Delta y_l(x, y) \cdot \Delta y_r(x, y)} \right. \\ & \quad \left. + \frac{c(x, y - \Delta y, t + \Delta t) - 2c(x, y, t + \Delta t) + c(x, y + \Delta y, t + \Delta t)}{\Delta y_l(x, y) \cdot \Delta y_r(x, y)} \right) \end{aligned}$$

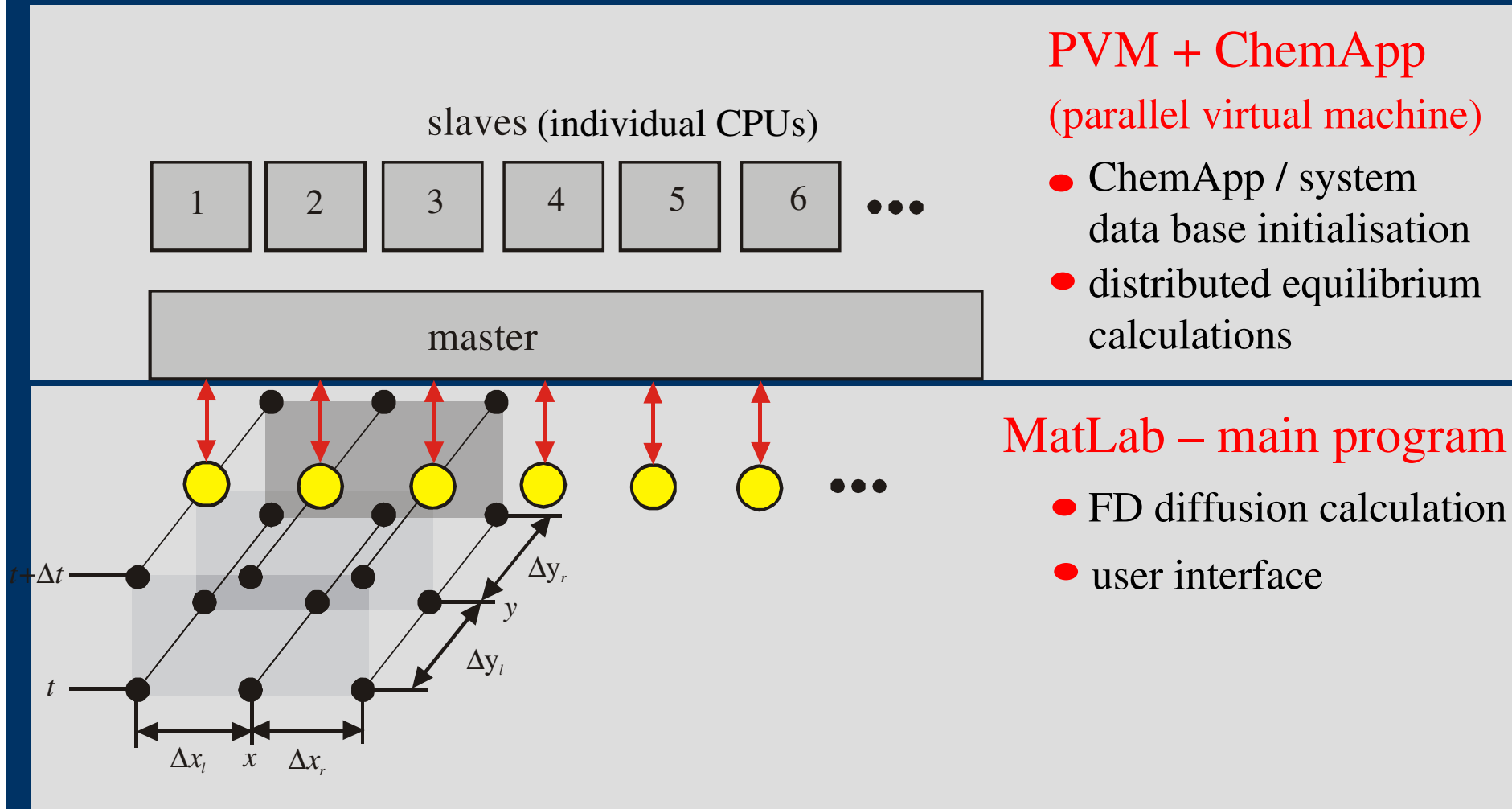
2D Finite-Difference Treatment of Diffusion (Crank Nicolson implicit approach)

PVM + ChemApp
(parallel virtual machine)

- ChemApp / system data base initialisation
- distributed equilibrium calculations

MatLab – main program

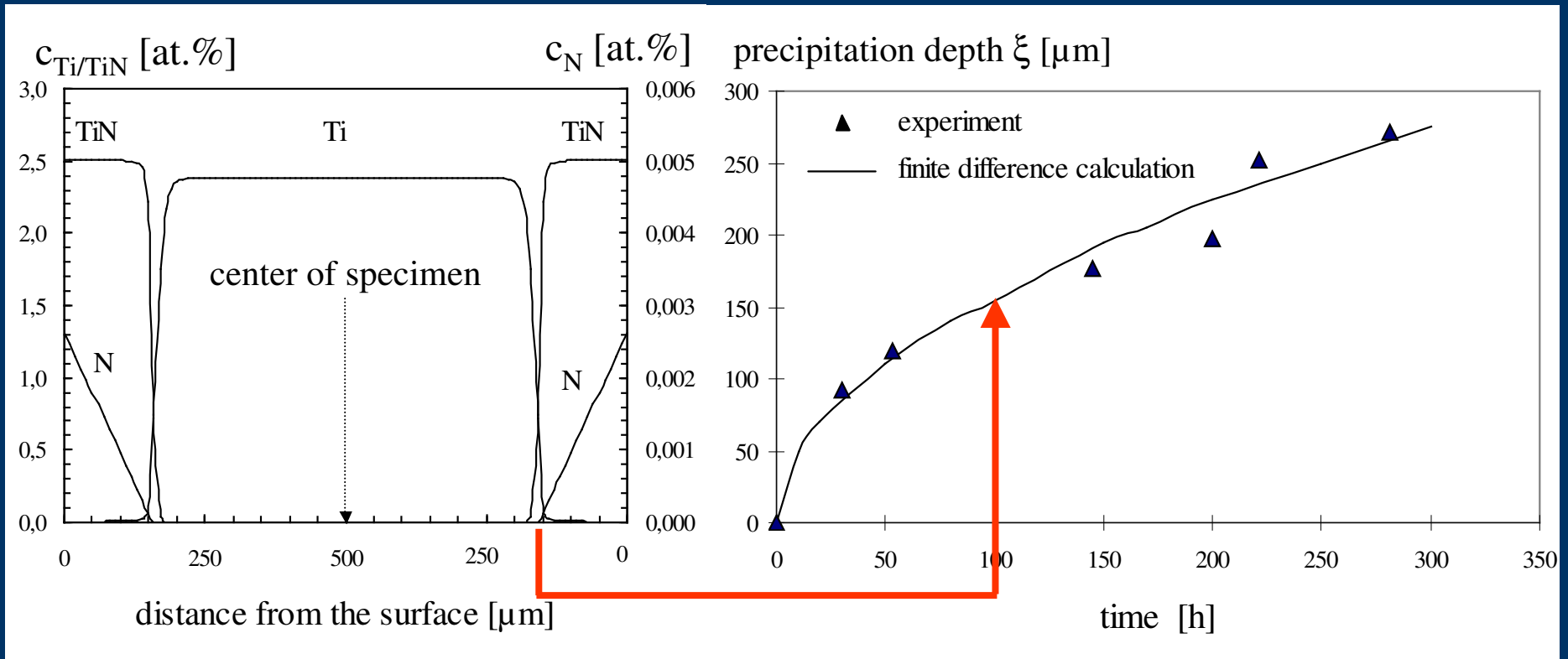
- FD diffusion calculation
- user interface



Computer Simulation of Internal Nitridation (TiN in Ni-20Cr-2Ti)

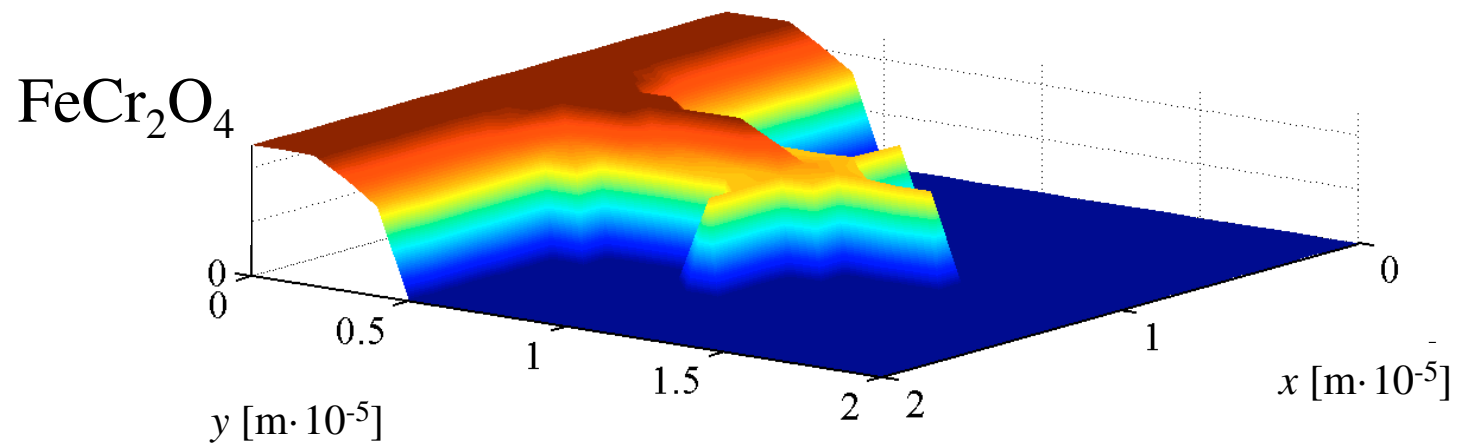
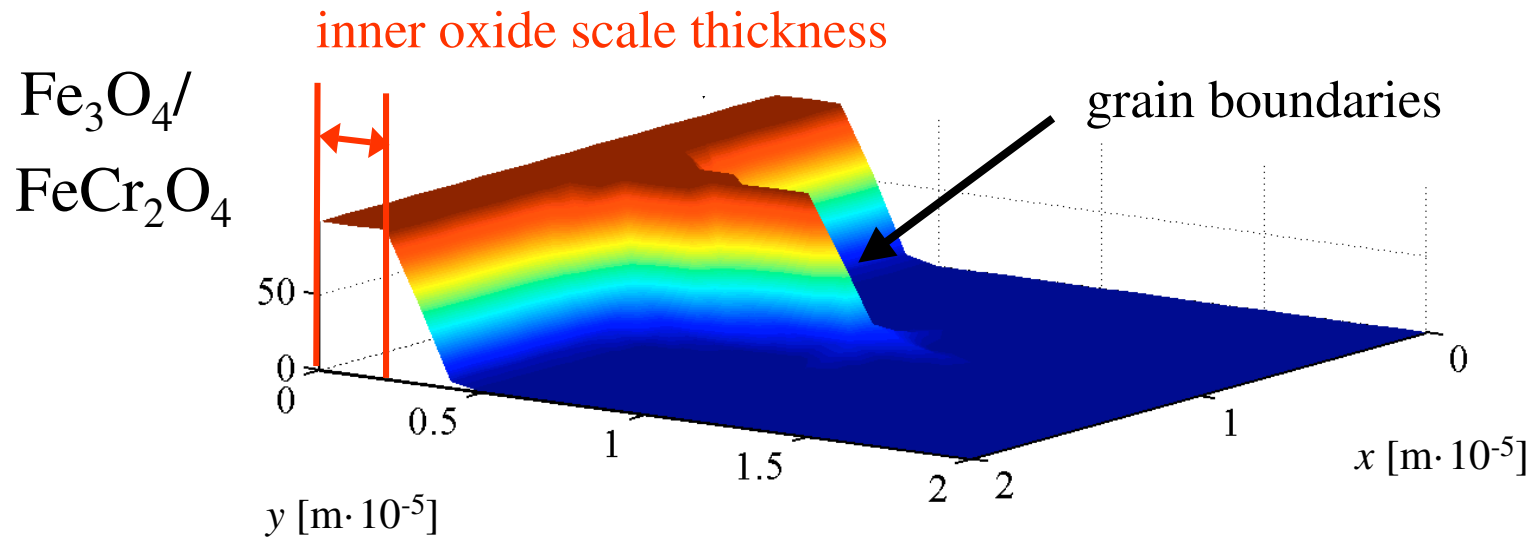
concentration profiles:

internal corrosion kinetics:



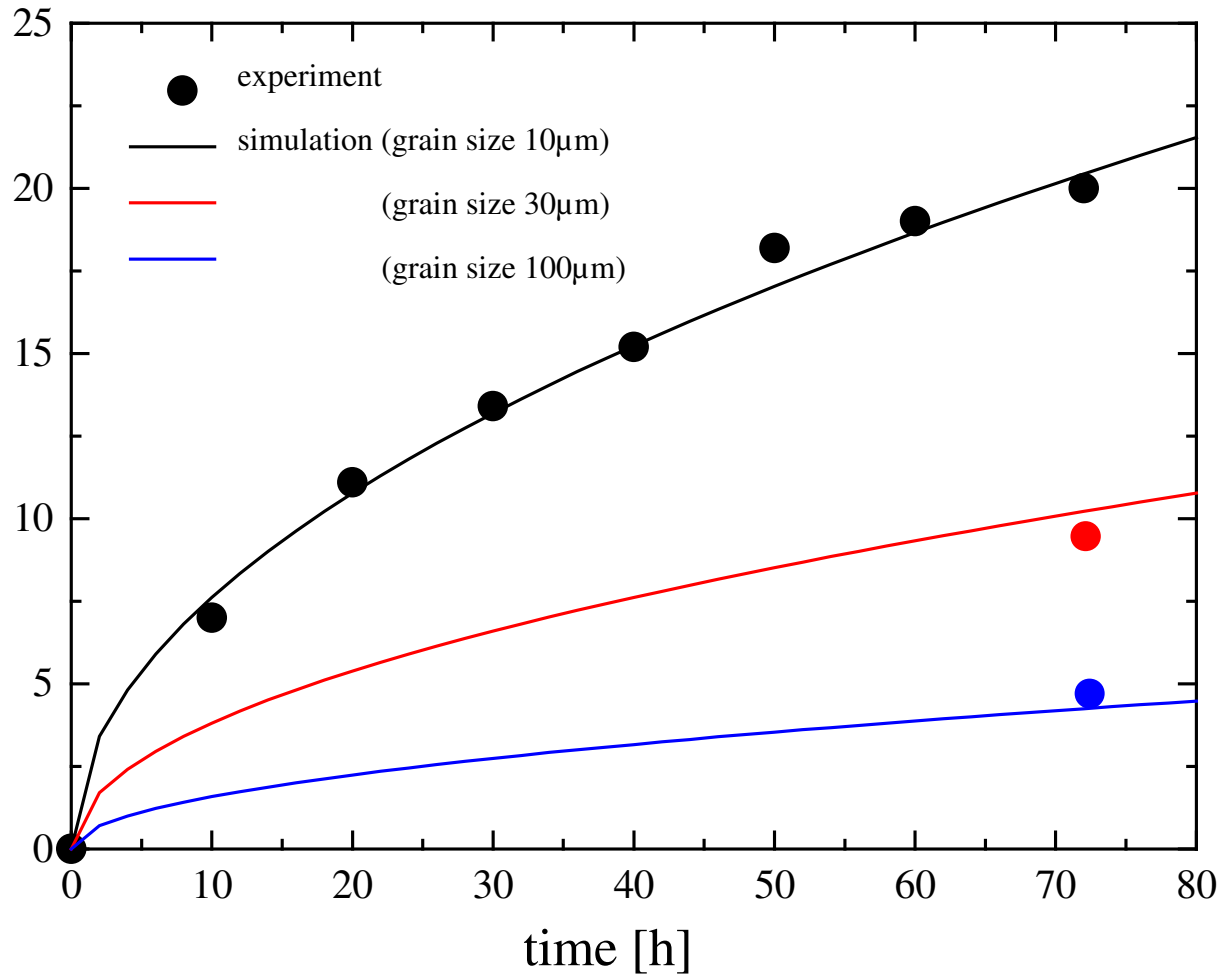
(1000°C, 100h, N₂ atmosphere)

2D Simulation of Internal Oxidation



Inner Oxide-Scale Growth (X60)


inner oxide-scale thickness [μm]



(1.43wt% Cr, 550°C, air)

Conclusions and Challenges

- internal corrosion may result in a strong deterioration of material properties (near-surface embrittlement, γ' dissolution)
- internal corrosion at lower temperatures governed by GB diffusion e.g. grain size effect of inner-oxide-scale growth on low-Cr steels



numerical model combining
-2D finite difference approach
-ChemApp + system data

flexible, sufficiently fast (parallel computation)